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NASA

MEMORANDUM

BASIC PRESSURE MEASUREMENTS AT TRANSONIC SPEEDS ON
A THIN 45° SWEPTBACK HIGHLY TAPERED WING WITH
SYSTEMATIC SPANWISE TWIST VARIATIONS

WING WITH QUADRATIC SPANWISE TWIST VARIATION

By John P. Mugler, Jr.

Langley Research Center
Langley Field, Va.

**NATIONAL AERONAUTICS AND
SPACE ADMINISTRATION**

WASHINGTON

April 1959

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SUMMARY

Pressure distributions obtained in the Langley 8-foot transonic pressure tunnel on a thin highly tapered twisted 45° sweptback wing-body combination are presented. The wing has a quadratic spanwise twist variation from 0° at 10 percent of the semispan to 6° at the tip. The tip is at a lower angle of attack than the root. Tests were made at stagnation pressures of both 0.5 and 1.0 atmosphere at Mach numbers from 0.800 to 1.200 through an angle-of-attack range from -4° to 20° .

INTRODUCTION

A research program is currently being conducted at the Langley Research Center to determine the loads due to wing twist at transonic and supersonic speeds. As part of this program, tests have been made in the Langley 8-foot transonic pressure tunnel on four wings; an untwisted wing to serve as a reference, and wings with linear, quadratic, and cubic variations of twist across the span. References 1 and 2 present the basic pressure measurements on the untwisted and linearly twisted wings, respectively. The present paper presents the basic pressure measurements on the wing with a quadratic variation of twist across the span. These data are being presented without analysis.

SYMBOLS

b	wing span
b'/2	unsupported semispan (distance from outer face of wing mounting block to tip)

c	airfoil section chord, measured parallel to plane of symmetry
\bar{c}	wing mean aerodynamic chord
c_m	wing section pitching-moment coefficient about $0.25c$, $\int_0^1 (C_{p,L} - C_{p,U}) \left(0.25 - \frac{x}{c}\right) d\left(\frac{x}{c}\right)$
c_n	wing section normal-force coefficient, $\int_0^1 (C_{p,L} - C_{p,U}) d\left(\frac{x}{c}\right)$
C_p	pressure coefficient
$C_{p,sonic}$	pressure coefficient corresponding to local Mach number of 1.0
D	diameter
l	body length
M	Mach number
q	free-stream dynamic pressure
R	Reynolds number based on \bar{c}
x	distance measured from leading edge of wing or from nose of body, positive rearward
y	spanwise distance measured from body center line
y'	spanwise distance measured from outer face of wing mounting block
$\frac{\partial \Delta \alpha}{\partial n}$	wing-twist influence coefficient due to normal load at $c/4$ point
$\frac{\partial \Delta \alpha}{\partial m}$	wing-twist influence coefficient due to moment about $c/4$ point
α	angle of attack of wing-body center line
$\Delta \alpha$	angle of attack of wing station minus angle of attack of wing-body center line

ϕ built-in twist angle

Subscripts:

L lower surface

U upper surface

APPARATUS

Tunnel

The investigation was conducted in the Langley 8-foot transonic pressure tunnel. The test section of this facility is rectangular in cross section. The upper and lower walls are slotted longitudinally to allow continuous operation through the transonic speed range with negligible effects of choking and blockage. During this investigation, the tunnel was operated at stagnation pressures of approximately 0.5 and 1.0 atmosphere. The dewpoint of the tunnel air was controlled and kept constant at approximately 0° F. The stagnation temperature of the tunnel air was automatically controlled and was kept constant and uniform across the tunnel at 123° F. Control of both dewpoint and stagnation temperature in this manner minimized humidity effects. Details of the test section have been presented in reference 3.

Models

The wing tested has the same plan form, thickness, and camber distribution as the untwisted wing described in reference 1. However, the wing of the present investigation had twist built into each wing panel from 10 percent of the semispan to the tip. The sections were twisted about their leading edge in planes parallel to the model plane of symmetry with the trailing edges up. Therefore, the tips are at a lower angle of attack than the wing-body center line. The twist varied quadratically from 0° at the 10-percent-semispan station to 6° at the tip. The wing was constructed of steel and was tested as a midwing configuration. The wing was tested in combination with the basic body of reference 1. Details of the wing-body combination are presented in figure 1 and the wing twist characteristics are presented in table I.

TESTS

The wing-body combination was tested at Mach numbers from 0.800 to 1.200 at tunnel stagnation pressures of 0.5 and 1.0 atmosphere. At the stagnation pressure of 0.5 atmosphere, the angle-of-attack range extended from -4° to 20° . At the stagnation pressure of 1.0 atmosphere, the angle-of-attack range extended from -4° to 20° only at the Mach numbers of 0.800, 0.900, and 0.940. For the remainder of the test Mach numbers at this stagnation pressure, the angle-of-attack range extended from -4° to 12° .

Transition strips were fixed on the model during all the tests. The strips were about 0.10 inch wide and were formed by sprinkling No. 120 carborundum grains on a plastic adhesive. The strips extended from the wing-body juncture to the wing tip at 10 percent of the local chord on the upper and lower wing surfaces and formed a ring around the body at 10 percent of the body length.

The Reynolds number based on the wing mean aerodynamic chord varied over the Mach number range from about 1.3×10^6 to 1.5×10^6 during tests at 0.5 atmosphere and from about 2.6×10^6 to 2.9×10^6 during tests at 1.0 atmosphere. (See fig. 2.)

MEASUREMENTS AND ACCURACY

Measurements of the local static pressures on the model were made using flush-mounted orifices distributed over the upper and lower wing surfaces and along longitudinal body rows. Figure 3 shows the location of the six stations on the wing and the five rows on the body where the orifices were located. Pressure coefficients determined from these measurements are estimated to be accurate within ± 0.006 .

The angle of attack of the model was measured with a strain-gage attitude transmitter mounted in the nose of the model and is estimated to be accurate within $\pm 0.1^{\circ}$. Calibrations of the test section of the Langley 8-foot transonic pressure tunnel indicate that local deviations from the average free-stream Mach number are of the order of ± 0.005 at subsonic speeds. With increases in Mach number, these deviations increased but did not exceed ± 0.010 in the region of the wing at $M = 1.2$. Several representative Mach number distributions at the center of the test section have been presented in reference 3. The average stream Mach number was held to within ± 0.003 of the nominal values shown in the figures.

The stagnation pressures of 1,058 and 2,116 pounds per square foot have been designated 0.5 and 1.0 atmosphere, respectively, throughout this paper. The stagnation pressure was generally held to within ± 10 pounds per square foot during tests at 0.5 atmosphere and to within ± 20 pounds per square foot during tests at 1.0 atmosphere.

Influence coefficients were obtained for this wing from a static calibration and are presented in table II. Wing-twist angles, computed by using the experimental wing section data in conjunction with the influence coefficients of table II, are estimated to be accurate to within one-quarter of a degree.

RESULTS

The pressure coefficients for the wing in the presence of the body are presented in tables III and IV for stagnation pressures of 0.5 and 1.0 atmosphere, respectively. Pressure coefficients for the body in the presence of the wing are presented in tables V and VI for stagnation pressures of 0.5 and 1.0 atmosphere, respectively. The values of the free-stream dynamic pressure shown in the tables is the average value over the angle-of-attack range. The pressure coefficients have been plotted to show the pressure-coefficient distributions over the surfaces and are presented in figure 4 for the wing in the presence of the body and in figure 5 for the body in the presence of the wing. The distributions over the wing (fig. 4) have been numerically integrated for section normal-force and section pitching-moment coefficients about 0.25c and the results are presented in table VII. The section data were used in conjunction with the influence coefficients of table II to calculate the change in angle at several wing stations and these values are also presented in table VII.

In figures 4 and 5, data have been presented for both stagnation pressures in the same figure. Fixing transition during the tests tended to minimize the effects of Reynolds number on the pressure coefficients. This fact is evident from figures 4 and 5, which show that in all cases changing the stagnation pressure from 0.5 to 1.0 atmosphere had no significant effects on the pressure coefficients over the body or over the inboard wing stations. Aeroelastic effects caused the wing to twist over the outboard regions. The results in table VII show that the outboard wing sections are generally operating at a lesser angle of attack at a stagnation pressure of 1.0 atmosphere than at 0.5 atmosphere due to the differences in dynamic pressure. Therefore, the differences in the pressure distributions over the outboard wing sections at the two

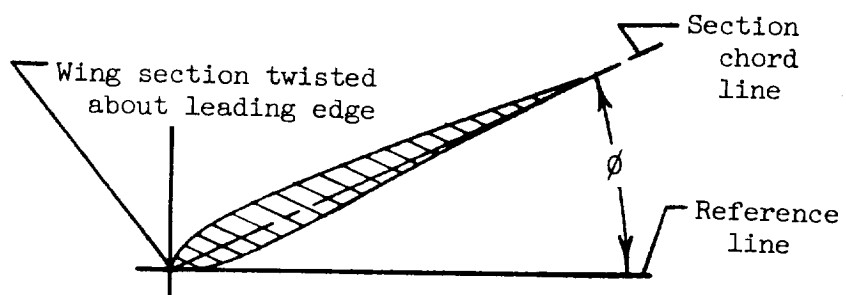
different stagnation pressures in figure 4 should be attributed to the differences in local angle of attack and not to Reynolds number effects.

Langley Research Center,
National Aeronautics and Space Administration,
Langley Field, Va., December 9, 1958.

REFERENCES

1. Mugler, John P., Jr.: Basic Pressure Measurements at Transonic Speeds on a Thin 45° Sweptback Highly Tapered Wing With Systematic Spanwise Twist Variations - Untwisted Wing. NASA MEMO 10-20-58L, 1958.
2. Mugler, John P., Jr.: Basic Pressure Measurements at Transonic Speeds on a Thin 45° Sweptback Highly Tapered Wing With Systematic Spanwise Twist Variations - Wing With Linear Spanwise Twist Variation. NASA MEMO 12-28-58L, 1959.
3. Mugler, John P., Jr.: Transonic Wind-Tunnel Investigation of the Aerodynamic Loading Characteristics of a 60° Delta Wing in the Presence of a Body With and Without Indentation. NACA RM L55G11, 1955.

TABLE I.- WING TWIST CHARACTERISTICS



Typical Section

$\frac{y}{b/2}$	ϕ , deg
0	0
.10	0
.12	.003
.25	.167
.40	.667
.60	1.852
.80	3.630
.95	5.352
1.00	6.000

TABLE II.- WING DEFLECTION CHARACTERISTICS

Twist measurement station, $\frac{y}{b/2}$	Rate of change in twist angle due to a load at section quarter chord, $\frac{\partial \Delta\alpha}{\partial n}$, deg/lb, at -				
	$\frac{y'}{b'/2} = 0.185$	$\frac{y'}{b'/2} = 0.348$	$\frac{y'}{b'/2} = 0.565$	$\frac{y'}{b'/2} = 0.795$	$\frac{y'}{b'/2} = 0.948$
0.25	0	-0.0002	-0.0007	-0.0010	-0.0006
.40	0	-.0002	-.0018	-.0029	-.0044
.60	0	-.0001	-.0014	-.0108	-.0175
.80	0	-.0001	-.0010	-.0116	-.0481
.95	0	-.0001	-.0008	-.0108	-.0640

Twist measurement station, $\frac{y}{b/2}$	Rate of change in twist angle due to a pitching moment about section quarter chord, $\frac{\partial \Delta\alpha}{\partial m}$, deg/in-lb, at -				
	$\frac{y'}{b'/2} = 0.185$	$\frac{y'}{b'/2} = 0.348$	$\frac{y'}{b'/2} = 0.565$	$\frac{y'}{b'/2} = 0.795$	$\frac{y'}{b'/2} = 0.948$
0.25	0.0001	0.0001	0.0001	0.0001	0.0005
.40	.0002	.0003	.0002	.0004	.0008
.60	.0002	.0006	.0024	.0027	.0021
.80	.0002	.0007	.0037	.0155	.0122
.95	.0002	.0007	.0037	.0245	.0970

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY

(a) 12-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 310 \text{ lb/sq ft}$												
Upper surface	.000	.197	.407	.515	.525	.507	.282	-.042	-.342	-.579	.000	
	.032	.316	.208	.098	-.015	-.157	-.472	-.810	-1.553	-1.337	.032	
	.078	.198	.105	.020	-.063	-.165	-.356	-.606	-.879	-1.240	.078	
	.150	.099	.018	-.060	-.137	-.227	-.404	-.593	-.771	-1.102	.150	
	.250	.018	-.054	-.127	-.191	-.272	-.444	-.612	-.605	-.901	.250	
	.350	-.001	-.070	-.132	-.188	-.256	-.411	-.553	-.588	-.766	.350	
	.450	-.048	-.111	-.173	-.220	-.291	-.433	-.521	-.613	-.701	.450	
	.550	-.084	-.140	-.196	-.246	-.307	-.443	-.466	-.629	-.666	.550	
	.650	-.057	-.108	-.155	-.195	-.248	-.338	-.387	-.554	-.605	.650	
	.760	-.050	-.093	-.129	-.157	-.193	-.254	-.347	-.485	-.568	.760	
	.840	-.052	-.083	-.110	-.127	-.153	-.189	-.271	-.424	-.566	.840	
	.926	-.029	-.050	-.066	-.077	-.090	-.109	-.169	-.317	-.516	.926	
Lower surface	.035	-.373	-.262	-.109	.022	.146	.355	.535	.695	.813	.035	
	.082										.082	
	.150	-.236	-.154	-.075	-.000	.078	.219	.354	.434	.574	.150	
	.250										.250	
	.350	-.222	-.159	-.091	-.033	.029	.144	.249	.357	.428	.350	
	.450	-.240	-.183	-.119	-.062	-.006	.099	.197	.287	.364	.450	
	.550	-.228	-.177	-.121	-.068	-.018	.075	.162	.245	.315	.550	
	.650	-.205	-.161	-.110	-.064	-.019	.061	.135	.201	.259	.650	
	.750	-.138	-.108	-.070	-.031	.004	.074	.130	.179	.220	.750	
	.850	-.090	-.069	-.038	-.010	.020	.075	.105	.135	.156	.850	
	.900	-.065	-.050	-.029	-.005	.020	.060	.077	.095	.101	.900	
$M = 0.900; q = 358 \text{ lb/sq ft}$												
Upper surface	.000	.318	.467	.548	.560	.544	.406	.164	-.073	-.299	.000	
	.032	.326	.221	.122	.013	-.109	-.390	-.733	-1.297	-1.286	.032	
	.078	.210	.123	.038	-.041	-.122	-.281	-.471	-.771	-1.231	.078	
	.150	.104	.022	-.049	-.130	-.209	-.354	-.496	-.631	-.908	.150	
	.250	.017	-.060	-.134	-.203	-.279	-.392	-.525	-.632	-.709	.250	
	.350	-.008	-.078	-.143	-.206	-.266	-.397	-.521	-.615	-.668	.350	
	.450	-.065	-.133	-.197	-.258	-.316	-.435	-.552	-.640	-.683	.450	
	.550	-.115	-.180	-.259	-.335	-.392	-.500	-.608	-.539	-.692	.550	
	.650	-.086	-.140	-.203	-.289	-.381	-.487	-.582	-.568	-.619	.650	
	.760	-.073	-.121	-.169	-.221	-.345	-.497	-.513	-.587	-.601	.760	
	.840	-.077	-.110	-.143	-.174	-.211	-.508	-.426	-.620	-.631	.840	
	.926	-.050	-.069	-.088	-.101	-.100	-.217	-.240	-.512	-.577	.926	
Lower surface	.035	-.348	-.235	-.094	.034	.146	.359	.550	.712	.839	.035	
	.082										.082	
	.150	-.226	-.156	-.072	-.004	.074	.231	.373	.501	.603	.150	
	.250										.250	
	.350	-.247	-.181	-.107	-.047	.015	.146	.265	.375	.465	.350	
	.450	-.271	-.221	-.149	-.089	-.025	.099	.205	.306	.395	.450	
	.550	-.325	-.246	-.167	-.108	-.045	.068	.166	.259	.346	.550	
	.650	-.331	-.226	-.153	-.098	-.048	.053	.134	.216	.296	.650	
	.750	-.208	-.145	-.094	-.053	-.013	.068	.127	.194	.262	.750	
	.850	-.118	-.091	-.056	-.025	.007	.065	.105	.145	.206	.850	
	.900	-.081	-.066	-.043	-.016	.008	.051	.075	.104	.153	.900	

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 368 lb/sq ft												
Upper surface	.000	.373	.492	.569	.581	.569	.451	.229	.010	-.221	.000	
	.032	.336	.239	.136	.036	-.079	-.343	-.658	-1.238	-1.383	.032	
	.078	.218	.139	.056	-.016	-.092	-.252	-.404	-.689	-1.357	.078	
	.150	.110	.036	-.037	-.111	-.182	-.313	-.442	-.556	-.719	.150	
	.250	.016	-.052	-.128	-.192	-.246	-.361	-.477	-.574	-.560	.250	
	.350	-.010	-.074	-.138	-.194	-.259	-.375	-.486	-.581	-.557	.350	
	.450	-.072	-.135	-.198	-.247	-.299	-.409	-.509	-.601	-.638	.450	
	.550	-.132	-.209	-.277	-.324	-.374	-.470	-.573	-.629	-.696	.550	
	.650	-.095	-.159	-.261	-.316	-.368	-.472	-.562	-.655	-.692	.650	
	.760	-.087	-.143	-.236	-.317	-.374	-.481	-.550	-.605	-.640	.760	
	.840	-.092	-.128	-.179	-.330	-.403	-.531	-.548	-.535	-.671	.840	
	.926	-.057	-.074	-.084	-.161	-.306	-.486	-.436	-.526	-.625	.926	
Lower surface	.035	-.310	-.220	-.073	.036	.149	.358	.555	.722	.857	.035	
	.082										.082	
	.150	-.207	-.146	-.068	-.005	.076	.227	.375	.513	.625	.150	
	.250										.250	
	.350	-.240	-.186	-.106	-.057	.013	.138	.263	.382	.487	.350	
	.450	-.268	-.211	-.155	-.102	-.034	.086	.201	.318	.420	.450	
	.550	-.316	-.272	-.204	-.135	-.057	.055	.168	.276	.368	.550	
	.650	-.338	-.302	-.207	-.127	-.064	.035	.132	.231	.318	.650	
	.750	-.317	-.258	-.121	-.074	-.031	.051	.128	.212	.286	.750	
	.850	-.285	-.140	-.067	-.037	-.007	.043	.104	.167	.239	.850	
	.900	-.198	-.082	-.044	-.025	-.008	.022	.070	.127	.186	.900	
M = 0.980; q = 385 lb/sq ft												
Upper surface	.000	.426	.536	.595	.609	.594	.497	.295	.095	-.127	.000	
	.032	.358	.261	.164	.068	-.039	-.292	-.596	-1.090	-1.230	.032	
	.078	.244	.163	.088	.019	-.053	-.202	-.352	-.567	-1.115	.078	
	.150	.129	.057	-.010	-.079	-.147	-.261	-.381	-.477	-.574	.150	
	.250	.034	-.037	-.109	-.159	-.213	-.318	-.416	-.510	-.607	.250	
	.350	.006	-.055	-.115	-.179	-.226	-.327	-.429	-.518	-.624	.350	
	.450	-.061	-.117	-.170	-.219	-.272	-.363	-.453	-.542	-.649	.450	
	.550	-.147	-.202	-.247	-.293	-.337	-.422	-.516	-.600	-.699	.550	
	.650	-.119	-.191	-.245	-.292	-.342	-.432	-.514	-.609	-.689	.650	
	.760	-.116	-.198	-.258	-.308	-.354	-.443	-.528	-.621	-.693	.760	
	.840	-.168	-.242	-.298	-.349	-.401	-.495	-.575	-.658	-.742	.840	
	.926	-.165	-.231	-.293	-.334	-.383	-.478	-.559	-.602	-.696	.926	
Lower surface	.035	-.269	-.165	-.043	.070	.176	.384	.576	.740	.885	.035	
	.082										.082	
	.150	-.165	-.106	-.043	.025	.094	.251	.403	.535	.653	.150	
	.250										.250	
	.350	-.221	-.162	-.092	-.038	.022	.161	.290	.412	.516	.350	
	.450	-.246	-.187	-.128	-.083	-.033	.101	.229	.344	.450	.450	
	.550	-.296	-.239	-.193	-.141	-.079	.064	.189	.304	.404	.550	
	.650	-.324	-.279	-.222	-.175	-.104	.041	.159	.262	.356	.650	
	.750	-.312	-.262	-.208	-.151	-.070	.053	.151	.243	.326	.750	
	.850	-.307	-.248	-.195	-.136	-.053	.041	.124	.205	.279	.850	
	.900	-.315	-.257	-.205	-.149	-.067	.015	.091	.164	.232	.900	

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 400 lb/sq ft												
Upper surface		.000	.495	.588	.638	.647	.642	.561	.372	.176	-.031	.000
		.032	.402	.307	.213	.117	.017	-.203	-.507	-1.006	-1.111	.032
		.078	.295	.214	.138	.073	.008	-.117	-.281	-.507	-1.011	.078
		.150	.183	.112	.043	-.022	-.085	-.176	-.295	-.387	-.476	.150
		.250	.086	.016	-.052	-.100	-.149	-.235	-.333	-.421	-.511	.250
		.350	.064	.007	-.065	-.118	-.165	-.247	-.346	-.433	-.527	.350
		.450	-.001	-.053	-.117	-.161	-.207	-.279	-.377	-.458	-.551	.450
		.550	-.085	-.133	-.185	-.226	-.268	-.339	-.430	-.510	-.602	.550
		.650	-.069	-.124	-.185	-.230	-.276	-.347	-.433	-.521	-.607	.650
		.760	-.074	-.130	-.197	-.242	-.286	-.364	-.449	-.534	-.604	.760
		.840	-.120	-.178	-.242	-.290	-.333	-.414	-.495	-.575	-.651	.840
		.926	-.118	-.170	-.232	-.274	-.317	-.401	-.484	-.568	-.632	.926
Lower surface		.035	-.188	-.106	.009	.115	.218	.431	.625	.788	.922	.035
		.082										.082
		.150	-.095	-.047	.011	.070	.139	.301	.452	.589	.697	.150
		.250										.250
		.350	-.147	-.111	-.047	.004	.075	.207	.342	.463	.566	.350
		.450	-.169	-.135	-.074	-.025	.024	.154	.281	.401	.501	.450
		.550	-.220	-.180	-.130	-.086	-.026	.116	.243	.358	.462	.550
		.650	-.247	-.216	-.161	-.119	-.055	.087	.210	.321	.412	.650
		.750	-.235	-.203	-.153	-.103	-.028	.103	.207	.305	.386	.750
		.850	-.234	-.189	-.139	-.086	-.021	.091	.181	.261	.342	.850
		.900	-.241	-.197	-.150	-.098	-.034	.071	.149	.225	.295	.900
M = 1.125; q = 421 lb/sq ft												
Upper surface		.000	.529	.582	.623	.628	.614	.581	.495	.451	.139	.000
		.032	.355	.259	.178	.075	-.025	-.249	-.471	-.858	-.920	.032
		.078	.270	.193	.135	.060	-.007	-.156	-.282	-.461	-.843	.078
		.150	.176	.111	.047	-.034	-.080	-.174	-.258	-.321	-.362	.150
		.250	.081	.024	-.016	-.076	-.126	-.206	-.279	-.337	-.378	.250
		.350	.071	.009	-.038	-.084	-.141	-.227	-.287	-.351	-.402	.350
		.450	.018	-.033	-.077	-.123	-.171	-.243	-.310	-.372	-.423	.450
		.550	-.045	-.097	-.131	-.177	-.223	-.291	-.364	-.416	-.466	.550
		.650	-.036	-.089	-.133	-.184	-.230	-.301	-.356	-.425	-.470	.650
		.760	-.053	-.105	-.147	-.197	-.242	-.307	-.370	-.431	-.463	.760
		.840	-.103	-.157	-.193	-.244	-.284	-.349	-.405	-.470	-.502	.840
		.926	-.081	-.138	-.174	-.224	-.268	-.337	-.399	-.463	-.494	.926
Lower surface		.035	-.209	-.117	-.008	.068	.170	.356	.574	.818	.985	.035
		.082										.082
		.150	-.091	-.040	.022	.072	.134	.272	.441	.614	.753	.150
		.250										.250
		.350	-.127	-.085	-.019	.007	.068	.208	.345	.504	.631	.350
		.450	-.144	-.101	-.036	-.000	.059	.162	.294	.446	.575	.450
		.550	-.185	-.151	-.087	-.050	.001	.117	.258	.413	.537	.550
		.650	-.209	-.174	-.116	-.079	-.031	.095	.233	.382	.498	.650
		.750	-.201	-.165	-.102	-.065	-.016	.122	.245	.374	.475	.750
		.850	-.183	-.146	-.086	-.050	.003	.125	.234	.343	.438	.850
		.900	-.189	-.151	-.095	-.056	-.004	.108	.209	.314	.395	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Concluded

		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 1.200; q = 436 \text{ lb/sq ft}$											
Upper surface	.000	.557	.605	.636	.641	.634	.602	.509	.429	.496	.000
	.032	.344	.256	.164	.079	-.023	-.219	-.424	-.701	-.753	.032
	.078	.268	.200	.133	.061	.011	-.148	-.273	-.380	-.738	.078
	.150	.165	.098	.040	.000	-.060	-.138	-.237	-.298	-.379	.150
	.250	.117	.061	-.003	-.064	-.098	-.178	-.248	-.296	-.339	.250
	.350	.096	.044	-.006	-.045	-.100	-.185	-.251	-.307	-.359	.350
	.450	.055	.004	-.040	-.077	-.123	-.199	-.270	-.332	-.380	.450
	.550	-.001	-.051	-.094	-.135	-.175	-.242	-.308	-.367	-.421	.550
	.650	-.001	-.055	-.105	-.144	-.184	-.250	-.317	-.373	-.435	.650
	.760	-.025	-.069	-.113	-.148	-.184	-.254	-.325	-.376	-.443	.760
	.840	-.084	-.128	-.167	-.205	-.236	-.302	-.364	-.416	-.476	.840
	.926	-.068	-.115	-.158	-.188	-.228	-.299	-.357	-.421	-.478	.926
Lower surface	.035	-.187	-.100	-.008	.081	.175	.348	.528	.702	.876	.035
	.082										.082
	.150	-.064	-.020	.038	.094	.137	.259	.425	.581	.732	.150
	.250										.250
	.350	-.093	-.052	-.008	.039	.095	.221	.353	.476	.605	.350
	.450	-.107	-.062	-.016	.032	.082	.192	.302	.424	.550	.450
	.550	-.149	-.109	-.070	-.023	.028	.145	.256	.390	.516	.550
	.650	-.175	-.132	-.090	-.044	.013	.110	.223	.355	.478	.650
	.750	-.167	-.125	-.085	-.037	.010	.111	.236	.362	.467	.750
	.850	-.145	-.114	-.083	-.038	.006	.113	.245	.347	.436	.850
	.900	-.162	-.118	-.088	-.055	-.013	.099	.232	.321	.400	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.800; q = 310 lb/sq ft											
Upper surface	.000	-.380	-.009	.323	.417	.364	-.163	-.674	-1.041	-1.169	.000
	.025	.313	.212	.075	-.102	-.349	-1.053	-1.359	-1.264	-1.092	.025
	.076	.160	.070	-.050	-.174	-.333	-.630	-1.118	-1.259	-1.111	.076
	.150										.150
	.250	.002	-.075	-.164	-.244	-.335	-.546	-.900	-1.183	-1.029	.250
	.350	-.050	-.120	-.197	-.262	-.346	-.528	-.689	-1.064	-.987	.350
	.450	-.074	-.138	-.198	-.261	-.326	-.477	-.503	-.939	-.916	.450
	.550	-.070	-.121	-.174	-.220	-.278	-.384	-.449	-.785	-.845	.550
	.650	-.065	-.111	-.151	-.188	-.234	-.303	-.410	-.663	-.783	.650
	.750	-.047	-.078	-.118	-.132	-.167	-.209	-.321	-.580	-.747	.750
Lower surface	.850	-.018	-.043	-.064	-.075	-.091	-.119	-.220	-.477	-.704	.850
	.926	.011	-.002	-.007	-.011	-.022	-.035	-.117	-.373	-.650	.926
	.023	-.658	-.512	-.219	-.004	.170	.385	.490	.558	.595	.023
	.072	-.516	-.296	-.124	-.016	.102	.277	.402	.510	.579	.072
	.150	-.431	-.232	-.096	-.011	.073	.219	.337	.442	.520	.150
	.250	-.302	-.200	-.109	-.035	.036	.164	.268	.369	.444	.250
	.350	-.252	-.182	-.109	-.043	.018	.133	.231	.316	.386	.350
	.450	-.225	-.174	-.111	-.059	.003	.099	.185	.264	.324	.450
	.550	-.191	-.146	-.096	-.047	.002	.087	.160	.225	.279	.550
	.650	-.143	-.110	-.070	-.030	.012	.087	.139	.185	.230	.650
Upper surface	.750	-.085	-.063	-.031	.003	.033	.092	.129	.153	.183	.750
	.860	-.029	-.019	-.001	.023	.052	.085	.101	.090	.093	.860
	.900	-.006	.003	.015	.036	.052	.079	.079	.045	.025	.900
M = 0.900; q = 358 lb/sq ft											
Upper surface	.000	-.250	.072	.331	.417	.394	-.057	-.384	-.754	-.842	.000
	.025	.306	.207	.083	-.079	-.291	-.939	-1.208	-1.203	-.932	.025
	.076	.159	.060	-.052	-.171	-.313	-.549	-1.003	-1.183	-.958	.076
	.150										.150
	.250	-.013	-.092	-.180	-.260	-.344	-.521	-.711	-1.010	-.969	.250
	.350	-.069	-.149	-.231	-.317	-.376	-.536	-.681	-.938	-.942	.350
	.450	-.102	-.170	-.256	-.372	-.442	-.577	-.661	-.874	-.893	.450
	.550	-.094	-.160	-.224	-.301	-.417	-.558	-.622	-.796	-.843	.550
	.650	-.091	-.143	-.200	-.263	-.417	-.570	-.590	-.715	-.794	.650
	.750	-.065	-.107	-.144	-.184	-.216	-.524	-.521	-.666	-.755	.750
Lower surface	.850	-.035	-.060	-.082	-.098	-.092	-.189	-.361	-.608	-.726	.850
	.926	.005	-.010	-.016	-.020	-.012	-.055	-.218	-.522	-.681	.926
	.023	-.673	-.506	-.243	-.024	.147	.375	.503	.583	.638	.023
	.072	-.512	-.286	-.141	-.030	.083	.271	.412	.522	.605	.072
	.150	-.404	-.250	-.117	-.029	.056	.218	.348	.455	.547	.150
	.250	-.360	-.238	-.136	-.058	.016	.157	.277	.387	.473	.250
	.350	-.328	-.230	-.143	-.071	-.004	.125	.233	.333	.420	.350
	.450	-.338	-.239	-.154	-.086	-.025	.091	.187	.282	.361	.450
	.550	-.325	-.204	-.132	-.076	-.021	.077	.159	.241	.316	.550
	.650	-.220	-.152	-.097	-.049	-.008	.077	.136	.206	.269	.650
Lower surface	.750	-.114	-.084	-.050	-.013	.020	.083	.124	.171	.224	.750
	.860	-.040	-.028	-.008	.018	.039	.076	.087	.110	.145	.860
	.900	-.008	-.004	.010	.033	.048	.065	.055	.054	.082	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 368 lb/sq ft											
Upper surface	.000	-.184	.095	.341	.426	.411	.133	-.281	-.648	-.900	.000
	.025	.304	.211	.090	-.058	-.258	-.782	-1.086	-1.213	-1.169	.025
	.076	.158	.070	-.041	-.151	-.289	-.508	-.873	-1.192	-1.142	.076
	.150										.150
	.250	-.016	-.088	-.175	-.242	-.339	-.494	-.642	-1.190	-1.069	.250
	.350	-.080	-.155	-.235	-.292	-.363	-.499	-.642	-.952	-1.044	.350
	.450	-.114	-.200	-.307	-.364	-.418	-.550	-.662	-.784	-.968	.450
	.550	-.112	-.182	-.276	-.343	-.407	-.536	-.630	-.717	-.888	.550
	.650	-.109	-.172	-.282	-.368	-.432	-.552	-.616	-.683	-.826	.650
	.750	-.083	-.122	-.180	-.331	-.404	-.522	-.571	-.667	-.766	.750
Lower surface	.850	-.045	-.065	-.079	-.153	-.349	-.488	-.503	-.629	-.743	.850
	.926	.004	-.004	-.008	-.000	-.075	-.200	-.288	-.528	-.669	.926
	.023	-.624	-.512	-.243	-.040	.138	.370	.509	.597	.655	.023
	.072	-.460	-.302	-.136	-.044	.073	.261	.409	.531	.628	.072
	.150	-.366	-.259	-.119	-.040	.050	.211	.346	.465	.571	.150
	.250	-.342	-.247	-.146	-.077	.006	.145	.277	.394	.495	.250
	.350	-.321	-.241	-.160	-.092	-.015	.113	.232	.344	.442	.350
	.450	-.331	-.274	-.196	-.119	-.042	.074	.182	.290	.385	.450
	.550	-.333	-.287	-.183	-.107	-.039	.059	.159	.253	.338	.550
	.650	-.332	-.280	-.126	-.076	-.023	.052	.134	.218	.295	.650
Upper surface	.750	-.295	-.133	-.057	-.026	.004	.061	.120	.190	.255	.750
	.860	-.089	-.133	-.006	.011	.025	.042	.080	.131	.180	.860
	.900	-.017	.005	.015	.031	.033	.021	.048	.075	.122	.900
M = 0.980; q = 385 lb/sq ft											
Upper surface	.000	-.111	.159	.363	.442	.436	.209	-.194	-.534	-.801	.000
	.025	.319	.225	.114	-.023	-.209	-.701	-1.019	-1.166	-1.206	.025
	.076	.173	.082	-.018	-.120	-.247	-.476	-.827	-1.077	-1.182	.076
	.150										.150
	.250	-.004	-.075	-.146	-.232	-.306	-.447	-.576	-1.079	-1.215	.250
	.350	-.076	-.143	-.207	-.269	-.333	-.452	-.580	-.996	-1.209	.350
	.450	-.137	-.217	-.281	-.334	-.388	-.504	-.610	-.759	-1.130	.450
	.550	-.130	-.205	-.269	-.322	-.382	-.495	-.611	-.782	-.796	.550
	.650	-.156	-.239	-.301	-.355	-.410	-.513	-.617	-.765	-.745	.650
	.750	-.147	-.220	-.289	-.332	-.386	-.486	-.597	-.751	-.744	.750
Lower surface	.850	-.148	-.225	-.286	-.339	-.389	-.484	-.587	-.745	-.765	.850
	.926	-.129	-.195	-.241	-.282	-.334	-.388	-.452	-.617	-.657	.926
	.023	-.589	-.462	-.222	-.020	.145	.387	.532	.620	.681	.023
	.072	-.426	-.237	-.119	-.025	.086	.287	.435	.553	.654	.072
	.150	-.324	-.213	-.110	-.023	.058	.230	.368	.488	.599	.150
	.250	-.319	-.216	-.123	-.061	.011	.167	.296	.417	.526	.250
	.350	-.304	-.221	-.138	-.083	-.024	.120	.255	.371	.477	.350
	.450	-.317	-.251	-.182	-.136	-.065	.080	.208	.314	.419	.450
	.550	-.324	-.262	-.204	-.156	-.086	.067	.179	.283	.376	.550
	.650	-.332	-.275	-.215	-.163	-.076	.057	.156	.250	.336	.650

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 1.030; q = 400 \text{ lb/sq ft}$												
Upper surface		.000	-.014	.220	.404	.482	.481	.290	-.093	-.436	-.682	.000
		.025	.365	.273	.166	.037	-.135	-.583	-1.013	-1.047	-1.081	.025
		.076	.220	.135	.037	-.059	-.177	-.394	-.890	-.991	-1.078	.076
		.150										.150
		.250	.054	-.017	-.101	-.171	-.241	-.359	-.476	-.968	-1.079	.250
		.350	-.018	-.072	-.149	-.207	-.267	-.367	-.485	-.927	-1.079	.350
		.450	-.085	-.147	-.212	-.268	-.319	-.413	-.516	-.750	-1.049	.450
		.550	-.079	-.138	-.210	-.259	-.312	-.412	-.517	-.520	-.778	.550
		.650	-.113	-.170	-.239	-.294	-.338	-.426	-.529	-.560	-.669	.650
		.750	-.105	-.153	-.226	-.270	-.317	-.404	-.511	-.558	-.627	.750
Lower surface		.850	-.111	-.156	-.224	-.277	-.318	-.406	-.512	-.565	-.574	.850
		.926	-.111	-.148	-.213	-.256	-.293	-.340	-.465	-.509	-.354	.926
		.023	-.479	-.394	-.168	.025	.189	.428	.577	.666	.732	.023
		.072	-.322	-.190	-.066	.017	.127	.327	.482	.606	.701	.072
		.150	-.235	-.152	-.061	.022	.107	.276	.421	.540	.646	.150
		.250	-.235	-.160	-.074	-.015	.060	.212	.352	.470	.575	.250
		.350	-.226	-.169	-.093	-.029	.033	.172	.305	.424	.527	.350
		.450	-.238	-.191	-.127	-.073	-.014	.129	.258	.375	.472	.450
		.550	-.242	-.203	-.145	-.096	-.030	.107	.231	.340	.433	.550
		.650	-.248	-.213	-.157	-.107	-.040	.099	.208	.309	.395	.650
Upper surface		.750	-.232	-.192	-.141	-.088	-.020	.106	.197	.281	.358	.750
		.860	-.217	-.184	-.138	-.085	-.011	.085	.157	.233	.291	.860
		.900	-.215	-.177	-.131	-.075	-.011	.063	.117	.186	.240	.900
$M = 1.125; q = 421 \text{ lb/sq ft}$												
Upper surface		.000	.071	.277	.440	.498	.501	.362	.069	-.268	-.506	.000
		.025	.369	.284	.197	.052	-.094	-.519	-.792	-.877	-.900	.025
		.076	.231	.152	.070	-.030	-.136	-.411	-.743	-.861	-.892	.076
		.150										.150
		.250	.072	-.004	-.063	-.133	-.202	-.302	-.378	-.696	-.884	.250
		.350	.013	-.051	-.105	-.161	-.221	-.314	-.384	-.629	-.869	.350
		.450	-.049	-.109	-.158	-.215	-.267	-.351	-.421	-.633	-.871	.450
		.550	-.050	-.113	-.159	-.215	-.271	-.348	-.428	-.576	-.666	.550
		.650	-.075	-.132	-.176	-.232	-.283	-.371	-.439	-.542	-.540	.650
		.750	-.064	-.116	-.161	-.209	-.263	-.347	-.420	-.513	-.496	.750
Lower surface		.850	-.073	-.123	-.167	-.216	-.264	-.346	-.412	-.484	-.413	.850
		.926	-.078	-.129	-.163	-.213	-.257	-.304	-.389	-.417	-.198	.926
		.023	-.462	-.372	-.137	.020	.187	.407	.571	.704	.795	.023
		.072	-.274	-.156	-.047	.029	.132	.312	.479	.641	.764	.072
		.150	-.176	-.104	-.015	.044	.113	.266	.420	.579	.713	.150
		.250	-.185	-.116	-.027	.032	.086	.220	.362	.516	.646	.250
		.350	-.175	-.116	-.053	-.003	.061	.190	.325	.473	.601	.350
		.450	-.186	-.140	-.076	-.038	.021	.147	.283	.436	.552	.450
		.550	-.199	-.157	-.093	-.052	.008	.124	.260	.404	.519	.550
		.650	-.204	-.163	-.103	-.064	-.006	.115	.247	.384	.484	.650
Lower surface		.750	-.193	-.153	-.091	-.049	.005	.129	.250	.363	.457	.750
		.860	-.176	-.144	-.085	-.050	.000	.125	.221	.324	.393	.860
		.900	-.185	-.147	-.093	-.054	.000	.116	.195	.282	.347	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Concluded

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		M = 1.200; q = 436 lb/sq ft										
Upper surface	.000	.182	.344	.466	.532	.529	.423	.180	-.117	-.362	.000	
	.025	.374	.296	.199	.080	-.049	-.439	-.670	-.779	-.753	.025	
	.076	.242	.164	.077	-.005	-.101	-.353	-.615	-.742	-.723	.076	
	.150										.150	
	.250	.081	.018	-.044	-.108	-.157	-.258	-.335	-.550	-.753	.250	
	.350	.037	-.017	-.072	-.120	-.179	-.281	-.347	-.452	-.748	.350	
	.450	-.021	-.075	-.133	-.178	-.232	-.310	-.371	-.467	-.778	.450	
	.550	-.029	-.084	-.144	-.192	-.242	-.309	-.380	-.478	-.687	.550	
	.650	-.061	-.109	-.159	-.198	-.241	-.326	-.400	-.468	-.535	.650	
	.750	-.045	-.092	-.144	-.179	-.223	-.302	-.377	-.456	-.469	.750	
Lower surface	.850	-.054	-.102	-.152	-.186	-.230	-.307	-.377	-.463	-.474	.850	
	.926	-.058	-.099	-.147	-.185	-.223	-.290	-.356	-.445	-.467	.926	
	.023	-.454	-.336	-.114	.060	.185	.400	.563	.679	.782	.023	
	.072	-.244	-.105	-.035	.043	.144	.315	.469	.605	.737	.072	
	.150	-.154	-.083	-.017	.050	.123	.269	.418	.547	.687	.150	
	.250	-.154	-.092	-.030	.037	.106	.224	.360	.485	.621	.250	
	.350	-.149	-.085	-.032	.016	.071	.198	.325	.446	.577	.350	
	.450	-.166	-.114	-.063	-.015	.039	.162	.279	.407	.535	.450	
	.550	-.183	-.134	-.086	-.033	.028	.140	.249	.381	.503	.550	
	.650	-.183	-.134	-.091	-.041	.010	.118	.235	.369	.476	.650	
	.750	-.158	-.123	-.087	-.035	.017	.123	.260	.364	.458	.750	
	.860	-.140	-.100	-.059	-.012	.028	.124	.254	.340	.410	.860	
	.900	-.144	-.104	-.064	-.019	.028	.128	.241	.310	.374	.900	

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.800; q = 310 lb/sq ft											
Upper surface	.000	.206	.257	.333	.267	-.419	-1.193	-1.295	-.934	-.872	.000
	.020	.360	.276	.128	-.093	-.458	-1.188	-1.280	-.940	-.864	.020
	.073	.185	.077	-.054	-.212	-.430	-1.096	-1.209	-.971	-.857	.073
	.150	.098	.008	-.105	-.212	-.370	-.993	-1.136	-.979	-.833	.150
	.250	.030	-.048	-.142	-.233	-.349	-.711	-1.103	-.922	-.813	.250
	.350	-.019	-.088	-.168	-.245	-.340	-.497	-.993	-.875	-.794	.350
	.440	-.041	-.107	-.173	-.237	-.320	-.421	-.939	-.845	-.772	.440
	.550	-.049	-.102	-.156	-.207	-.271	-.344	-.807	-.811	-.757	.550
	.650	-.051	-.094	-.138	-.172	-.222	-.270	-.702	-.769	-.743	.650
	.750	-.039	-.075	-.103	-.127	-.160	-.192	-.586	-.731	-.723	.750
	.850	-.012	-.039	-.058	-.071	-.092	-.112	-.453	-.689	-.707	.850
	.923	.030	.009	.002	-.002	-.014	-.033	-.304	-.636	-.681	.923
Lower surface	.024	-.745	-.619	-.361	-.038	.187	.385	.471	.510	.526	.024
	.073	-.683	-.430	-.153	-.025	.108	.284	.396	.475	.525	.073
	.150	-.723	-.351	-.138	-.038	.065	.211	.317	.403	.469	.150
	.250	-.629	-.251	-.124	-.043	.037	.162	.259	.336	.395	.250
	.350	-.267	-.189	-.107	-.040	.029	.138	.219	.291	.348	.350
	.450	-.140	-.154	-.091	-.029	.029	.119	.186	.246	.293	.450
	.550	-.099	-.108	-.060	-.012	.035	.110	.162	.208	.247	.550
	.650	-.069	-.068	-.028	.012	.046	.109	.144	.167	.197	.650
	.750	-.020	-.022	.009	.041	.068	.116	.129	.130	.141	.750
	.850	.024	.018	.034	.061	.080	.112	.101	.064	.048	.850
	.900	.036	.033	.042	.064	.082	.103	.076	.000	-.018	.900
M = 0.900; q = 358 lb/sq ft											
Upper surface	.000	.220	.274	.333	.282	-.197	-1.231	-1.196	-.785	-.897	.000
	.020	.342	.252	.121	-.087	-.408	-1.265	-1.203	-.810	-.934	.020
	.073	.162	.057	-.073	-.235	-.426	-.977	-1.166	-.819	-.849	.073
	.150	.076	-.015	-.133	-.259	-.397	-.716	-1.091	-.848	-.836	.150
	.250	.009	-.077	-.181	-.290	-.417	-.643	-1.069	-.858	-.824	.250
	.350	-.042	-.121	-.210	-.338	-.422	-.631	-1.004	-.848	-.802	.350
	.440	-.066	-.138	-.221	-.313	-.476	-.638	-.896	-.821	-.780	.440
	.550	-.072	-.131	-.199	-.279	-.465	-.652	-.817	-.795	-.769	.550
	.650	-.069	-.119	-.170	-.220	-.260	-.632	-.740	-.766	-.758	.650
	.750	-.053	-.093	-.125	-.159	-.154	-.303	-.670	-.745	-.739	.750
	.850	-.023	-.046	-.069	-.086	-.085	-.108	-.610	-.714	-.726	.850
	.923	.023	.008	.000	-.006	-.005	-.022	-.515	-.683	-.701	.923
Lower surface	.024	-.805	-.621	-.417	-.075	.144	.370	.473	.534	.560	.024
	.073	-.678	-.467	-.183	-.055	.077	.267	.389	.486	.552	.073
	.150	-.647	-.356	-.182	-.067	.037	.194	.314	.417	.493	.150
	.250	-.691	-.336	-.174	-.077	.009	.143	.249	.345	.425	.250
	.350	-.482	-.268	-.143	-.069	.002	.124	.212	.303	.377	.350
	.450	-.333	-.216	-.125	-.057	.005	.104	.183	.257	.328	.450
	.550	-.205	-.151	-.084	-.028	.018	.099	.159	.221	.281	.550
	.650	-.120	-.090	-.046	-.001	.036	.099	.138	.181	.237	.650
	.750	-.048	-.032	-.001	.035	.064	.110	.119	.149	.193	.750
	.850	.006	.014	.035	.060	.080	.106	.083	.086	.114	.850
	.900	.024	.032	.048	.067	.083	.097	.050	.033	.055	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY' - Continued

(c) 40-percent-semispan station - Continued

		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.940; q = 368 \text{ lb/sq ft}$											
Upper surface	.000	.238	.280	.338	.302	-.090	-1.050	-1.130	-1.070	-.861	.000
	.020	.330	.251	.120	-.058	-.352	-1.061	-1.135	-1.030	-.891	.020
	.073	.151	.051	-.075	-.216	-.401	-.992	-1.129	-.983	-.882	.073
	.150	.065	-.028	-.142	-.243	-.379	-.610	-1.014	-.916	-.902	.150
	.250	-.006	-.094	-.199	-.300	-.395	-.586	-.970	-.852	-.893	.250
	.350	-.060	-.134	-.265	-.325	-.416	-.594	-.956	-.806	-.860	.350
	.440	-.082	-.162	-.286	-.376	-.455	-.609	-.918	-.794	-.836	.440
	.550	-.088	-.155	-.262	-.388	-.467	-.615	-.819	-.805	-.830	.550
	.650	-.086	-.131	-.189	-.392	-.473	-.627	-.758	-.796	-.819	.650
	.750	-.064	-.095	-.122	-.227	-.462	-.614	-.693	-.773	-.798	.750
	.850	-.024	-.044	-.066	-.047	-.161	-.383	-.609	-.756	-.782	.850
	.923	.028	.014	.006	.020	-.002	-.147	-.506	-.718	-.754	.923
Lower surface	.024	-.763	-.634	-.421	-.113	.124	.355	.472	.546	.580	.024
	.073	-.612	-.493	-.186	-.085	.058	.248	.384	.495	.569	.073
	.150	-.547	-.375	-.204	-.102	.014	.178	.309	.424	.512	.150
	.250	-.533	-.372	-.226	-.111	-.012	.127	.248	.354	.445	.250
	.350	-.469	-.346	-.184	-.101	-.016	.102	.209	.312	.396	.350
	.450	-.416	-.344	-.159	-.090	-.016	.080	.175	.268	.348	.450
	.550	-.372	-.270	-.094	-.051	.001	.074	.153	.235	.308	.550
	.650	-.305	-.111	-.047	-.011	.023	.075	.135	.195	.263	.650
	.750	-.115	-.028	.002	.030	.054	.081	.117	.167	.219	.750
	.850	.003	.023	.038	.063	.076	.074	.084	.108	.149	.850
	.900	.032	.040	.052	.073	.083	.061	.054	.062	.095	.900
$M = 0.980; q = 385 \text{ lb/sq ft}$											
Upper surface	.000	.260	.295	.356	.336	.026	-1.020	-1.080	-1.161	-1.197	.000
	.020	.336	.257	.144	-.022	-.288	-1.009	-1.103	-1.178	-1.181	.020
	.073	.150	.053	-.052	-.191	-.356	-.904	-1.027	-1.130	-1.161	.073
	.150	.060	-.026	-.119	-.219	-.359	-.538	-.913	-1.141	-1.120	.150
	.250	-.024	-.101	-.187	-.268	-.368	-.551	-.866	-1.136	-1.069	.250
	.350	-.077	-.172	-.236	-.310	-.392	-.540	-.851	-1.148	-1.031	.350
	.440	-.115	-.204	-.286	-.354	-.422	-.562	-.842	-1.158	-.983	.440
	.550	-.140	-.227	-.310	-.371	-.442	-.569	-.821	-1.156	-.961	.550
	.650	-.157	-.240	-.323	-.385	-.454	-.584	-.774	-1.123	-.928	.650
	.750	-.166	-.256	-.324	-.390	-.452	-.576	-.727	-.870	-.876	.750
	.850	-.128	-.222	-.308	-.371	-.435	-.554	-.669	-.802	-.854	.850
	.923	-.021	-.074	-.132	-.180	-.283	-.374	-.446	-.742	-.816	.923
Lower surface	.024	-.745	-.591	-.394	-.113	.107	.363	.494	.564	.605	.024
	.073	-.592	-.454	-.180	-.079	.052	.259	.402	.512	.598	.073
	.150	-.516	-.321	-.176	-.098	-.002	.189	.326	.444	.541	.150
	.250	-.447	-.322	-.215	-.137	-.045	.131	.265	.380	.480	.250
	.350	-.434	-.303	-.205	-.141	-.059	.104	.229	.337	.434	.350
	.450	-.418	-.319	-.232	-.169	-.065	.078	.194	.298	.387	.450
	.550	-.384	-.304	-.219	-.149	-.052	.071	.174	.266	.347	.550
	.650	-.359	-.279	-.205	-.128	-.031	.061	.152	.234	.306	.650
	.750	-.311	-.240	-.166	-.085	-.009	.061	.134	.208	.265	.750
	.850	-.220	-.165	-.088	-.007	.007	.036	.094	.164	.200	.850
	.900	-.139	-.089	-.032	.016	.006	.017	.065	.125	.144	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 1.030; q = 400 \text{ lb/sq ft}$												
Upper surface		.000	.318	.352	.398	.389	.118	-.834	-.975	-1.054	-1.094	.000
		.020	.381	.308	.194	.046	-.205	-.832	-.993	-1.068	-1.102	.020
		.073	.202	.113	-.001	-.125	-.282	-.760	-.940	-1.024	-1.089	.073
		.150	.116	.033	-.066	-.156	-.279	-.453	-.815	-1.032	-1.095	.150
		.250	.029	-.033	-.127	-.204	-.295	-.457	-.741	-1.042	-1.115	.250
		.350	-.038	-.104	-.175	-.242	-.323	-.453	-.702	-1.046	-1.118	.350
		.440	-.067	-.139	-.220	-.282	-.350	-.471	-.667	-1.045	-1.112	.440
		.550	-.102	-.161	-.240	-.303	-.369	-.482	-.640	-1.057	-1.106	.550
		.650	-.111	-.176	-.254	-.316	-.381	-.496	-.629	-1.058	-1.079	.650
		.750	-.132	-.188	-.261	-.324	-.381	-.494	-.619	-1.031	-1.033	.750
Lower surface		.850	-.119	-.174	-.253	-.308	-.366	-.474	-.602	-.936	-.746	.850
		.923	-.086	-.121	-.181	-.230	-.292	-.346	-.437	-.876	-.775	.923
		.024	-.637	-.537	-.352	-.063	.152	.403	.537	.613	.654	.024
		.073	-.477	-.391	-.139	-.027	.103	.304	.448	.562	.647	.073
		.150	-.400	-.264	-.121	-.039	.052	.229	.375	.497	.589	.150
		.250	-.332	-.253	-.149	-.080	.004	.178	.314	.428	.527	.250
		.350	-.330	-.239	-.149	-.084	-.006	.152	.279	.392	.486	.350
		.450	-.326	-.252	-.175	-.113	-.027	.126	.246	.352	.442	.450
		.550	-.306	-.240	-.168	-.100	-.018	.119	.223	.320	.404	.550
		.650	-.287	-.221	-.152	-.085	-.010	.115	.202	.291	.366	.650
Upper surface		.750	-.242	-.183	-.118	-.051	.020	.116	.187	.263	.330	.750
		.850	-.192	-.141	-.079	-.021	.035	.094	.148	.214	.269	.850
		.900	-.148	-.104	-.052	-.005	.029	.068	.112	.176	.224	.900
$M = 1.125; q = 421 \text{ lb/sq ft}$												
Upper surface		.000	.358	.379	.434	.429	.230	-.665	-.894	-.896	-.914	.000
		.020	.389	.308	.222	.097	-.128	-.681	-.885	-.911	-.920	.020
		.073	.212	.122	.035	-.079	-.221	-.630	-.867	-.889	-.916	.073
		.150	.133	.055	-.028	-.115	-.228	-.524	-.821	-.864	-.915	.150
		.250	.058	-.012	-.081	-.162	-.253	-.385	-.759	-.871	-.922	.250
		.350	.000	-.064	-.121	-.197	-.274	-.405	-.662	-.865	-.915	.350
		.440	-.040	-.108	-.161	-.226	-.292	-.414	-.522	-.858	-.914	.440
		.550	-.066	-.132	-.187	-.246	-.309	-.406	-.482	-.873	-.913	.550
		.650	-.083	-.149	-.201	-.267	-.329	-.427	-.492	-.866	-.889	.650
		.750	-.099	-.160	-.210	-.274	-.334	-.434	-.495	-.843	-.841	.750
Lower surface		.850	-.093	-.155	-.201	-.262	-.321	-.409	-.480	-.748	-.634	.850
		.923	-.063	-.125	-.173	-.231	-.283	-.343	-.405	-.669	-.615	.923
		.024	-.613	-.545	-.331	-.082	.151	.398	.543	.656	.726	.024
		.073	-.430	-.355	-.119	-.019	.117	.299	.459	.604	.716	.073
		.150	-.349	-.220	-.085	-.015	.085	.234	.385	.546	.666	.150
		.250	-.278	-.207	-.092	-.035	.030	.178	.333	.485	.608	.250
		.350	-.248	-.187	-.092	-.048	.019	.164	.307	.458	.573	.350
		.450	-.261	-.193	-.117	-.070	-.008	.141	.280	.424	.532	.450
		.550	-.259	-.193	-.118	-.068	-.003	.143	.268	.402	.498	.550
		.650	-.247	-.181	-.106	-.056	.010	.146	.256	.371	.463	.650
		.750	-.205	-.150	-.073	-.023	.037	.162	.252	.352	.429	.750
		.850	-.161	-.107	-.041	.001	.060	.158	.223	.312	.373	.850
		.900	-.140	-.090	-.029	.012	.065	.141	.195	.275	.328	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station - Concluded

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.200; q = 436 lb/sq ft											
Upper surface	.000	.405	.432	.481	.467	.304	-.479	-.760	-.792	-.759	.000
	.020	.420	.351	.264	.124	-.056	-.541	-.747	-.793	-.746	.020
	.073	.242	.165	.073	-.040	-.168	-.482	-.723	-.828	-.762	.073
	.150	.157	.086	.003	-.083	-.180	-.430	-.691	-.782	-.766	.150
	.250	.083	.017	-.051	-.116	-.195	-.366	-.649	-.724	-.763	.250
	.350	.031	-.032	-.098	-.150	-.222	-.340	-.630	-.681	-.763	.350
	.440	-.012	-.070	-.131	-.180	-.248	-.364	-.587	-.637	-.770	.440
	.550	-.045	-.101	-.153	-.207	-.255	-.364	-.422	-.609	-.775	.550
	.650	-.069	-.122	-.186	-.230	-.281	-.367	-.418	-.614	-.769	.650
	.750	-.085	-.136	-.188	-.239	-.293	-.372	-.437	-.599	-.780	.750
	.850	-.082	-.128	-.183	-.226	-.272	-.359	-.436	-.588	-.765	.850
	.923	-.065	-.111	-.158	-.196	-.239	-.318	-.397	-.467	-.731	.923
Lower surface	.024	-.581	-.521	-.295	-.047	.160	.422	.553	.647	.721	.024
	.073	-.399	-.318	-.108	.019	.140	.327	.457	.582	.697	.073
	.150	-.301	-.162	-.061	.023	.105	.260	.383	.518	.640	.150
	.250	-.224	-.154	-.077	-.001	.071	.189	.322	.459	.585	.250
	.350	-.203	-.144	-.075	-.016	.046	.172	.296	.433	.553	.350
	.450	-.223	-.157	-.096	-.043	.014	.133	.267	.403	.514	.450
	.550	-.233	-.171	-.111	-.053	.008	.127	.271	.386	.488	.550
	.650	-.212	-.158	-.110	-.051	.003	.119	.273	.370	.460	.650
	.750	-.177	-.116	-.073	-.024	.022	.151	.278	.360	.433	.750
	.850	-.142	-.084	-.032	.017	.067	.187	.267	.326	.389	.850
	.900	-.130	-.074	-.027	.026	.074	.181	.245	.298	.352	.900

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 310 \text{ lb/sq ft}$												
Upper surface		.000	.116	.336	.476	.365	-.323	-.981	-.781	-.821	-.787	.000
		.025	.392	.313	.149	-.112	-.676	-.949	-.773	-.711	-.725	.025
		.075	.260	.164	.032	-.163	-.406	-.929	-.744	-.686	-.689	.075
		.150	.153	.060	-.060	-.205	-.371	-.909	-.768	-.686	-.699	.150
		.250	.093	.010	-.091	-.187	-.323	-.896	-.756	-.669	-.687	.250
		.350	.047	-.030	-.109	-.194	-.303	-.878	-.735	-.649	-.675	.350
		.450										.450
		.550	-.011	-.061	-.128	-.179	-.248	-.717	-.672	-.624	-.664	.550
		.650	-.027	-.074	-.120	-.165	-.212	-.575	-.626	-.605	-.645	.650
		.750	-.024	-.059	-.095	-.123	-.161	-.377	-.595	-.586	-.630	.750
		.850	-.004	-.033	-.056	-.070	-.095	-.194	-.541	-.568	-.620	.850
		.900	.015	-.013	-.032	-.040	-.055	-.120	-.533	-.561	-.607	.900
		.925										.925
		.040	-.642	-.553	-.255	-.006	.196	.366	.436	.469	.484	.040
Lower surface		.091	-.604	-.518	-.169	-.022	.130	.284	.367	.417	.453	.091
		.150	-.574	-.519	-.128	-.029	.105	.238	.313	.372	.410	.150
		.250	-.607	-.482	-.100	-.010	.082	.192	.257	.308	.346	.250
		.360	-.618	-.281	-.080	-.003	.070	.164	.208	.250	.292	.360
		.450	-.555	-.117	-.053	.006	.065	.143	.178	.207	.237	.450
		.550	-.419	-.043	-.032	.020	.068	.128	.143	.161	.183	.550
		.650	-.210	-.006	.001	.042	.078	.128	.118	.118	.134	.650
		.800	.057	.037	.039	.069	.091	.114	.054	.028	.033	.800
		.874	.100	.049	.043	.069	.086	.096	-.009	-.047	-.047	.874
$M = 0.900; q = 358 \text{ lb/sq ft}$												
Upper surface		.000	.124	.342	.462	.354	-.174	-1.277	-.871	-.846	-.837	.000
		.025	.381	.295	.148	-.155	-.824	-1.400	-.800	-.764	-.756	.025
		.075	.249	.146	.009	-.211	-.460	-1.326	-.726	-.708	-.714	.075
		.150	.138	.040	-.088	-.272	-.473	-1.251	-.726	-.710	-.723	.150
		.250	.080	-.009	-.118	-.256	-.465	-.937	-.714	-.697	-.715	.250
		.350	.033	-.049	-.138	-.254	-.482	-.747	-.703	-.686	-.708	.350
		.450										.450
		.550	-.022	-.082	-.148	-.223	-.240	-.539	-.672	-.667	-.693	.550
		.650	-.039	-.093	-.143	-.198	-.240	-.363	-.657	-.649	-.680	.650
		.750	-.033	-.070	-.115	-.149	-.173	-.248	-.631	-.637	-.670	.750
		.850	-.009	-.040	-.068	-.088	-.098	-.155	-.596	-.622	-.665	.850
		.900	.013	-.018	-.037	-.050	-.055	-.108	-.577	-.610	-.656	.900
		.925										.925
		.040	-.773	-.590	-.351	-.031	.161	.339	.422	.472	.504	.040
Lower surface		.091	-.730	-.536	-.208	-.038	.102	.262	.356	.422	.474	.091
		.150	-.706	-.539	-.169	-.030	.080	.220	.302	.378	.434	.150
		.250	-.713	-.544	-.131	-.019	.066	.173	.247	.313	.371	.250
		.360	-.713	-.389	-.098	-.019	.056	.147	.201	.260	.320	.360
		.450	-.684	-.204	-.069	-.003	.055	.131	.167	.221	.266	.450
		.550	-.545	-.078	-.038	.016	.062	.122	.134	.177	.218	.550
		.650	-.256	-.020	-.005	.040	.076	.120	.103	.134	.174	.650
		.800	.114	.037	.040	.073	.096	.114	.042	.059	.084	.800
		.874	.138	.050	.052	.072	.089	.093	-.016	-.006	.013	.874

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 368 lb/sq ft											
Upper surface	.000	.151	.327	.443	.362	-.049	-.989	-1.079	-.904	-.950	.000
	.025	.355	.282	.108	-.116	-.660	-1.100	-1.070	-.834	-.797	.025
	.075	.227	.126	-.022	-.210	-.412	-1.116	-.778	-.735	-.757	.075
	.150	.118	.023	-.127	-.295	-.440	-1.069	-.809	-.744	-.772	.150
	.250	.063	-.018	-.155	-.320	-.439	-.914	-.785	-.733	-.768	.250
	.350	.013	-.058	-.170	-.342	-.477	-.627	-.738	-.724	-.755	.350
	.450										.450
	.550	-.034	-.081	-.157	-.333	-.488	-.666	-.691	-.704	-.739	.550
	.650	-.047	-.091	-.146	-.155	-.506	-.642	-.670	-.689	-.723	.650
	.750	-.035	-.072	-.113	-.113	-.222	-.546	-.649	-.680	-.712	.750
	.850	-.014	-.039	-.065	-.072	-.054	-.404	-.605	-.665	-.709	.850
	.900	.006	-.017	-.033	-.038	-.013	-.365	-.602	-.654	-.697	.900
	.925										.925
Lower surface	.040	-.752	-.660	-.403	-.088	.128	.313	.418	.477	.520	.040
	.091	-.681	-.580	-.249	-.096	.070	.231	.346	.430	.495	.091
	.150	-.643	-.559	-.186	-.088	.049	.186	.289	.385	.453	.150
	.250	-.684	-.528	-.150	-.055	.042	.149	.242	.323	.393	.250
	.360	-.681	-.456	-.107	-.037	.036	.122	.197	.270	.339	.360
	.450	-.593	-.323	-.076	-.022	.039	.103	.166	.229	.294	.450
	.550	-.472	-.204	-.039	.005	.049	.090	.134	.190	.247	.550
	.650	-.323	-.097	-.002	.041	.070	.093	.110	.147	.201	.650
	.800	-.054	.002	.045	.075	.097	.081	.059	.083	.120	.800
	.874	.033	.031	.053	.083	.094	.055	.007	.023	.048	.874
M = 0.980; q = 385 lb/sq ft											
Upper surface	.000	.192	.343	.428	.381	.094	-.856	-1.129	-1.102	-.831	.000
	.025	.336	.246	.115	-.070	-.469	-1.060	-1.144	-1.052	-.824	.025
	.075	.193	.088	-.025	-.177	-.383	-1.039	-1.030	-.896	-.776	.075
	.150	.079	-.023	-.149	-.268	-.427	-1.004	-1.054	-.939	-.806	.150
	.250	.018	-.079	-.199	-.296	-.403	-.930	-1.011	-.912	-.808	.250
	.350	-.041	-.150	-.233	-.343	-.431	-.827	-.963	-.880	-.803	.350
	.450										.450
	.550	-.114	-.202	-.307	-.378	-.483	-.597	-.851	-.815	-.783	.550
	.650	-.138	-.247	-.340	-.409	-.490	-.643	-.833	-.778	-.774	.650
	.750	-.064	-.246	-.361	-.450	-.524	-.665	-.786	-.755	-.778	.750
	.850	-.041	-.028	-.184	-.380	-.515	-.666	-.730	-.743	-.773	.850
	.900	-.021	.007	-.039	-.157	-.376	-.630	-.709	-.735	-.773	.900
	.925										.925
Lower surface	.040	-.728	-.615	-.441	-.159	.063	.303	.429	.504	.551	.040
	.091	-.658	-.537	-.298	-.174	.009	.222	.358	.450	.526	.091
	.150	-.638	-.522	-.247	-.165	-.005	.182	.304	.406	.485	.150
	.250	-.681	-.492	-.254	-.157	-.016	.134	.256	.350	.429	.250
	.360	-.719	-.488	-.277	-.178	-.020	.102	.211	.301	.376	.360
	.450	-.697	-.458	-.253	-.156	-.027	.079	.181	.265	.331	.450
	.550	-.627	-.392	-.221	-.108	-.018	.063	.150	.225	.285	.550
	.650	-.508	-.294	-.154	-.007	.007	.052	.127	.188	.242	.650
	.800	-.233	-.095	.020	.053	.034	.034	.084	.123	.166	.800
	.874	-.130	-.020	.055	.064	.029	.004	.038	.069	.102	.874

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - Continued

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 400 lb/sq ft											
Upper surface	.000	.262	.394	.468	.435	.168	-.665	-1.070	-1.030	-1.020	.000
	.025	.370	.301	.183	-.009	-.366	-.885	-1.095	-.997	-.996	.025
	.075	.234	.150	.036	-.112	-.308	-.873	-1.089	-.973	-.972	.075
	.150	.120	.039	-.080	-.197	-.351	-.841	-1.078	-.984	-.966	.150
	.250	.053	-.018	-.134	-.227	-.339	-.782	-1.046	-.944	-.927	.250
	.350	-.013	-.077	-.176	-.269	-.363	-.718	-1.028	-.912	-.888	.350
	.450										.450
	.550	-.081	-.146	-.230	-.308	-.409	-.509	-.935	-.856	-.839	.550
	.650	-.114	-.182	-.264	-.332	-.423	-.550	-.922	-.828	-.833	.650
	.750	-.139	-.212	-.293	-.376	-.442	-.576	-.871	-.794	-.816	.750
	.850	-.139	-.202	-.297	-.369	-.451	-.581	-.722	-.766	-.787	.850
	.900	-.097	-.163	-.263	-.348	-.432	-.574	-.610	-.752	-.779	.900
	.925										.925
Lower surface	.040	-.616	-.548	-.389	-.100	.102	.339	.467	.550	.596	.040
	.091	-.533	-.469	-.256	-.113	.046	.262	.398	.503	.573	.091
	.150	-.503	-.450	-.201	-.098	.029	.220	.347	.460	.535	.150
	.250	-.542	-.415	-.190	-.092	.007	.178	.296	.403	.482	.250
	.360	-.583	-.409	-.210	-.125	-.000	.149	.255	.355	.433	.360
	.450	-.564	-.394	-.196	-.107	.002	.129	.225	.322	.392	.450
	.550	-.520	-.342	-.175	-.091	.009	.113	.194	.287	.348	.550
	.650	-.447	-.269	-.137	-.054	.024	.107	.172	.253	.310	.650
	.800	-.253	-.157	-.061	.007	.044	.086	.130	.196	.236	.800
	.874	-.169	-.099	-.026	.020	.036	.059	.089	.145	.175	.874
M = 1.125; q = 421 lb/sq ft											
Upper surface	.000	.323	.438	.499	.481	.253	-.405	-.822	-.919	-.889	.000
	.025	.398	.332	.231	.059	-.241	-.730	-.891	-.865	-.851	.025
	.075	.260	.183	.088	-.047	-.226	-.699	-.873	-.769	-.784	.075
	.150	.149	.066	-.022	-.133	-.282	-.683	-.865	-.813	-.816	.150
	.250	.087	.001	-.066	-.163	-.272	-.643	-.841	-.801	-.788	.250
	.350	.027	-.052	-.119	-.202	-.299	-.612	-.829	-.782	-.758	.350
	.450										.450
	.550	-.044	-.109	-.179	-.261	-.338	-.412	-.755	-.736	-.723	.550
	.650	-.078	-.145	-.199	-.283	-.366	-.454	-.783	-.706	-.689	.650
	.750	-.101	-.176	-.244	-.308	-.388	-.485	-.763	-.668	-.655	.750
	.850	-.106	-.184	-.245	-.320	-.396	-.495	-.707	-.628	-.639	.850
	.900	-.099	-.180	-.244	-.316	-.394	-.499	-.689	-.606	-.620	.900
	.925										.925
Lower surface	.040	-.558	-.476	-.348	-.063	.131	.341	.496	.614	.682	.040
	.091	-.452	-.403	-.199	-.075	.070	.264	.427	.571	.657	.091
	.150	-.422	-.365	-.137	-.069	.051	.228	.381	.534	.620	.150
	.250	-.436	-.312	-.132	-.055	.034	.187	.338	.479	.573	.250
	.360	-.429	-.293	-.159	-.092	-.006	.175	.304	.437	.527	.360
	.450	-.421	-.295	-.146	-.084	-.002	.159	.277	.406	.490	.450
	.550	-.414	-.276	-.138	-.087	.002	.158	.254	.378	.450	.550
	.650	-.394	-.233	-.109	-.049	.026	.162	.239	.343	.414	.650
	.800	-.287	-.161	-.056	-.003	.067	.154	.202	.294	.346	.800
	.874	-.221	-.123	-.027	.017	.077	.133	.170	.249	.290	.874

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - (concluded)

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		M = 1.200; q = 436 lb/sq ft										
Upper surface		.000	.340	.438	.482	.490	.301	-.204	-.652	-.835	-.783	.000
		.025	.408	.341	.240	.090	-.146	-.586	-.758	-.791	-.709	.025
		.075	.273	.196	.105	-.016	-.167	-.557	-.726	-.788	-.731	.075
		.150	.157	.084	-.002	-.104	-.236	-.555	-.727	-.818	-.742	.150
		.250	.093	.026	-.050	-.127	-.228	-.529	-.708	-.814	-.744	.250
		.350	.043	-.027	-.091	-.165	-.252	-.514	-.705	-.815	-.753	.350
		.450										.450
		.550	-.013	-.081	-.151	-.215	-.275	-.458	-.675	-.790	-.738	.550
		.650	-.042	-.101	-.172	-.239	-.310	-.374	-.671	-.800	-.766	.650
		.750	-.075	-.143	-.201	-.270	-.336	-.419	-.673	-.748	-.741	.750
		.850	-.091	-.149	-.226	-.284	-.348	-.430	-.652	-.663	-.729	.850
		.900	-.085	-.155	-.219	-.287	-.353	-.438	-.664	-.619	-.741	.900
		.925										.925
Lower surface		.040	-.575	-.597	-.365	-.066	.132	.337	.486	.597	.671	.040
		.091	-.454	-.451	-.222	-.062	.074	.261	.422	.548	.641	.091
		.150	-.397	-.352	-.123	-.053	.060	.223	.382	.513	.609	.150
		.250	-.369	-.253	-.123	-.033	.048	.187	.350	.464	.563	.250
		.360	-.337	-.211	-.133	-.070	-.002	.157	.327	.427	.520	.360
		.450	-.301	-.196	-.120	-.052	.020	.185	.309	.399	.485	.450
		.550	-.286	-.185	-.108	-.039	.031	.176	.298	.374	.450	.550
		.650	-.283	-.153	-.076	-.007	.062	.191	.290	.347	.419	.650
		.800	-.230	-.103	-.031	.037	.103	.208	.264	.306	.361	.800
		.874	-.191	-.074	-.001	.063	.123	.195	.233	.268	.314	.874

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(e) 80-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$c = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.940; q = 368 \text{ lb/sq ft}$												
Upper surface	.022	.411	.361	.243	-.079	-.685	-1.231	-.620	-.641	-.687	.022	
	.076	.304	.228	.093	-.174	-.598	-1.131	-.618	-.627	-.677	.076	
	.150	.219	.143	.012	-.210	-.464	-1.067	-.607	-.618	-.667	.150	
	.250	.144	.072	-.039	-.204	-.456	-1.046	-.573	-.605	-.659	.250	
	.370	.082	.016	-.087	-.206	-.492	-.997	-.564	-.598	-.652	.370	
	.450	.041	-.015	-.115	-.220	-.528	-.903	-.551	-.584	-.643	.450	
	.550	.006	-.044	-.125	-.216	-.549	-.765	-.527	-.582	-.636	.550	
	.600										.600	
	.650	-.024	-.065	-.137	-.198	-.243	-.584	-.516	-.579	-.632	.650	
	.750	-.040	-.059	-.114	-.161	-.100	-.482	-.503	-.567	-.622	.750	
.850	-.070	-.047	-.089	-.108	-.061	-.432	-.496	-.563	-.615	.850		
.900										.900		
Lower surface	.078	-.529	-.504	-.524	-.071	.107	.247	.313	.371	.415	.078	
	.150	-.490	-.491	-.390	-.064	.059	.177	.240	.308	.373	.150	
	.250	-.465	-.488	-.228	-.020	.079	.159	.205	.264	.321	.250	
	.360	-.443	-.511	-.110	-.009	.061	.127	.151	.207	.263	.360	
	.450										.450	
	.560	-.492	-.530	-.023	.013	.070	.098	.079	.120	.170	.560	
	.610	-.517	-.532	-.011	.026	.071	.091	.062	.099	.143	.610	
	.700	-.485	-.500	.025	.047	.091	.096	.050	.077	.114	.700	
	.800	-.447	-.404	.053	.073	.107	.085	.014	.036	.064	.800	
	$M = 0.980; q = 385 \text{ lb/sq ft}$											
Upper surface	.022	.367	.276	.175	.008	-.372	-1.140	-.978	-.650	-.750	.022	
	.076	.255	.134	.018	-.136	-.407	-1.040	-.836	-.659	-.742	.076	
	.150	.170	.047	-.073	-.208	-.422	-.999	-.837	-.668	-.743	.150	
	.250	.098	-.034	-.137	-.254	-.407	-.970	-.816	-.671	-.744	.250	
	.370	.040	-.105	-.212	-.310	-.441	-.952	-.793	-.675	-.741	.370	
	.450	.007	-.146	-.268	-.351	-.480	-.927	-.765	-.671	-.729	.450	
	.550	-.016	-.075	-.314	-.388	-.529	-.940	-.747	-.682	-.736	.550	
	.600										.600	
	.650	-.035	-.057	-.342	-.422	-.551	-.905	-.730	-.687	-.728	.650	
	.750	-.036	-.050	-.083	-.442	-.540	-.891	-.706	-.684	-.719	.750	
.850	-.054	-.037	.001	-.255	-.520	-.889	-.686	-.677	-.711	.850		
.900										.900		
Lower surface	.078	-.693	-.729	-.694	-.337	.009	.203	.327	.398	.441	.078	
	.150	-.637	-.715	-.606	-.193	-.028	.132	.256	.337	.403	.150	
	.250	-.592	-.712	-.485	-.065	.006	.111	.220	.294	.351	.250	
	.360	-.562	-.694	-.314	-.061	-.010	.069	.171	.243	.298	.360	
	.450										.450	
	.560	-.511	-.595	-.038	-.008	.008	.038	.104	.159	.207	.560	
	.610	-.521	-.563	.005	.009	.011	.028	.088	.137	.186	.610	
	.700	-.545	-.455	.050	.037	.035	.035	.077	.119	.157	.700	
	.800	-.552	-.200	.092	.081	.052	.023	.047	.080	.110	.800	

TABLE III.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(e) 80-percent-semispan station - Concluded

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		$M = 1.200; q = 436 \text{ lb/sq ft}$										
Upper surface	.022	.416	.363	.287	.164	-.035	-.590	-.799	-.818	-.734	.022	
	.076	.309	.239	.154	.035	-.138	-.521	-.739	-.799	-.707	.076	
	.150	.226	.156	.073	-.033	-.199	-.512	-.714	-.793	-.696	.150	
	.250	.157	.092	.018	-.073	-.194	-.508	-.703	-.801	-.702	.250	
	.370	.094	.027	-.038	-.114	-.222	-.516	-.695	-.792	-.692	.370	
	.450	.043	-.014	-.087	-.152	-.252	-.516	-.673	-.761	-.660	.450	
	.550	-.001	-.060	-.128	-.203	-.287	-.550	-.673	-.779	-.672	.550	
	.600										.600	
	.650	-.040	-.103	-.167	-.234	-.312	-.543	-.661	-.745	-.648	.650	
	.750	-.072	-.136	-.196	-.257	-.332	-.513	-.654	-.710	-.630	.750	
Lower surface	.850	-.097	-.157	-.228	-.280	-.351	-.507	-.659	-.670	-.597	.850	
	.900										.900	
	.078	-.694	-.686	-.521	-.357	.001	.263	.417	.503	.574	.078	
	.150	-.665	-.663	-.441	-.130	-.008	.198	.358	.452	.540	.150	
	.250	-.626	-.576	-.266	-.104	.000	.202	.339	.417	.502	.250	
	.360	-.590	-.418	-.238	-.115	-.008	.178	.304	.380	.458	.360	
	.450										.450	
	.560	-.445	-.279	-.189	-.083	.018	.176	.266	.321	.388	.560	
	.610	-.382	-.258	-.173	-.067	.029	.184	.260	.308	.372	.610	
	.700	-.297	-.219	-.131	-.031	.074	.204	.259	.300	.356	.700	
.800	-.241	-.167	-.054	.050	.134	.213	.247	.277	.324	.800		

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY

(a) 12-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 627 \text{ lb/sq ft}$												
Upper surface	.000	.183	.408	.514	.529	.498	.249	-.087	-.360	-.607	.000	
	.032	.309	.203	.089	-.031	-.163	-.474	-.895	-1.644	-1.590	.032	
	.078	.195	.109	.017	-.070	-.167	-.366	-.573	-.813	-1.454	.078	
	.150	.093	.015	-.060	-.143	-.226	-.415	-.615	-.767	-1.080	.150	
	.250	.015	-.056	-.127	-.198	-.276	-.447	-.619	-.602	-.828	.250	
	.350	-.003	-.065	-.129	-.192	-.262	-.413	-.552	-.582	-.733	.350	
	.450	-.048	-.107	-.161	-.223	-.287	-.429	-.511	-.612	-.663	.450	
	.550	-.085	-.138	-.191	-.247	-.307	-.436	-.460	-.607	-.648	.550	
	.650	-.063	-.108	-.153	-.197	-.244	-.331	-.391	-.529	-.579	.650	
	.760	-.050	-.089	-.123	-.159	-.192	-.247	-.343	-.464	-.538	.760	
	.840	-.057	-.081	-.106	-.128	-.155	-.188	-.269	-.403	-.545	.840	
	.926	-.033	-.053	-.063	-.079	-.092	-.110	-.168	-.305	-.508	.926	
Lower surface	.035	-.381	-.243	-.100	.028	.141	.358	.543	.685	.809	.035	
	.082										.082	
	.150	-.241	-.147	-.066	.007	.079	.227	.368	.478	.577	.150	
	.250										.250	
	.350	-.229	-.153	-.086	-.028	.027	.147	.258	.349	.436	.350	
	.450	-.242	-.174	-.113	-.060	-.008	.102	.203	.284	.366	.450	
	.550	-.227	-.170	-.113	-.067	-.021	.080	.168	.239	.311	.550	
	.650	-.207	-.156	-.106	-.066	-.026	.061	.135	.194	.258	.650	
	.750	-.138	-.098	-.061	-.030	.002	.074	.132	.172	.222	.750	
	.850	-.089	-.061	-.032	-.009	.016	.073	.111	.136	.164	.850	
	.900	-.069	-.047	-.025	-.007	.012	.059	.084	.095	.110	.900	
$M = 0.900; q = 713 \text{ lb/sq ft}$												
Upper surface	.000	.310	.471	.549	.560	.541	.380	.129	-.093	-.311	.000	
	.032	.318	.213	.111	-.003	-.115	-.386	-.786	-1.338	-1.500	.032	
	.078	.207	.119	.039	-.044	-.124	-.272	-.473	-.708	-1.464	.078	
	.150	.097	.020	-.053	-.129	-.200	-.359	-.503	-.623	-.675	.150	
	.250	.011	-.063	-.133	-.207	-.280	-.408	-.539	-.637	-.706	.250	
	.350	-.010	-.076	-.140	-.205	-.264	-.399	-.530	-.622	-.685	.350	
	.450	-.062	-.127	-.189	-.256	-.315	-.433	-.552	-.671	-.696	.450	
	.550	-.114	-.179	-.250	-.332	-.388	-.498	-.618	-.653	-.688	.550	
	.650	-.086	-.140	-.196	-.273	-.381	-.488	-.598	-.650	-.611	.650	
	.760	-.074	-.118	-.163	-.213	-.316	-.496	-.506	-.554	-.584	.760	
	.840	-.079	-.109	-.138	-.170	-.191	-.490	-.397	-.599	-.606	.840	
	.926	-.050	-.067	-.082	-.095	-.095	-.182	-.228	-.516	-.561	.926	
Lower surface	.035	-.342	-.217	-.087	.039	.148	.361	.553	.704	.837	.035	
	.082										.082	
	.150	-.230	-.147	-.069	.005	.079	.230	.376	.495	.606	.150	
	.250										.250	
	.350	-.245	-.172	-.105	-.040	.021	.146	.263	.366	.463	.350	
	.450	-.278	-.211	-.143	-.081	-.023	.096	.203	.299	.394	.450	
	.550	-.323	-.235	-.157	-.096	-.040	.070	.165	.250	.341	.550	
	.650	-.323	-.213	-.145	-.093	-.045	.051	.130	.205	.289	.650	
	.750	-.193	-.135	-.088	-.049	-.010	.067	.126	.186	.255	.750	
	.850	-.113	-.083	-.051	-.022	.008	.067	.103	.144	.204	.850	
	.900	-.084	-.062	-.038	-.017	.008	.055	.074	.100	.150	.900	

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Continued

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 743 lb/sq ft											
Upper surface	.000	.361	.503	.563	.578	.562	.428	.206	-.008	-.218	.000
	.032	.330	.226	.124	.018	-.087	-.342	-.704	-1.221	-1.421	.032
	.078	.218	.131	.051	-.025	-.096	-.227	-.424	-.645	-1.356	.078
	.150	.105	.027	-.044	-.115	-.174	-.330	-.447	-.560	-.648	.150
	.250	.014	-.063	-.132	-.202	-.250	-.371	-.484	-.580	-.637	.250
	.350	-.010	-.078	-.138	-.197	-.261	-.380	-.488	-.585	-.579	.350
	.450	-.069	-.136	-.194	-.248	-.299	-.409	-.510	-.604	-.678	.450
	.550	-.135	-.218	-.276	-.326	-.370	-.473	-.574	-.621	-.670	.550
	.650	-.104	-.174	-.266	-.325	-.364	-.477	-.573	-.645	-.667	.650
	.760	-.094	-.155	-.237	-.324	-.374	-.482	-.572	-.638	-.639	.760
	.840	-.096	-.138	-.175	-.342	-.405	-.533	-.568	-.563	-.665	.840
	.926	-.063	-.079	-.087	-.170	-.323	-.509	-.440	-.548	-.626	.926
Lower surface	.035	-.304	-.197	-.075	.045	.157	.366	.558	.716	.853	.035
	.082										.082
	.150	-.204	-.136	-.065	.005	.083	.234	.382	.512	.625	.150
	.250										.250
	.350	-.247	-.174	-.111	-.050	.018	.144	.268	.381	.485	.350
	.450	-.267	-.205	-.157	-.100	-.032	.089	.206	.314	.416	.450
	.550	-.316	-.267	-.202	-.130	-.059	.058	.166	.266	.364	.550
	.650	-.347	-.295	-.203	-.126	-.065	.034	.130	.222	.312	.650
	.750	-.327	-.254	-.116	-.071	-.028	.047	.125	.201	.281	.750
	.850	-.293	-.126	-.062	-.038	-.010	.040	.101	.163	.233	.850
	.900	-.212	-.069	-.044	-.029	-.012	.019	.067	.121	.183	.900
M = 0.980; q = 771 lb/sq ft											
Upper surface	.000	.417	.538	.599	.605	.592	.479	.269			.000
	.032	.348	.253	.159	.056	-.046	-.291	-.624			.032
	.078	.238	.159	.087	.016	-.051	-.190	-.379			.078
	.150	.126	.052	-.010	-.075	-.139	-.272	-.388			.150
	.250	.028	-.043	-.106	-.160	-.215	-.323	-.421			.250
	.350	.004	-.056	-.113	-.175	-.226	-.332	-.431			.350
	.450	-.060	-.115	-.162	-.215	-.268	-.365	-.454			.450
	.550	-.150	-.201	-.240	-.290	-.338	-.427	-.517			.550
	.650	-.133	-.194	-.245	-.293	-.343	-.433	-.522			.650
	.760	-.130	-.202	-.256	-.307	-.355	-.444	-.535			.760
	.840	-.177	-.247	-.298	-.350	-.402	-.496	-.580			.840
	.926	-.179	-.239	-.295	-.342	-.385	-.487	-.574			.926
Lower surface	.035	-.254	-.153	-.037	.074	.177	.383	.577			.035
	.082										.082
	.150	-.158	-.103	-.035	.030	.101	.251	.402			.150
	.250										.250
	.350	-.224	-.155	-.091	-.032	.027	.157	.287			.350
	.450	-.243	-.181	-.124	-.083	-.030	.097	.224			.450
	.550	-.295	-.239	-.183	-.137	-.079	.060	.182			.550
	.650	-.327	-.277	-.223	-.173	-.105	.031	.144			.650
	.750	-.316	-.256	-.207	-.148	-.073	.041	.138			.750
	.850	-.306	-.244	-.190	-.136	-.060	.031	.114			.850
	.900	-.316	-.258	-.203	-.147	-.069	.005	.081			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 803 lb/sq ft												
Upper surface		.000	.481	.585	.637	.645	.637	.543	.353			.000
		.032	.401	.298	.202	.106	.012	-.211	-.517			.032
		.078	.293	.209	.135	.070	.009	-.121	-.300			.078
		.150	.182	.105	.040	-.018	-.082	-.189	-.298			.150
		.250	.087	.010	-.058	-.104	-.148	-.244	-.336			.250
		.350	.065	.002	-.063	-.120	-.164	-.253	-.348			.350
		.450	.003	-.052	-.112	-.161	-.202	-.285	-.374			.450
		.550	-.083	-.134	-.181	-.228	-.267	-.346	-.435			.550
		.650	-.076	-.132	-.187	-.235	-.274	-.356	-.441			.650
		.760	-.079	-.139	-.199	-.247	-.287	-.368	-.452			.760
		.840	-.128	-.189	-.245	-.293	-.335	-.420	-.498			.840
		.926	-.129	-.182	-.238	-.281	-.317	-.411	-.495			.926
Lower surface		.035	-.177	-.096	.012	.116	.219	.430	.619			.035
		.082										.082
		.150	-.088	-.043	.017	.076	.147	.301	.448			.150
		.250										.250
		.350	-.153	-.104	-.044	.016	.080	.205	.335			.350
		.450	-.170	-.127	-.075	-.024	.027	.146	.272			.450
		.550	-.221	-.180	-.131	-.081	-.024	.108	.231			.550
		.650	-.251	-.216	-.165	-.117	-.055	.077	.193			.650
		.750	-.241	-.199	-.153	-.097	-.030	.090	.188			.750
		.850	-.235	-.185	-.140	-.081	-.026	.083	.167			.850
		.900	-.246	-.195	-.151	-.093	-.041	.062	.138			.900
M = 1.125; q = 856 lb/sq ft												
Upper surface		.000	.536	.600	.617	.625	.616	.577	.486			.000
		.032	.337	.234	.156	.052	-.033	-.271	-.460			.032
		.078	.263	.180	.123	.054	-.008	-.156	-.293			.078
		.150	.169	.101	.046	-.019	-.074	-.170	-.261			.150
		.250	.075	.022	-.019	-.073	-.124	-.211	-.275			.250
		.350	.059	-.001	-.044	-.094	-.141	-.226	-.286			.350
		.450	.016	-.040	-.082	-.131	-.170	-.241	-.306			.450
		.550	-.050	-.102	-.139	-.183	-.219	-.287	-.359			.550
		.650	-.046	-.100	-.140	-.186	-.229	-.302	-.365			.650
		.760	-.060	-.113	-.154	-.199	-.240	-.312	-.365			.760
		.840	-.117	-.167	-.200	-.247	-.285	-.347	-.402			.840
		.926	-.102	-.156	-.193	-.236	-.269	-.341	-.401			.926
Lower surface		.035	-.195	-.088	-.008	.084	.168	.361	.583			.035
		.082										.082
		.150	-.078	-.017	.031	.088	.148	.278	.448			.150
		.250										.250
		.350	-.121	-.063	-.029	.020	.074	.209	.350			.350
		.450	-.140	-.088	-.046	.008	.061	.162	.294			.450
		.550	-.189	-.135	-.090	-.042	.007	.114	.259			.550
		.650	-.211	-.163	-.123	-.074	-.027	.091	.230			.650
		.750	-.200	-.150	-.107	-.061	-.012	.116	.237			.750
		.850	-.181	-.132	-.091	-.045	.001	.122	.228			.850
		.900	-.185	-.139	-.098	-.053	-.004	.105	.208			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(a) 12-percent-semispan station - Concluded

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.200; q = 888 lb/sq ft											
Upper surface	.000	.562	.612	.633	.609	.632	.600	.502			.000
	.032	.332	.235	.143	.067	-.043	-.275	-.473			.032
	.078	.263	.193	.123	.064	.004	-.150	-.280			.078
	.150	.154	.090	.040	-.008	-.063	-.147	-.247			.150
	.250	.106	.048	-.006	-.062	-.108	-.186	-.253			.250
	.350	.091	.034	-.016	-.058	-.110	-.196	-.259			.350
	.450	.049	.001	-.045	-.090	-.134	-.208	-.272			.450
	.550	-.006	-.055	-.099	-.142	-.181	-.250	-.313			.550
	.650	-.008	-.064	-.112	-.153	-.192	-.260	-.321			.650
	.760	-.034	-.076	-.114	-.151	-.190	-.258	-.330			.760
	.840	-.092	-.135	-.173	-.208	-.243	-.310	-.363			.840
	.926	-.079	-.124	-.165	-.199	-.238	-.309	-.367			.926
Lower surface	.035	-.182	-.092	-.001	.080	.161	.348	.539			.035
	.082										.082
	.150	-.065	-.015	.039	.085	.139	.260	.430			.150
	.250										.250
	.350	-.094	-.050	-.004	.046	.100	.221	.358			.350
	.450	-.113	-.065	-.018	.029	.079	.187	.305			.450
	.550	-.150	-.111	-.069	-.023	.027	.142	.257			.550
	.650	-.179	-.135	-.092	-.044	.012	.107	.221			.650
	.750	-.169	-.124	-.080	-.035	.010	.105	.228			.750
	.850	-.138	-.115	-.081	-.039	.004	.105	.227			.850
	.900	-.160	-.117	-.092	-.058	-.016	.091	.220			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 627 \text{ lb/sq ft}$												
Upper surface		.000	-.381	-.042	.325	.413	.354	-.195	-.708	-1.040	-1.163	.000
		.025	.306	.211	.070	-.116	-.355	-1.204	-1.379	-1.331	-1.117	.025
		.076	.160	.067	-.050	-.177	-.331	-.645	-1.211	-1.353	-1.098	.076
		.150										.150
		.250	.002	-.073	-.151	-.237	-.328	-.537	-.881	-1.233	-1.029	.250
		.350	-.050	-.118	-.188	-.263	-.344	-.527	-.649	-1.076	-.969	.350
		.450	-.074	-.134	-.196	-.259	-.330	-.474	-.501	-.900	-.892	.450
		.550	-.070	-.120	-.171	-.224	-.279	-.379	-.447	-.730	-.820	.550
		.650	-.066	-.108	-.149	-.190	-.234	-.301	-.396	-.612	-.764	.650
		.750	-.045	-.076	-.107	-.137	-.167	-.210	-.298	-.525	-.720	.750
		.850	-.020	-.038	-.058	-.077	-.094	-.115	-.192	-.442	-.685	.850
		.926	.013	.004	-.006	-.014	-.022	-.031	-.094	-.338	-.634	.926
Lower surface		.023	-.630	-.441	-.195	.014	.171	.386	.493	.550	.591	.023
		.072	-.535	-.261	-.112	.001	.100	.281	.409	.499	.577	.072
		.150	-.427	-.204	-.091	-.004	.076	.226	.346	.435	.521	.150
		.250	-.301	-.185	-.101	-.032	.034	.166	.277	.360	.445	.250
		.350	-.251	-.172	-.099	-.040	.018	.135	.234	.309	.389	.350
		.450	-.227	-.166	-.104	-.053	-.001	.103	.191	.255	.327	.450
		.550	-.188	-.139	-.088	-.043	.000	.089	.165	.218	.280	.550
		.650	-.141	-.103	-.062	-.026	.010	.085	.144	.183	.231	.650
		.750	-.083	-.056	-.024	.004	.031	.091	.133	.149	.183	.750
		.860	-.030	-.014	.006	.026	.043	.085	.104	.093	.100	.860
		.900	-.009	.005	.019	.034	.047	.076	.083	.046	.031	.900
$M = 0.900; q = 713 \text{ lb/sq ft}$												
Upper surface		.000	-.276	.056	.331	.419	.390	.038	-.403	-.739	-.886	.000
		.025	.300	.203	.077	-.095	-.302	-1.008	-1.301	-1.372	-.985	.025
		.076	.156	.059	-.048	-.174	-.307	-.582	-.993	-1.375	-1.002	.076
		.150										.150
		.250	-.011	-.089	-.170	-.252	-.331	-.530	-.728	-1.068	-.998	.250
		.350	-.072	-.147	-.225	-.313	-.371	-.533	-.690	-.949	-.948	.350
		.450	-.101	-.171	-.251	-.350	-.432	-.573	-.687	-.851	-.886	.450
		.550	-.096	-.156	-.218	-.291	-.424	-.566	-.652	-.778	-.828	.550
		.650	-.092	-.142	-.193	-.255	-.392	-.572	-.623	-.695	-.776	.650
		.750	-.066	-.103	-.137	-.175	-.191	-.509	-.503	-.628	-.735	.750
		.850	-.034	-.055	-.074	-.092	-.092	-.160	-.271	-.571	-.709	.850
		.926	.008	-.003	-.010	-.017	-.011	-.042	-.166	-.479	-.664	.926
Lower surface		.023	-.676	-.406	-.207	-.002	.153	.376	.503	.573	.629	.023
		.072	-.514	-.260	-.128	-.013	.089	.272	.410	.510	.602	.072
		.150	-.413	-.221	-.113	-.021	.063	.219	.345	.451	.545	.150
		.250	-.341	-.218	-.129	-.052	.021	.158	.274	.373	.469	.250
		.350	-.310	-.216	-.134	-.065	.001	.125	.230	.322	.414	.350
		.450	-.327	-.223	-.144	-.080	-.021	.091	.185	.267	.354	.450
		.550	-.297	-.193	-.126	-.070	-.019	.078	.157	.229	.307	.550
		.650	-.197	-.140	-.090	-.046	-.005	.076	.135	.194	.264	.650
		.750	-.109	-.077	-.042	-.009	.023	.084	.121	.162	.222	.750
		.860	-.039	-.023	-.002	.020	.041	.078	.086	.099	.144	.860
		.900	-.013	.000	.015	.031	.046	.068	.057	.047	.080	.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 743 lb/sq ft											
Upper surface	.000	-.200	.091	.326	.419	.407	.114	-.291	-.631	-.885	.000
	.025	.302	.204	.085	-.074	-.270	-.884	-1.370	-1.292	-1.123	.025
	.076	.155	.061	-.044	-.161	-.287	-.531	-1.177	-1.280	-1.118	.076
	.150										.150
	.250	-.016	-.095	-.167	-.242	-.331	-.499	-.632	-1.233	-1.055	.250
	.350	-.083	-.165	-.236	-.298	-.366	-.507	-.632	-.973	-1.008	.350
	.450	-.119	-.212	-.293	-.361	-.415	-.548	-.647	-.769	-.947	.450
	.550	-.118	-.191	-.281	-.360	-.418	-.544	-.640	-.701	-.885	.550
	.650	-.114	-.183	-.280	-.376	-.431	-.560	-.635	-.670	-.823	.650
	.750	-.084	-.129	-.170	-.348	-.403	-.539	-.598	-.632	-.773	.750
	.850	-.045	-.065	-.077	-.155	-.349	-.508	-.546	-.585	-.739	.850
	.926	.005	-.002	-.004	-.005	-.076	-.223	-.299	-.474	-.664	.926
Lower surface	.023	-.671	-.419	-.208	-.012	.147	.374	.508	.589	.649	.023
	.072	-.476	-.260	-.135	-.023	.084	.269	.414	.524	.620	.072
	.150	-.389	-.232	-.122	-.033	.057	.214	.348	.461	.564	.150
	.250	-.333	-.217	-.145	-.068	.011	.151	.277	.386	.491	.250
	.350	-.312	-.228	-.155	-.087	-.013	.116	.232	.336	.435	.350
	.450	-.330	-.263	-.193	-.114	-.041	.076	.184	.281	.377	.450
	.550	-.333	-.278	-.179	-.102	-.040	.060	.156	.243	.333	.550
	.650	-.338	-.270	-.121	-.071	-.025	.052	.133	.210	.290	.650
	.750	-.302	-.116	-.053	-.024	.005	.056	.117	.179	.250	.750
	.860	-.093	-.016	-.003	.011	.022	.038	.075	.119	.177	.860
	.900	-.014	.010	.016	.025	.025	.015	.037	.066	.115	.900
M = 0.980; q = 771 lb/sq ft											
Upper surface	.000	-.158	.114	.346	.438	.432	.192	-.202			.000
	.025	.312	.221	.112	-.030	-.220	-.749	-1.254			.025
	.076	.172	.079	-.015	-.122	-.244	-.469	-1.144			.076
	.150										.150
	.250	-.007	-.070	-.137	-.222	-.296	-.449	-.555			.250
	.350	-.082	-.147	-.201	-.270	-.336	-.460	-.566			.350
	.450	-.141	-.210	-.266	-.328	-.388	-.502	-.601			.450
	.550	-.144	-.213	-.273	-.333	-.393	-.497	-.602			.550
	.650	-.165	-.241	-.298	-.357	-.414	-.517	-.617			.650
	.750	-.156	-.229	-.282	-.337	-.390	-.496	-.600			.750
	.850	-.160	-.229	-.282	-.334	-.389	-.490	-.596			.850
	.926	-.139	-.188	-.232	-.267	-.319	-.396	-.521			.926
Lower surface	.023	-.622	-.428	-.185	.004	.153	.384	.525			.023
	.072	-.425	-.210	-.109	-.006	.093	.280	.429			.072
	.150	-.334	-.201	-.099	-.017	.065	.225	.365			.150
	.250	-.302	-.200	-.123	-.057	.013	.159	.292			.250
	.350	-.292	-.211	-.137	-.078	-.019	.119	.246			.350
	.450	-.311	-.242	-.178	-.128	-.064	.075	.196			.450
	.550	-.320	-.258	-.199	-.149	-.085	.054	.166			.550
	.650	-.327	-.270	-.212	-.157	-.078	.043	.140			.650
	.750	-.303	-.249	-.193	-.136	-.046	.043	.124			.750
	.860	-.293	-.239	-.190	-.121	-.037	.020	.079			.860
	.900	-.278	-.217	-.169	-.100	-.048	-.010	.038			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 803 lb/sq ft											
Upper surface	.000	-.070	.178	.387	.474	.477	.275	-.092			.000
	.025	.363	.267	.160	.028	-.144	-.622	-1.114			.025
	.076	.223	.129	.037	-.067	-.176	-.374	-1.020			.076
	.150										.150
	.250	.056	-.022	-.093	-.165	-.233	-.367	-.456			.250
	.350	-.017	-.081	-.149	-.210	-.266	-.377	-.471			.350
	.450	-.080	-.147	-.211	-.268	-.315	-.419	-.508			.450
	.550	-.081	-.149	-.218	-.274	-.318	-.417	-.509			.550
	.650	-.116	-.177	-.242	-.295	-.342	-.441	-.531			.650
	.750	-.107	-.166	-.226	-.276	-.321	-.421	-.514			.750
	.850	-.113	-.167	-.226	-.277	-.317	-.417	-.511			.850
	.926	-.118	-.161	-.211	-.248	-.279	-.352	-.462			.926
Lower surface	.023	-.526	-.373	-.148	.047	.193	.427	.566			.023
	.072	-.342	-.155	-.048	.036	.138	.326	.473			.072
	.150	-.253	-.140	-.055	.022	.112	.273	.410			.150
	.250	-.228	-.145	-.073	-.011	.065	.207	.340			.250
	.350	-.217	-.159	-.089	-.024	.037	.168	.295			.350
	.450	-.234	-.185	-.126	-.069	-.010	.123	.246			.450
	.550	-.244	-.199	-.145	-.092	-.032	.101	.216			.550
	.650	-.251	-.209	-.159	-.102	-.040	.090	.193			.650
	.750	-.233	-.189	-.140	-.082	-.026	.094	.180			.750
	.860	-.224	-.179	-.136	-.075	-.014	.077	.140			.860
	.900	-.227	-.172	-.132	-.069	-.017	.051	.102			.900
M = 1.125; q = 856 lb/sq ft											
Upper surface	.000	.071	.297	.419	.495	.499	.359	.080			.000
	.025	.356	.261	.178	.037	-.096	-.586	-.863			.025
	.076	.224	.135	.059	-.041	-.137	-.443	-.803			.076
	.150										.150
	.250	.064	-.008	-.065	-.133	-.193	-.307	-.368			.250
	.350	.002	-.061	-.108	-.164	-.216	-.319	-.381			.350
	.450	-.060	-.120	-.164	-.216	-.264	-.351	-.408			.450
	.550	-.064	-.129	-.171	-.220	-.265	-.345	-.412			.550
	.650	-.086	-.149	-.193	-.243	-.286	-.367	-.442			.650
	.750	-.067	-.123	-.165	-.213	-.259	-.348	-.422			.750
	.850	-.077	-.131	-.171	-.217	-.260	-.342	-.413			.850
	.926	-.085	-.133	-.170	-.212	-.249	-.316	-.388			.926
Lower surface	.023	-.471	-.377	-.126	.058	.198	.405	.572			.023
	.072	-.250	-.115	-.036	.062	.145	.314	.481			.072
	.150	-.178	-.091	-.028	.045	.115	.273	.426			.150
	.250	-.177	-.085	-.021	.043	.099	.219	.364			.250
	.350	-.164	-.094	-.048	.012	.066	.189	.326			.350
	.450	-.180	-.123	-.078	-.028	.024	.148	.282			.450
	.550	-.189	-.137	-.093	-.043	.010	.126	.259			.550
	.650	-.196	-.141	-.098	-.048	.003	.113	.243			.650
	.750	-.185	-.130	-.086	-.036	.009	.121	.240			.750
	.860	-.177	-.128	-.086	-.040	.004	.124	.218			.860
	.900	-.183	-.132	-.093	-.048	.001	.111	.190			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(b) 25-percent-semispan station - Concluded

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		$M = 1.200; q = 888 \text{ lb/sq ft}$										
Upper surface	.000	.168	.332	.457	.527	.520	.422	.171				.000
	.025	.366	.284	.182	.069	-.062	-.475	-.723				.025
	.076	.235	.153	.065	-.016	-.113	-.402	-.670				.076
	.150											.150
	.250	.083	.016	-.047	-.102	-.161	-.272	-.322				.250
	.350	.027	-.030	-.080	-.131	-.190	-.295	-.352				.350
	.450	-.028	-.083	-.136	-.187	-.236	-.319	-.380				.450
	.550	-.038	-.099	-.153	-.204	-.249	-.319	-.377				.550
	.650	-.066	-.117	-.165	-.207	-.250	-.334	-.406				.650
	.750	-.055	-.104	-.147	-.192	-.237	-.315	-.387				.750
	.850	-.057	-.109	-.154	-.193	-.236	-.316	-.382				.850
	.926	-.064	-.109	-.152	-.192	-.234	-.302	-.362				.926
Lower surface	.023	-.575	-.367	-.105	.069	.191	.398	.565				.023
	.072	-.180	-.086	-.027	.060	.154	.311	.472				.072
	.150	-.145	-.078	-.005	.062	.130	.269	.421				.150
	.250	-.148	-.087	-.028	.033	.098	.220	.361				.250
	.350	-.142	-.082	-.033	.015	.071	.196	.327				.350
	.450	-.164	-.115	-.064	-.012	.038	.157	.280				.450
	.550	-.182	-.135	-.087	-.036	.022	.136	.249				.550
	.650	-.183	-.137	-.088	-.037	.010	.116	.229				.650
	.750	-.154	-.130	-.086	-.036	.014	.118	.234				.750
	.860	-.139	-.099	-.055	-.018	.015	.103	.240				.860
	.900	-.145	-.104	-.063	-.018	.028	.115	.226				.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 627 \text{ lb/sq ft}$												
Upper surface		.000	.194	.243	.316	.239	-.457	-1.217	-1.294	-.979	-.881	.000
		.020	.354	.270	.127	-.115	-.451	-1.196	-1.272	-.992	-.873	.020
		.073	.177	.079	-.044	-.213	-.412	-1.121	-1.201	-1.008	-.865	.073
		.150	.099	.011	-.099	-.222	-.370	-1.042	-1.129	-1.003	-.837	.150
		.250	.028	-.048	-.139	-.237	-.351	-.769	-1.137	-.950	-.815	.250
		.350	-.022	-.088	-.163	-.248	-.340	-.528	-1.033	-.901	-.792	.350
		.440	-.043	-.104	-.169	-.240	-.315	-.428	-.960	-.858	-.777	.440
		.550	-.046	-.098	-.151	-.209	-.267	-.343	-.824	-.811	-.756	.550
		.650	-.049	-.088	-.132	-.176	-.221	-.273	-.714	-.767	-.735	.650
		.750	-.038	-.070	-.100	-.131	-.162	-.195	-.579	-.723	-.715	.750
		.850	-.014	-.035	-.055	-.075	-.093	-.119	-.455	-.684	-.698	.850
		.923	.024	.010	-.000	-.011	-.021	-.035	-.304	-.632	-.675	.923
Lower surface		.024	-.787	-.568	-.329	-.020	.185	.384	.472	.505	.524	.024
		.073	-.764	-.431	-.143	-.014	.109	.282	.398	.466	.526	.073
		.150	-.801	-.359	-.132	-.025	.059	.208	.319	.392	.463	.150
		.250	-.532	-.230	-.116	-.038	.034	.160	.259	.327	.398	.250
		.350	-.211	-.170	-.097	-.032	.027	.137	.221	.282	.346	.350
		.450	-.147	-.140	-.084	-.029	.020	.115	.185	.234	.289	.450
		.550	-.109	-.097	-.053	-.009	.032	.110	.164	.200	.245	.550
		.650	-.071	-.056	-.022	.013	.043	.109	.145	.163	.195	.650
		.750	-.023	-.011	.014	.041	.065	.114	.131	.127	.143	.750
		.850	.015	.023	.039	.058	.075	.108	.100	.054	.052	.850
		.900	.030	.036	.048	.064	.075	.102	.077	.001	-.015	.900
$M = 0.900; q = 713 \text{ lb/sq ft}$												
Upper surface		.000	.214	.261	.314	.256	-.229	-1.425	-1.214	-.808	-.904	.000
		.020	.335	.251	.121	-.101	-.420	-1.441	-1.229	-.819	-.944	.020
		.073	.157	.053	-.064	-.230	-.414	-1.158	-1.190	-.845	-.872	.073
		.150	.076	-.017	-.129	-.259	-.387	-.664	-1.163	-.870	-.850	.150
		.250	.005	-.077	-.175	-.290	-.414	-.619	-1.120	-.876	-.831	.250
		.350	-.045	-.121	-.206	-.328	-.433	-.623	-1.055	-.865	-.811	.350
		.440	-.068	-.138	-.213	-.301	-.478	-.636	-.932	-.831	-.794	.440
		.550	-.071	-.130	-.192	-.272	-.432	-.644	-.827	-.795	-.773	.550
		.650	-.069	-.117	-.165	-.216	-.223	-.639	-.737	-.764	-.754	.650
		.750	-.053	-.087	-.119	-.152	-.159	-.253	-.655	-.735	-.732	.750
		.850	-.022	-.045	-.064	-.082	-.089	-.075	-.583	-.707	-.717	.850
		.923	.019	.008	-.001	-.009	-.011	-.001	-.485	-.672	-.699	.923
Lower surface		.024	-.815	-.602	-.392	-.055	.150	.368	.467	.524	.553	.024
		.073	-.730	-.431	-.176	-.042	.084	.265	.384	.474	.546	.073
		.150	-.792	-.376	-.173	-.054	.033	.191	.306	.399	.484	.150
		.250	-.657	-.309	-.159	-.069	.008	.143	.246	.334	.417	.250
		.350	-.377	-.234	-.133	-.058	.006	.121	.210	.288	.369	.350
		.450	-.262	-.192	-.115	-.053	.001	.101	.174	.240	.318	.450
		.550	-.163	-.130	-.076	-.026	.018	.098	.154	.208	.274	.550
		.650	-.099	-.074	-.037	.002	.037	.101	.133	.173	.230	.650
		.750	-.038	-.020	.006	.036	.063	.109	.119	.137	.182	.750
		.850	.010	.021	.038	.059	.078	.107	.080	.070	.103	.850
		.900	.028	.036	.050	.066	.081	.101	.051	.020	.044	.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station - Continued

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.940; q = 743 \text{ lb/sq ft}$												
Upper surface	.000	.224	.264	.307	.280	-.109	-1.291	-1.186	-1.071	-.870	.000	
	.020	.326	.241	.121	-.074	-.372	-1.285	-1.199	-1.039	-.884	.020	
	.073	.143	.040	-.070	-.215	-.404	-1.089	-1.170	-.990	-.903	.073	
	.150	.060	-.037	-.143	-.246	-.371	-.585	-1.151	-.924	-.927	.150	
	.250	-.013	-.107	-.197	-.302	-.388	-.592	-1.101	-.857	-.906	.250	
	.350	-.065	-.150	-.266	-.335	-.416	-.599	-1.052	-.796	-.880	.350	
	.440	-.092	-.176	-.282	-.384	-.454	-.611	-.979	-.796	-.863	.440	
	.550	-.091	-.167	-.254	-.395	-.467	-.614	-.838	-.808	-.845	.550	
	.650	-.087	-.139	-.184	-.402	-.473	-.631	-.762	-.789	-.819	.650	
	.750	-.063	-.096	-.120	-.232	-.465	-.622	-.680	-.762	-.794	.750	
.850	-.024	-.046	-.062	-.048	-.162	-.396	-.613	-.745	-.777	.850		
.923	.025	.010	.002	.016	-.012	-.142	-.512	-.718	-.753	.923		
Lower surface	.024	-.790	-.601	-.453	-.088	.126	.356	.469	.536	.572	.024	
	.073	-.669	-.438	-.199	-.069	.063	.251	.382	.484	.562	.073	
	.150	-.629	-.362	-.206	-.088	.016	.176	.303	.410	.500	.150	
	.250	-.631	-.345	-.220	-.108	-.015	.125	.242	.345	.437	.250	
	.350	-.452	-.307	-.180	-.093	-.016	.101	.207	.299	.390	.350	
	.450	-.388	-.317	-.157	-.083	-.020	.076	.169	.254	.339	.450	
	.550	-.354	-.247	-.092	-.048	-.002	.071	.148	.222	.298	.550	
	.650	-.299	-.079	-.044	-.011	.021	.069	.127	.187	.255	.650	
	.750	-.099	-.006	.005	.030	.051	.074	.112	.152	.212	.750	
	.850	.013	.032	.040	.059	.070	.063	.076	.092	.136	.850	
.900	.040	.045	.053	.069	.075	.053	.049	.045	.083	.900		
$M = 0.980; q = 771 \text{ lb/sq ft}$												
Upper surface	.000	.247	.285	.331	.315	.007	-1.122	-1.145				.000
	.020	.327	.252	.142	-.031	-.306	-1.127	-1.198				.020
	.073	.141	.050	-.039	-.186	-.367	-.955	-1.073				.073
	.150	.053	-.030	-.114	-.217	-.342	-.537	-.998				.150
	.250	-.032	-.104	-.185	-.268	-.365	-.550	-.948				.250
	.350	-.088	-.176	-.234	-.312	-.394	-.548	-.918				.350
	.440	-.125	-.209	-.283	-.356	-.421	-.566	-.879				.440
	.550	-.151	-.231	-.304	-.370	-.444	-.568	-.834				.550
	.650	-.164	-.248	-.320	-.387	-.455	-.587	-.779				.650
	.750	-.179	-.262	-.323	-.389	-.455	-.580	-.720				.750
.850	-.149	-.231	-.308	-.375	-.437	-.562	-.677				.850	
.923	-.024	-.052	-.111	-.169	-.266	-.398	-.498				.923	
Lower surface	.024	-.779	-.585	-.468	-.088	.114	.357	.483				.024
	.073	-.614	-.408	-.160	-.063	.054	.252	.394				.073
	.150	-.523	-.327	-.180	-.092	-.002	.174	.314				.150
	.250	-.491	-.309	-.212	-.137	-.049	.120	.252				.250
	.350	-.431	-.282	-.204	-.130	-.058	.094	.216				.350
	.450	-.398	-.300	-.231	-.159	-.070	.065	.177				.450
	.550	-.368	-.289	-.220	-.145	-.055	.056	.156				.550
	.650	-.342	-.267	-.201	-.131	-.036	.047	.134				.650
	.750	-.299	-.228	-.164	-.085	-.010	.044	.116				.750
	.850	-.227	-.157	-.084	-.006	-.001	.016	.073				.850
.900	-.138	-.069	-.018	.018	-.000	-.007	.044				.900	

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 803 lb/sq ft											
Upper surface	.000	.307	.333	.373	.374	.105	-.968	-1.156			.000
	.020	.378	.300	.186	.037	-.220	-.989	-1.200			.020
	.073	.198	.105	.008	-.124	-.284	-.823	-1.109			.073
	.150	.113	.029	-.061	-.157	-.253	-.457	-.975			.150
	.250	.028	-.036	-.129	-.208	-.293	-.470	-.793			.250
	.350	-.043	-.109	-.176	-.250	-.322	-.462	-.704			.350
	.440	-.073	-.146	-.224	-.287	-.348	-.480	-.647			.440
	.550	-.105	-.167	-.241	-.308	-.368	-.488	-.624			.550
	.650	-.117	-.187	-.258	-.322	-.384	-.508	-.621			.650
	.750	-.140	-.198	-.262	-.327	-.381	-.505	-.614			.750
Lower surface	.850	-.127	-.190	-.256	-.315	-.367	-.487	-.602			.850
	.923	-.095	-.137	-.185	-.236	-.283	-.374	-.471			.923
	.024	-.689	-.530	-.440	-.043	.157	.396	.523			.024
	.073	-.515	-.345	-.114	-.012	.105	.294	.436			.073
	.150	-.406	-.263	-.124	-.037	.051	.218	.357			.150
	.250	-.360	-.243	-.148	-.079	-.004	.165	.295			.250
	.350	-.337	-.216	-.146	-.075	-.006	.140	.260			.350
	.450	-.324	-.238	-.175	-.105	-.031	.112	.223			.450
	.550	-.302	-.229	-.167	-.093	-.021	.105	.201			.550
	.650	-.279	-.209	-.150	-.079	-.017	.099	.180			.650
Upper surface	.750	-.241	-.172	-.115	-.048	.012	.099	.162			.750
	.850	-.205	-.137	-.081	-.022	.022	.075	.119			.850
	.900	-.166	-.103	-.055	-.008	.019	.051	.086			.900
M = 1.125; q = 856 lb/sq ft											
Upper surface	.000	.347	.375	.420	.406	.221	-.697	-.970			.000
	.020	.372	.292	.207	.079	-.138	-.758	-.951			.020
	.073	.193	.099	.025	-.084	-.221	-.643	-.904			.073
	.150	.125	.037	-.034	-.120	-.199	-.376	-.859			.150
	.250	.049	-.020	-.089	-.164	-.247	-.401	-.818			.250
	.350	-.010	-.076	-.135	-.208	-.277	-.413	-.597			.350
	.440	-.055	-.120	-.172	-.235	-.296	-.419	-.544			.440
	.550	-.078	-.143	-.193	-.247	-.309	-.411	-.505			.550
	.650	-.098	-.160	-.213	-.275	-.328	-.426	-.499			.650
	.750	-.106	-.172	-.217	-.271	-.328	-.432	-.500			.750
Lower surface	.850	-.112	-.168	-.212	-.268	-.321	-.414	-.488			.850
	.923	-.085	-.149	-.192	-.242	-.286	-.356	-.447			.923
	.024	-.730	-.539	-.407	-.046	.156	.396	.539			.024
	.073	-.435	-.248	-.097	.014	.123	.300	.453			.073
	.150	-.329	-.193	-.093	-.006	.083	.223	.379			.150
	.250	-.276	-.185	-.097	-.022	.034	.163	.325			.250
	.350	-.265	-.160	-.100	-.035	.020	.156	.298			.350
	.450	-.258	-.175	-.125	-.070	-.013	.135	.269			.450
	.550	-.244	-.162	-.114	-.057	.001	.137	.256			.550
	.650	-.229	-.154	-.107	-.047	.009	.135	.244			.650
Lower surface	.750	-.198	-.129	-.080	-.020	.037	.150	.237			.750
	.850	-.151	-.088	-.044	.008	.056	.143	.205			.850
	.900	-.134	-.069	-.030	.019	.062	.130	.178			.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(c) 40-percent-semispan station - Concluded

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		$M = 1.200; q = 888 \text{ lb/sq ft}$										
Upper surface	.000	.404	.421	.463	.451	.267	-.521	-.830				.000
	.020	.407	.338	.254	.108	-.080	-.597	-.817				.020
	.073	.229	.151	.068	-.031	-.185	-.525	-.767				.073
	.150	.152	.079	-.002	-.079	-.161	-.448	-.733				.150
	.250	.076	.005	-.058	-.129	-.206	-.369	-.708				.250
	.350	.018	-.045	-.102	-.165	-.233	-.359	-.666				.350
	.440	-.019	-.081	-.136	-.195	-.261	-.380	-.522				.440
	.550	-.052	-.106	-.158	-.216	-.268	-.376	-.462				.550
	.650	-.076	-.136	-.191	-.241	-.291	-.381	-.448				.650
	.750	-.095	-.145	-.195	-.247	-.300	-.378	-.452				.750
	.850	-.095	-.144	-.193	-.238	-.285	-.370	-.452				.850
	.923	-.083	-.131	-.172	-.214	-.254	-.335	-.416				.923
Lower surface	.024	-.670	-.570	-.352	-.023	.164	.417	.551				.024
	.073	-.433	-.242	-.040	.039	.149	.326	.458				.073
	.150	-.277	-.154	-.061	.025	.100	.247	.377				.150
	.250	-.220	-.154	-.071	.006	.070	.183	.315				.250
	.350	-.208	-.134	-.074	-.012	.046	.167	.288				.350
	.450	-.224	-.152	-.096	-.045	.008	.123	.258				.450
	.550	-.229	-.165	-.109	-.051	.006	.119	.248				.550
	.650	-.202	-.160	-.110	-.053	.002	.109	.259				.650
	.750	-.165	-.117	-.073	-.034	.012	.122	.264				.750
	.850	-.136	-.080	-.030	.014	.057	.167	.244				.850
	.900	-.126	-.072	-.023	.025	.069	.169	.224				.900

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
$M = 0.800; q = 627 \text{ lb/sq ft}$												
Upper surface		.000	.130	.349	.459	.363	-.359	-1.029	-.949	-.852	-.804	.000
		.025	.386	.303	.166	-.134	-.540	-.998	-.818	-.707	-.694	.025
		.075	.249	.153	.027	-.170	-.409	-.965	-.796	-.689	-.683	.075
		.150	.156	.067	-.041	-.192	-.376	-.934	-.786	-.679	-.679	.150
		.250	.091	.012	-.075	-.185	-.321	-.911	-.761	-.665	-.672	.250
		.350	.042	-.024	-.103	-.197	-.301	-.864	-.723	-.649	-.664	.350
		.450										.450
		.550	-.009	-.060	-.117	-.180	-.244	-.678	-.649	-.618	-.648	.550
		.650	-.026	-.066	-.114	-.165	-.215	-.518	-.613	-.600	-.637	.650
		.750	-.023	-.053	-.087	-.125	-.157	-.345	-.583	-.582	-.624	.750
		.850	-.003	-.027	-.050	-.076	-.093	-.195	-.546	-.564	-.609	.850
		.900	.012	-.009	-.027	-.042	-.056	-.135	-.535	-.554	-.602	.900
		.925										.925
		.040	-.641	-.512	-.225	.004	.188	.359	.434	.456	.478	.040
		.091	-.614	-.466	-.156	-.001	.126	.282	.367	.405	.449	.091
		.150	-.602	-.455	-.120	.012	.111	.242	.319	.358	.402	.150
		.250	-.609	-.462	-.089	.003	.078	.192	.259	.292	.338	.250
Lower surface		.360	-.593	-.273	-.069	.001	.062	.157	.211	.236	.279	.360
		.450	-.525	-.130	-.047	.011	.060	.140	.179	.193	.230	.450
		.550	-.390	-.060	-.022	.024	.063	.126	.144	.145	.175	.550
		.650	-.218	-.017	.008	.045	.073	.122	.117	.104	.126	.650
		.800	.001	.032	.046	.071	.088	.112	.052	.019	.029	.800
		.874	.055	.044	.053	.071	.082	.095	-.013	-.054	-.052	.874
$M = 0.900; q = 713 \text{ lb/sq ft}$												
Upper surface		.000	.149	.357	.443	.356	-.212	-1.316	-1.010	-.881	-.805	.000
		.025	.374	.289	.151	-.161	-.899	-1.559	-.990	-.746	-.724	.025
		.075	.234	.133	.005	-.212	-.445	-1.396	-.763	-.715	-.708	.075
		.150	.141	.045	-.066	-.243	-.475	-1.322	-.755	-.705	-.705	.150
		.250	.076	-.007	-.103	-.239	-.455	-.954	-.741	-.695	-.696	.250
		.350	.028	-.046	-.130	-.246	-.437	-.768	-.722	-.682	-.689	.350
		.450										.450
		.550	-.023	-.077	-.139	-.213	-.256	-.558	-.674	-.659	-.675	.550
		.650	-.036	-.083	-.135	-.194	-.241	-.243	-.647	-.644	-.668	.650
		.750	-.032	-.067	-.102	-.142	-.168	-.153	-.616	-.625	-.658	.750
		.850	-.008	-.035	-.060	-.081	-.093	-.104	-.580	-.606	-.647	.850
		.900	.007	-.014	-.030	-.044	-.049	-.072	-.564	-.593	-.640	.900
		.925										.925
		.040	-.737	-.551	-.270	-.021	.158	.333	.415	.457	.492	.040
		.091	-.701	-.496	-.195	-.022	.103	.256	.348	.404	.459	.091
		.150	-.678	-.479	-.154	-.008	.092	.218	.301	.357	.418	.150
		.250	-.673	-.502	-.117	-.014	.062	.173	.242	.295	.355	.250
Lower surface		.360	-.662	-.339	-.090	-.012	.051	.143	.195	.241	.300	.360
		.450	-.595	-.180	-.062	.002	.053	.130	.161	.199	.253	.450
		.550	-.453	-.093	-.033	.018	.061	.119	.126	.153	.199	.550
		.650	-.251	-.037	.001	.042	.076	.120	.098	.115	.154	.650
		.800	.022	.025	.047	.072	.093	.116	.038	.039	.065	.800
		.874	.080	.040	.055	.075	.089	.104	-.019	-.026	-.006	.874

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - (continued)

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.940; q = 743 lb/sq ft											
Upper surface	.000	.169	.342	.411	.360	-.050	-1.083	-1.077	-.969	-.890	.000
	.025	.351	.261	.129	-.139	-.725	-1.386	-1.038	-.865	-.823	.025
	.075	.211	.104	-.027	-.220	-.411	-1.246	-.856	-.751	-.768	.075
	.150	.120	.019	-.103	-.278	-.449	-1.193	-.863	-.742	-.758	.150
	.250	.055	-.031	-.137	-.307	-.437	-1.079	-.857	-.732	-.750	.250
	.350	.012	-.064	-.161	-.350	-.474	-.712	-.819	-.721	-.740	.350
	.450										.450
	.550	-.030	-.085	-.149	-.354	-.505	-.656	-.752	-.700	-.722	.550
	.650	-.041	-.088	-.144	-.155	-.515	-.675	-.705	-.686	-.711	.650
	.750	-.033	-.069	-.107	-.112	-.222	-.525	-.655	-.672	-.701	.750
	.850	-.009	-.036	-.062	-.069	-.048	-.175	-.613	-.655	-.691	.850
	.900	.006	-.013	-.032	-.037	-.008	-.113	-.587	-.643	-.684	.900
	.925										.925
	.040	-.761	-.599	-.334	-.077	.121	.304	.405	.461	.506	.040
Lower surface	.091	-.729	-.548	-.246	-.065	.072	.227	.335	.409	.475	.091
	.150	-.717	-.518	-.195	-.043	.065	.191	.289	.365	.433	.150
	.250	-.720	-.487	-.142	-.042	.038	.143	.230	.304	.373	.250
	.360	-.708	-.380	-.101	-.032	.030	.112	.185	.251	.319	.360
	.450	-.628	-.236	-.069	-.013	.036	.098	.154	.212	.275	.450
	.550	-.474	-.135	-.036	.010	.047	.087	.121	.167	.222	.550
	.650	-.308	-.063	.000	.039	.068	.088	.096	.128	.178	.650
	.800	-.093	.012	.048	.075	.094	.086	.041	.060	.095	.800
	.874	-.021	.032	.057	.079	.094	.076	-.012	.001	.029	.874
M = 0.980; q = 771 lb/sq ft											
Upper surface	.000	.207	.344	.413	.371	.075	-.818	-1.290			.000
	.025	.319	.236	.128	-.084	-.498	-1.214	-1.382			.025
	.075	.171	.076	-.026	-.182	-.362	-1.094	-1.328			.075
	.150	.070	-.019	-.111	-.247	-.407	-1.048	-1.280			.150
	.250	-.004	-.083	-.171	-.286	-.399	-.969	-1.231			.250
	.350	-.052	-.154	-.240	-.337	-.429	-.635	-1.209			.350
	.450										.450
	.550	-.128	-.210	-.294	-.386	-.476	-.616	-1.086			.550
	.650	-.143	-.247	-.332	-.409	-.493	-.643	-.947			.650
	.750	-.056	-.222	-.352	-.447	-.520	-.653	-.882			.750
	.850	-.036	-.003	-.139	-.350	-.504	-.644	-.740			.850
	.900	-.021	.020	-.014	-.118	-.289	-.638	-.653			.900
	.925										.925
	.040	-.708	-.543	-.365	-.145	.054	.282	.400			.040
Lower surface	.091	-.674	-.533	-.286	-.154	.009	.205	.324			.091
	.150	-.667	-.508	-.262	-.116	.007	.165	.276			.150
	.250	-.685	-.480	-.250	-.146	-.022	.114	.216			.250
	.360	-.718	-.477	-.267	-.171	-.030	.080	.170			.360
	.450	-.712	-.419	-.246	-.144	-.030	.058	.137			.450
	.550	-.634	-.355	-.221	-.097	-.020	.038	.102			.550
	.650	-.473	-.270	-.151	-.004	-.001	.025	.075			.650
	.800	-.207	-.063	.036	.056	.028	.001	.028			.800
	.874	-.128	.008	.071	.066	.028	-.023	-.012			.874

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - Continued

	x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 1.030; q = 803 lb/sq ft											
Upper surface	.000	.266	.379	.431	.414	.139	-.717	-1.159			.000
	.025	.361	.288	.184	-.017	-.381	-1.091	-1.249			.025
	.075	.218	.135	.028	-.122	-.295	-.951	-1.177			.075
	.150	.120	.043	-.058	-.178	-.320	-.911	-1.132			.150
	.250	.042	-.032	-.122	-.217	-.328	-.850	-1.087			.250
	.350	-.023	-.084	-.170	-.270	-.353	-.548	-1.066			.350
	.450										.450
	.550	-.082	-.158	-.226	-.313	-.408	-.531	-1.042			.550
	.650	-.113	-.189	-.264	-.335	-.407	-.561	-.841			.650
	.750	-.138	-.214	-.289	-.374	-.442	-.571	-.792			.750
	.850	-.128	-.211	-.294	-.374	-.447	-.565	-.718			.850
	.900	-.085	-.164	-.262	-.351	-.428	-.563	-.638			.900
	.925										.925
Lower surface	.040	-.610	-.472	-.363	-.085	.096	.319	.442			.040
	.091	-.575	-.465	-.225	-.094	.045	.244	.369			.091
	.150	-.566	-.437	-.202	-.058	.042	.208	.323			.150
	.250	-.576	-.401	-.187	-.084	-.002	.160	.264			.250
	.360	-.611	-.405	-.204	-.119	-.016	.127	.220			.360
	.450	-.622	-.357	-.188	-.097	.009	.107	.187			.450
	.550	-.571	-.301	-.171	-.081	-.003	.088	.154			.550
	.650	-.461	-.247	-.133	-.056	.010	.076	.127			.650
	.800	-.263	-.146	.000	.000	.028	.050	.077			.800
	.874	-.187	-.091	-.022	.012	.023	.026	.043			.874
M = 1.125; q = 856 lb/sq ft											
Upper surface	.000	.327	.426	.461	.462	.234	-.419	-.880			.000
	.025	.383	.309	.226	.032	-.249	-.851	-.948			.025
	.075	.242	.161	.075	-.059	-.225	-.736	-.920			.075
	.150	.144	.071	-.002	-.113	-.264	-.714	-.889			.150
	.250	.071	-.007	-.062	-.151	-.251	-.681	-.861			.250
	.350	.015	-.062	-.120	-.195	-.275	-.594	-.850			.350
	.450										.450
	.550	-.057	-.128	-.184	-.266	-.336	-.434	-.827			.550
	.650	-.088	-.153	-.210	-.283	-.357	-.448	-.835			.650
	.750	-.110	-.186	-.245	-.306	-.372	-.474	-.684			.750
	.850	-.118	-.193	-.252	-.325	-.381	-.477	-.608			.850
	.900	-.111	-.189	-.252	-.321	-.391	-.483	-.557			.900
	.925										.925
Lower surface	.040	-.503	-.402	-.294	-.017	.132	.333	.480			.040
	.091	-.457	-.355	-.151	-.029	.079	.259	.408			.091
	.150	-.444	-.304	-.132	-.009	.087	.225	.368			.150
	.250	-.432	-.262	-.122	-.030	.040	.176	.315			.250
	.360	-.420	-.260	-.148	-.075	-.007	.153	.279			.360
	.450	-.422	-.241	-.141	-.066	.001	.144	.254			.450
	.550	-.406	-.221	-.137	-.068	.001	.136	.227			.550
	.650	-.364	-.186	-.110	-.038	.021	.135	.206			.650
	.800	-.272	-.127	-.061	-.000	.050	.124	.164			.800
	.874	-.225	-.094	-.034	.021	.063	.108	.136			.874

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(d) 60-percent-semispan station - Concluded

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
		M = 1.200; q = 888 lb/sq ft										
Upper surface		.000	.330	.410	.454	.489	.282	-.216	-.702			.000
		.025	.390	.321	.227	.074	-.167	-.659	-.832			.025
		.075	.252	.174	.087	-.029	-.184	-.597	-.783			.075
		.150	.156	.088	.009	-.093	-.258	-.588	-.764			.150
		.250	.077	.018	-.052	-.132	-.223	-.562	-.744			.250
		.350	.024	-.039	-.103	-.170	-.254	-.544	-.737			.350
		.450										.450
		.550	-.030	-.097	-.159	-.228	-.283	-.391	-.721			.550
		.650	-.051	-.111	-.179	-.244	-.318	-.414	-.730			.650
		.750	-.084	-.152	-.208	-.274	-.339	-.432	-.732			.750
		.850	-.095	-.160	-.227	-.291	-.354	-.431	-.628			.850
		.900	-.090	-.161	-.227	-.294	-.360	-.438	-.492			.900
		.925										.925
		.040	-.601	-.652	-.291	-.041	.132	.323	.466			.040
		.091	-.491	-.515	-.179	-.034	.076	.250	.395			.091
		.150	-.430	-.309	-.127	-.016	.085	.225	.360			.150
Lower surface		.250	-.370	-.209	-.121	-.027	.044	.169	.320			.250
		.360	-.325	-.201	-.139	-.072	-.005	.132	.299			.360
		.450	-.301	-.186	-.121	-.058	.003	.155	.281			.450
		.550	-.286	-.174	-.107	-.043	.019	.157	.265			.550
		.650	-.267	-.145	-.077	-.013	.052	.162	.255			.650
		.800	-.209	-.098	-.029	.035	.093	.170	.218			.800
		.874	-.176	-.066	.005	.061	.109	.170	.195			.874

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(e) 80-percent-semispan station - Continued

x/c		$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c	
M = 0.940; q = 743 lb/sq ft												
Upper surface	.022	.388	.346	.234	-.080	-.677	-1.342	-.601	-.625	-.663	.022	
	.076	.292	.214	.094	-.174	-.452	-1.193	-.586	-.611	-.654	.076	
	.150	.209	.124	.029	-.222	-.472	-1.136	-.574	-.602	-.648	.150	
	.250	.140	.065	-.034	-.196	-.450	-1.082	-.564	-.595	-.642	.250	
	.370	.078	.008	-.081	-.195	-.487	-1.044	-.555	-.589	-.636	.370	
	.450	.036	-.030	-.111	-.222	-.532	-.967	-.545	-.583	-.630	.450	
	.550	.005	-.053	-.122	-.216	-.552	-.615	-.540	-.583	-.626	.550	
	.600										.600	
	.650	-.023	-.072	-.129	-.206	-.234	-.513	-.533	-.579	-.622	.650	
	.750	-.036	-.066	-.111	-.162	-.092	-.484	-.528	-.576	-.615	.750	
	.850	-.065	-.051	-.085	-.113	-.056	-.470	-.523	-.571	-.608	.850	
	.900										.900	
Lower surface	.078	-.537	-.514	-.462	-.057	.098	.230	.294	.343	.387	.078	
	.150	-.514	-.510	-.408	-.037	.067	.176	.233	.288	.345	.150	
	.250	-.495	-.512	-.278	-.017	.062	.141	.180	.232	.289	.250	
	.360	-.486	-.525	-.113	-.011	.053	.112	.132	.181	.235	.360	
	.450										.450	
	.560	-.523	-.489	-.021	.025	.067	.083	.062	.097	.142	.560	
	.610	-.545	-.462	-.006	.032	.070	.077	.045	.076	.122	.610	
	.700	-.551	-.390	.034	.063	.092	.081	.031	.056	.093	.700	
	.800	-.509	-.236	.064	.085	.106	.069	-.002	.016	.044	.800	
	M = 0.980; q = 771 lb/sq ft											
	Upper surface	.022	.341	.260	.171	-.013	-.324	-1.182	-.964			.022
		.076	.229	.123	.023	-.124	-.379	-1.065	-.838			.076
.150		.143	.032	-.057	-.205	-.396	-1.013	-.835			.150	
.250		.084	-.033	-.124	-.250	-.373	-.970	-.822			.250	
.370		.032	-.108	-.200	-.299	-.418	-.946	-.800			.370	
.450		-.005	-.133	-.261	-.352	-.472	-.947	-.772			.450	
.550		-.029	-.046	-.310	-.381	-.516	-.955	-.751			.550	
.600											.600	
.650		-.050	-.058	-.311	-.429	-.540	-.940	-.724			.650	
.750		-.055	-.053	-.043	-.450	-.568	-.756	-.696			.750	
.850		-.075	-.039	.003	-.131	-.563	-.707	-.672			.850	
.900											.900	
Lower surface	.078	-.682	-.810	-.578	-.237	-.006	.159	.288			.078	
	.150	-.639	-.789	-.501	-.209	-.035	.096	.228			.150	
	.250	-.602	-.770	-.396	-.075	-.017	.066	.179			.250	
	.360	-.574	-.711	-.279	-.050	-.020	.035	.136			.360	
	.450										.450	
	.560	-.552	-.503	-.039	.006	.006	.003	.074			.560	
	.610	-.570	-.394	.002	.020	.010	-.004	.059			.610	
	.700	-.619	-.093	.058	.059	.036	.004	.050			.700	
	.800	-.603	.154	.095	.089	.051	-.001	.024			.800	

TABLE IV.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR WING IN PRESENCE OF BODY - Continued

(r) 95-percent-semispan station

		x/c	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/c
M = 0.800; q = 627 lb/sq ft												
Upper surface		.073	.315	.284	.210	.054	-.229	-.437	-.335	-.371	-.433	.073
		.150	.205	.184	.110	-.039	-.239	-.420	-.332	-.370	-.432	.150
		.250	.111	.084	.018	-.092	-.246	-.401	-.334	-.371	-.432	.250
		.350	.043	.024	-.033	-.119	-.226	-.369	-.331	-.371	-.432	.350
		.460	-.026	-.029	-.072	-.138	-.213	-.332	-.327	-.373	-.436	.460
		.550	-.078	-.065	-.094	-.144	-.199	-.302	-.324	-.372	-.439	.550
		.660	-.109	-.083	-.087	-.123	-.164	-.272	-.318	-.373	-.443	.660
		.750	-.122	-.086	-.062	-.083	-.118	-.250	-.318	-.374	-.445	.750
		.800										.800
		.100	-.226	-.317	-.433	-.133	.057	.168	.214	.245	.277	.100
Lower surface		.200	-.214	-.294	-.344	-.090	.033	.104	.138	.169	.200	.200
		.250	-.208	-.284	-.321	-.066	.027	.080	.107	.132	.164	.250
		.350	-.197	-.268	-.293	-.039	.019	.037	.052	.069	.094	.350
		.450	-.187	-.251	-.242	-.015	.016	.000	-.000	.003	.024	.450
		.550	-.175	-.239	-.160	.012	.023	-.018	-.036	-.039	-.034	.550
		.600	-.170	-.236	-.108	.020	.026	-.027	-.052	-.059	-.060	.600
		.690	-.160	-.238	-.027	.038	.036	-.039	-.078	-.097	-.111	.690
M = 0.900; q = 713 lb/sq ft												
Upper surface		.073	.326	.289	.212	.033	-.300	-.518	-.397	-.429	-.485	.073
		.150	.208	.183	.116	-.064	-.266	-.507	-.396	-.429	-.483	.150
		.250	.120	.084	.010	-.122	-.292	-.491	-.400	-.430	-.480	.250
		.350	.044	.018	-.046	-.156	-.290	-.468	-.401	-.429	-.479	.350
		.460	-.034	-.044	-.100	-.179	-.242	-.437	-.403	-.432	-.482	.460
		.550	-.100	-.087	-.126	-.174	-.216	-.408	-.405	-.434	-.484	.550
		.660	-.139	-.102	-.111	-.140	-.171	-.379	-.405	-.437	-.486	.660
		.750	-.152	-.098	-.073	-.090	-.117	-.355	-.409	-.440	-.488	.750
		.800										.800
		.100	-.247	-.332	-.443	-.139	.073	.203	.202	.239	.276	.100
Lower surface		.200	-.234	-.309	-.343	-.094	.042	.132	.127	.168	.207	.200
		.250	-.229	-.298	-.324	-.069	.035	.107	.096	.134	.174	.250
		.350	-.218	-.282	-.298	-.041	.022	.056	.036	.069	.108	.350
		.450	-.208	-.266	-.255	-.017	.011	.003	-.031	-.003	.029	.450
		.550	-.197	-.256	-.180	.012	.020	-.029	-.077	-.060	-.035	.550
		.600	-.192	-.253	-.131	.022	.025	-.041	-.095	-.088	-.064	.600
		.690	-.182	-.255	-.039	.041	.037	-.061	-.131	-.135	-.125	.690

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING

(a) Station A

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 310 \text{ lb/sq ft}$										
.055										.055
.166	.041	.018	.007	-.006	-.023	-.035	-.028	-.029	-.028	.166
.277	.017	.004	-.007	-.028	-.036	-.036	-.036	-.033	-.053	.277
.367	.107	.069	.045	.007	-.002	-.045	-.092	-.138	-.153	.367
.387	.097	.052	.022	-.004	-.037	-.108	-.186	-.263	-.284	.387
.415	.074	.022	-.019	-.060	-.102	-.201	-.312	-.395	-.429	.415
.443	.045	-.007	-.056	-.095	-.151	-.260	-.389	-.426	-.489	.443
.498	.019	-.041	-.088	-.136	-.191	-.301	-.396	-.408	-.433	.498
.553	-.010	-.061	-.104	-.145	-.191	-.285	-.309	-.404	-.416	.553
.581										.581
.609	-.012	-.044	-.065	-.125	-.160	-.207	-.238	-.340	-.385	.609
.636	-.022	-.053	-.080	-.097	-.128	-.155	-.210	-.301	-.386	.636
.664	-.022	-.050	-.065	-.076	-.097	-.114	-.172	-.270	-.408	.664
.692	-.011	-.028	-.036	-.048	-.055	-.065	-.114	-.199	-.369	.692
.719	.004	-.007	-.015	-.016	-.024	-.023	-.060	-.136	-.305	.719
.774	.010	.000	.003	.007	.003	.003	-.016	-.072	-.199	.774
.830	-.004	-.008	-.003	.001	.003	.007	-.004	-.036	-.109	.830
.871	.007	.000	.006	.010	.011	.018	.013	-.007	-.046	.871
.954	.015	.020	.027	.037	.041	.037	.034	.024	.028	.954
$M = 0.900; q = 358 \text{ lb/sq ft}$										
.055										.055
.166	.039	.015	.003	-.014	-.024	-.030	-.019	-.014	-.009	.166
.277	.015	.000	-.014	-.034	-.041	-.031	-.013	-.001	-.008	.277
.367	.120	.081	.064	.011	.028	.006	-.022	-.052	-.072	.367
.387	.116	.071	.042	.015	-.004	-.059	-.114	-.179	-.220	.387
.415	.083	.031	-.006	-.047	-.094	-.157	-.234	-.334	-.388	.415
.443	.052	-.007	-.052	-.099	-.151	-.236	-.320	-.405	-.412	.443
.498	.008	-.056	-.105	-.155	-.204	-.306	-.414	-.488	-.445	.498
.553	-.034	-.091	-.156	-.231	-.287	-.377	-.483	-.321	-.486	.553
.581										.581
.609	-.030	-.098	-.139	-.184	-.231	-.438	-.483	-.415	-.450	.609
.636	-.045	-.081	-.111	-.143	-.173	-.451	-.418	-.479	-.441	.636
.664	-.036	-.063	-.084	-.100	-.100	-.243	-.202	-.506	-.442	.664
.692	-.018	-.036	-.044	-.052	-.047	-.035	-.100	-.460	-.452	.692
.719	.000	-.011	-.016	-.020	-.017	.006	-.080	-.169	-.349	.719
.774	.008	-.001	.002	.004	.008	.027	-.050	-.131	-.306	.774
.830	-.012	-.013	-.006	-.003	.004	.013	-.022	-.077	-.202	.830
.871	-.001	-.001	.005	.008	.013	.023	.007	-.035	-.118	.871
.954	.013	.020	.031	.033	.041	.040	.030	.015	-.016	.954

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Continued

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.940; q = 368 \text{ lb/sq ft}$										
.055										.055
.166	.040	.014	.001	-.011	-.020	-.035	-.021	-.004	.001	.166
.277	.012	-.004	-.016	-.036	-.039	-.029	-.005	.018	.014	.277
.367	.130	.095	.071	.023	.043	.026	.009	-.010	-.043	.367
.387	.126	.085	.057	.039	.013	-.035	-.086	-.137	-.196	.387
.415	.092	.040	-.001	-.024	-.071	-.136	-.201	-.289	-.371	.415
.443	.057	-.002	-.050	-.088	-.134	-.214	-.287	-.367	-.461	.443
.498	.005	-.055	-.107	-.145	-.199	-.292	-.389	-.454	-.325	.498
.553	-.048	-.118	-.187	-.227	-.272	-.362	-.447	-.490	-.446	.553
.581										.581
.609	-.043	-.133	-.152	-.281	-.331	-.421	-.492	-.410	-.515	.609
.636	-.055	-.102	-.142	-.284	-.350	-.447	-.509	-.405	-.544	.636
.664	-.048	-.070	-.085	-.179	-.347	-.474	-.483	-.451	-.517	.664
.692	-.019	-.032	-.034	-.027	-.082	-.387	-.404	-.482	-.493	.692
.719	.005	-.005	-.009	.002	.005	-.030	-.055	-.385	-.372	.719
.774	.009	.005	.008	.013	.026	.034	-.039	-.242	-.318	.774
.830	-.011	-.011	-.008	.002	.014	.029	-.032	-.096	-.253	.830
.871	.000	.002	.005	.011	.021	.031	-.006	-.050	-.152	.871
.954	.019	.024	.033	.039	.049	.051	.033	.015	-.038	.954
$M = 0.980; q = 385 \text{ lb/sq ft}$										
.055										.055
.166	.044	.023	.004	-.008	-.020	-.024	.000	.017	.031	.166
.277	.020	-.003	-.015	-.030	-.033	-.017	.020	.050	.055	.277
.367	.153	.124	.104	.039	.082	.068	.057	.044	.013	.367
.387	.154	.113	.087	.100	.048	.010	-.031	-.079	-.134	.387
.415	.115	.067	.030	.003	-.037	-.090	-.154	-.229	-.308	.415
.443	.077	.021	-.021	-.063	-.103	-.169	-.234	-.312	-.396	.443
.498	.022	-.036	-.080	-.126	-.174	-.251	-.337	-.405	-.481	.498
.553	-.068	-.121	-.164	-.206	-.245	-.322	-.400	-.453	-.529	.553
.581										.581
.609	-.064	-.123	-.228	-.263	-.311	-.388	-.457	-.510	-.535	.609
.636	-.111	-.181	-.241	-.288	-.334	-.416	-.489	-.544	-.535	.636
.664	-.143	-.205	-.257	-.311	-.362	-.440	-.514	-.578	-.338	.664
.692	-.133	-.201	-.257	-.308	-.354	-.450	-.537	-.589	-.389	.692
.719	-.028	-.053	-.088	-.133	-.206	-.343	-.466	-.351	-.499	.719
.774	-.003	.024	.040	.034	.010	-.073	-.085	-.108	-.202	.774
.830	-.011	.009	.028	.037	.040	.014	-.066	-.161	-.266	.830
.871	.003	.019	.032	.039	.047	.048	-.030	-.165	-.254	.871
.954	.030	.041	.054	.064	.076	.091	.054	-.039	-.096	.954

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Continued

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 400 \text{ lb/sq ft}$										
.055										.055
.166	.083	.069	.053	.041	.026	.012	.026	.048	.073	.166
.277	.024	.025	.010	-.011	-.016	-.021	.061	.102	.112	.277
.367	.197	.159	.129	.014	.108	.135	.122	.113	.090	.367
.387	.204	.167	.139	.173	.115	.079	.038	-.006	-.048	.387
.415	.171	.123	.081	.065	.021	-.013	-.082	-.153	-.218	.415
.443	.132	.075	.028	-.007	-.047	-.092	-.155	-.236	-.309	.443
.498	.076	.024	-.034	-.073	-.118	-.179	-.263	-.323	-.393	.498
.553	-.003	-.056	-.103	-.143	-.182	-.244	-.321	-.376	-.439	.553
.581										.581
.609	-.034	-.074	-.115	-.216	-.243	-.311	-.385	-.428	-.485	.609
.636	-.066	-.123	-.185	-.225	-.270	-.338	-.411	-.467	-.524	.636
.664	-.091	-.142	-.206	-.252	-.296	-.364	-.440	-.507	-.549	.664
.692	-.104	-.149	-.209	-.250	-.294	-.381	-.466	-.532	-.587	.692
.719	-.084	-.108	-.154	-.185	-.207	-.309	-.440	-.528	-.589	.719
.774	-.048	-.039	-.026	-.029	-.052	-.094	-.117	-.017	.007	.774
.830	-.070	-.055	-.048	-.045	-.059	-.069	-.066	-.067	-.186	.830
.871	-.057	-.042	-.042	-.041	-.049	-.048	-.032	-.067	-.140	.871
.954	-.143	-.124	-.085	-.065	-.053	-.033	-.056	-.154	-.205	.954
$M = 1.125; q = 421 \text{ lb/sq ft}$										
.055										.055
.166	.063	.042	.031	.013	-.002	-.014	-.026	-.027	-.037	.166
.277	.017	.009	.000	-.027	-.032	-.031	-.034	-.039	-.088	.277
.367	-.007	-.015	-.006	-.012	-.033	-.012	.010	.124	.188	.367
.387	.123	.087	.055	.003	.044	.036	.031	.057	.076	.387
.415	.165	.124	.103	.072	.038	-.022	-.058	-.075	-.088	.415
.443	.135	.089	.055	.032	-.015	-.074	-.118	-.148	-.183	.443
.498	.088	.035	-.007	-.046	-.089	-.149	-.208	-.241	-.276	.498
.553	.029	-.021	-.061	-.102	-.140	-.205	-.250	-.278	-.318	.553
.581										.581
.609	-.018	-.052	-.082	-.159	-.198	-.260	-.309	-.342	-.353	.609
.636	-.038	-.095	-.136	-.180	-.215	-.281	-.327	-.378	-.376	.636
.664	-.056	-.106	-.149	-.196	-.236	-.300	-.361	-.398	-.391	.664
.692	-.067	-.115	-.158	-.201	-.245	-.315	-.377	-.414	-.422	.692
.719	-.066	-.108	-.140	-.179	-.216	-.285	-.369	-.417	-.424	.719
.774	-.039	-.047	-.050	-.054	-.066	-.068	-.083	.056	.112	.774
.830	-.050	-.050	-.042	-.042	-.043	-.034	-.029	.056	-.042	.830
.871	-.039	-.038	-.027	-.024	-.025	-.011	.008	.058	-.004	.871
.954	-.074	-.074	-.052	-.037	-.011	.012	.071	-.016	-.084	.954

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.200; q = 436 \text{ lb/sq ft}$										
.055										.055
.166	.075	.057	.042	.027	.014	-.003	-.003	-.008	-.025	.166
.277	.033	.024	.001	-.002	-.003	-.013	-.012	-.044	-.088	.277
.367	.018	.006	.010	.008	-.011	-.010	-.008	-.053	-.051	.367
.387	.036	.030	.023	.019	.025	.034	.028	.067	.056	.387
.415	.171	.137	.059	.019	.048	.003	-.042	-.071	-.063	.415
.443	.160	.117	.102	.074	.025	-.049	-.099	-.133	-.161	.443
.498	.118	.067	.028	-.014	-.055	-.119	-.173	-.218	-.246	.498
.553	.057	.014	-.026	-.061	-.099	-.164	-.217	-.260	-.284	.553
.581										.581
.609	.006	-.027	-.059	-.129	-.150	-.224	-.271	-.307	-.340	.609
.636	-.023	-.066	-.107	-.139	-.173	-.241	-.293	-.339	-.376	.636
.664	-.035	-.075	-.125	-.168	-.201	-.264	-.311	-.355	-.393	.664
.692	-.054	-.096	-.139	-.172	-.203	-.274	-.336	-.383	-.406	.692
.719	-.062	-.099	-.140	-.175	-.209	-.274	-.342	-.397	-.412	.719
.774	-.048	-.057	-.066	-.069	-.068	-.070	-.076	-.074	-.070	.774
.830	-.039	-.041	-.044	-.038	-.029	-.025	-.014	-.026	.010	.830
.871	-.041	-.034	-.027	-.016	-.008	-.000	.010	.000	.026	.871
.954	-.100	-.082	-.075	-.056	-.036	-.031	-.033	-.050	-.084	.954

TABLE V. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(b) Station B

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 310 \text{ lb/sq ft}$										
.166	.030	.013	.004	-.006	-.020	-.052	-.074	-.110	-.120	.166
.277	.003	-.010	-.013	-.027	-.034	-.059	-.080	-.083	-.073	.277
.367	.102	.074	.050	.026	-.011	-.085	-.167	-.234	-.255	.367
.387	.161	.109	.069	.021	-.031	-.147	-.273	-.395	-.426	.387
.443	.068	.002	-.051	-.111	-.173	-.309	-.466	-.550	-.660	.443
.498	.009	-.049	-.099	-.155	-.214	-.349	-.478	-.560	-.646	.498
.553	-.045	-.095	-.140	-.187	-.240	-.359	-.406	-.558	-.644	.553
.609	-.037	-.075	-.106	-.139	-.173	-.244	-.332	-.462	-.611	.609
.664	-.024	-.049	-.066	-.074	-.092	-.122	-.198	-.356	-.612	.664
.719	-.001	-.015	-.013	-.013	-.019	-.020	-.076	-.189	-.391	.719
.774	.011	.002	.005	.007	.008	.006	-.019	-.071	-.171	.774
.830	-.007	-.007	-.005	.000	.003	.006	-.003	-.029	-.080	.830
.871	-.012	-.015	-.007	-.004	-.001	.006	.002	-.010	-.041	.871
$M = 0.900; q = 358 \text{ lb/sq ft}$										
.166	.029	.012	.002	-.013	-.022	-.051	-.067	-.096	-.105	.166
.277	-.001	-.013	-.019	-.034	-.036	-.047	-.055	-.051	-.036	.277
.367	.122	.091	.068	.044	.025	-.026	-.082	-.122	-.168	.367
.387	.176	.129	.086	.044	.004	-.090	-.184	-.285	-.365	.387
.443	.069	.005	-.055	-.108	-.167	-.271	-.386	-.502	-.642	.443
.498	-.002	-.063	-.120	-.176	-.228	-.347	-.470	-.539	-.682	.498
.553	-.070	-.128	-.198	-.282	-.342	-.446	-.561	-.667	-.848	.553
.609	-.060	-.107	-.151	-.201	-.326	-.481	-.528	-.566	-.626	.609
.664	-.042	-.063	-.080	-.096	-.095	-.215	-.248	-.568	-.648	.664
.719	-.004	-.013	-.012	-.013	-.010	-.001	-.100	-.266	-.452	.719
.774	.008	.002	.005	.005	.012	.021	.059	-.139	-.267	.774
.830	-.013	-.013	-.004	-.004	.004	.013	-.030	-.072	-.180	.830
.871	-.020	-.014	-.010	-.010	-.003	.010	-.006	-.033	-.120	.871
$M = 0.940; q = 368 \text{ lb/sq ft}$										
.166	.029	.009	.000	-.008	-.018	-.051	-.061	-.092	-.098	.166
.277	-.004	-.017	-.024	-.033	-.037	-.049	-.047	-.035	-.015	.277
.367	.131	.102	.079	.060	.043	-.005	-.050	-.078	-.140	.367
.387	.188	.142	.102	.066	.022	-.060	-.147	-.235	-.327	.387
.443	.073	.010	-.045	-.098	-.148	-.248	-.349	-.461	-.569	.443
.498	-.003	-.063	-.117	-.164	-.220	-.331	-.437	-.537	-.652	.498
.553	-.086	-.162	-.236	-.280	-.324	-.426	-.530	-.591	-.632	.553
.609	-.076	-.133	-.222	-.303	-.353	-.470	-.562	-.640	-.672	.609
.664	-.050	-.069	-.081	-.155	-.334	-.494	-.500	-.530	-.680	.664
.719	.002	-.006	-.006	.005	.006	-.062	-.114	-.344	-.399	.719
.774	.011	.007	.009	.017	.028	.022	.066	-.238	-.282	.774
.830	-.014	-.011	-.008	.000	.013	.026	.043	-.105	-.221	.830
.871	-.018	-.014	-.009	-.002	.006	.008	-.019	-.053	-.165	.871
$M = 0.980; q = 385 \text{ lb/sq ft}$										
.166	.038	.018	.007	-.005	-.016	-.038	-.047	-.066	-.064	.166
.277	.002	-.013	-.021	-.031	-.034	-.037	-.022	-.006	.021	.277
.367	.158	.133	.110	.087	.075	.038	.003	-.023	-.076	.367
.387	.216	.170	.133	.102	.060	-.015	-.094	-.171	-.268	.387
.443	.092	.032	-.015	-.062	-.110	-.202	-.292	-.391	-.503	.443
.498	.017	-.044	-.088	-.145	-.192	-.283	-.379	-.475	-.585	.498
.553	-.104	-.159	-.206	-.248	-.296	-.380	-.474	-.558	-.663	.553
.609	-.102	-.187	-.241	-.286	-.337	-.426	-.520	-.607	-.615	.609
.664	-.150	-.217	-.277	-.323	-.372	-.465	-.567	-.653	-.577	.664
.719	-.043	-.051	-.071	-.103	-.166	-.258	-.304	-.267	-.316	.719
.774	.001	.023	.035	.028	.001	-.085	-.130	-.141	-.243	.774
.830	-.016	.010	.026	.033	.032	.004	-.095	-.165	-.244	.830
.871	-.010	.007	.017	.025	.033	.012	-.090	-.201	-.258	.871

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(b) Station B - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
M = 1.030; q = 400 lb/sq ft										
.166	.074	.067	.054	.045	.030	.001	-.023	-.031	-.021	.166
.277	.011	.011	.005	-.005	-.015	-.044	.016	.043	.071	.277
.367	.204	.172	.146	.107	.111	.104	.086	.053	.008	.367
.387	.265	.218	.179	.151	.111	.058	-.026	-.093	-.175	.387
.443	.143	.085	.035	-.007	-.056	-.121	-.213	-.308	-.407	.443
.498	.069	.012	-.041	-.090	-.133	-.209	-.306	-.393	-.487	.498
.553	-.048	-.096	-.146	-.184	-.231	-.300	-.392	-.469	-.565	.553
.609	-.063	-.120	-.181	-.227	-.273	-.352	-.440	-.522	-.625	.609
.664	-.104	-.154	-.217	-.259	-.307	-.393	-.486	-.579	-.684	.664
.719	-.091	-.098	-.123	-.138	-.157	-.217	-.285	-.360	-.429	.719
.774	-.054	-.037	-.028	-.035	-.056	-.110	-.168	-.090	-.089	.774
.830	-.075	-.058	-.050	-.048	-.061	-.084	-.096	-.083	-.181	.830
.871	-.064	-.054	-.060	-.057	-.066	-.102	-.105	-.154	-.194	.871
M = 1.125; q = 421 lb/sq ft										
.166	.047	.037	.033	.019	.002	-.029	-.067	-.119	-.147	.166
.277	.004	.000	-.002	-.017	-.024	-.046	-.081	-.102	-.115	.277
.367	-.035	-.028	-.031	-.022	-.032	-.021	-.009	.031	.116	.367
.387	.220	.178	.150	.110	.074	.009	-.037	-.047	-.051	.387
.443	.141	.091	.057	.012	-.036	-.113	-.183	-.232	-.290	.443
.498	.079	.021	-.019	-.061	-.102	-.181	-.253	-.307	-.359	.498
.553	-.015	-.063	-.100	-.144	-.187	-.255	-.326	-.381	-.437	.553
.609	-.046	-.097	-.135	-.182	-.229	-.296	-.364	-.437	-.491	.609
.664	-.066	-.124	-.164	-.211	-.255	-.336	-.411	-.493	-.534	.664
.719	-.068	-.089	-.106	-.126	-.146	-.168	-.203	-.225	-.146	.719
.774	-.039	-.039	-.041	-.049	-.060	-.080	-.109	.025	.092	.774
.830	-.061	-.056	-.047	-.044	-.048	-.051	-.051	.042	-.030	.830
.871	-.042	-.042	-.037	-.036	-.038	-.066	-.054	.005	-.036	.871
M = 1.200; q = 436 lb/sq ft										
.166	.064	.051	.043	.031	.015	-.016	-.046	-.096	-.133	.166
.277	.020	.014	.001	-.003	-.007	-.026	-.051	-.089	-.121	.277
.367	-.043	-.040	.019	.011	-.049	-.049	-.036	-.055	-.062	.367
.387	.200	.169	.050	.029	.094	.024	-.032	-.088	-.098	.387
.443	.163	.116	.084	.035	-.003	-.086	-.163	-.225	-.281	.443
.498	.101	.059	.026	-.015	-.064	-.144	-.216	-.287	-.353	.498
.553	.023	-.024	-.056	-.099	-.137	-.213	-.284	-.345	-.431	.553
.609	-.018	-.056	-.094	-.128	-.171	-.247	-.323	-.395	-.485	.609
.664	-.057	-.103	-.148	-.188	-.220	-.293	-.370	-.448	-.546	.664
.719	-.071	-.088	-.111	-.122	-.135	-.160	-.185	-.238	-.251	.719
.774	-.042	-.046	-.057	-.063	-.071	-.096	-.147	-.148	-.188	.774
.830	-.062	-.057	-.056	-.050	-.048	-.049	-.055	-.066	-.046	.830
.871	-.037	-.032	-.030	-.028	-.029	-.048	-.049	-.054	-.024	.871

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(c) Station C

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 310 \text{ lb/sq ft}$										
.055										.055
.166	-.007	-.004	-.001	.000	-.006	-.047	-.110	-.191	-.296	.166
.277	-.026	-.020	-.013	-.016	-.025	-.065	-.127	-.206	-.305	.277
.353										.353
.367	.225	.297	.322	.330	.332	.280	.140	-.040	-.179	.367
.692	.032	.031	.036	.042	.047	.043	-.015	-.052	-.226	.692
.719	.009	.004	.009	.013	.017	.022	-.010	-.071	-.248	.719
.774	-.006	-.008	-.004	.001	.000	.007	-.016	-.065	-.192	.774
.830	.008	.003	.004	.012	.018	.025	.014	-.018	-.103	.830
.871	.020	.017	.022	.025	.031	.040	.032	.021	-.028	.871
.954	.036	.033	.036	.039	.041	.035	.036	.046	.030	.954
$M = 0.900; q = 358 \text{ lb/sq ft}$										
.055										.055
.166	-.008	-.005	-.002	-.006	-.008	-.045	-.100	-.181	-.274	.166
.277	-.027	-.024	-.020	-.027	-.027	-.058	-.107	-.172	-.258	.277
.353										.353
.367	.261	.305	.333	.334	.342	.318	.223	.078	-.090	.367
.692	.032	.031	.037	.039	.046	.025	-.059	-.153	-.216	.692
.719	.012	.009	.010	.012	.025	.040	-.042	-.171	-.298	.719
.774	-.006	-.006	-.001	-.001	.007	.025	-.063	-.172	-.318	.774
.830	.001	.002	.003	.006	.016	.032	-.018	-.097	-.240	.830
.871	.014	.017	.019	.022	.029	.045	.019	-.022	-.116	.871
.954	.035	.036	.041	.038	.041	.038	.039	.040	.003	.954
$M = 0.940; q = 368 \text{ lb/sq ft}$										
.055										.055
.166	-.005	-.005	-.001	-.002	-.004	-.049	-.095	-.168	-.263	.166
.277	-.025	-.026	-.022	-.026	-.030	-.059	-.099	-.151	-.242	.277
.353										.353
.367	.276	.317	.341	.346	.355	.332	.252	.122	-.035	.367
.692	.031	.035	.040	.043	.015	-.079	-.145	-.168	-.201	.692
.719	.022	.015	.016	.030	.032	-.022	-.077	-.196	-.270	.719
.774	.000	-.002	.004	.011	.021	.021	-.078	-.265	-.330	.774
.830	.000	.002	.003	.012	.025	.034	-.045	-.174	-.306	.830
.871	.014	.016	.020	.027	.038	.049	.001	-.066	-.190	.871
.954	.041	.041	.042	.043	.047	.039	.037	.037	-.010	.954
$M = 0.980; q = 385 \text{ lb/sq ft}$										
.055										.055
.166	.001	.005	-.008	.004	-.001	-.036	-.083	-.146	-.233	.166
.277	-.022	-.021	-.018	-.021	-.030	-.048	-.078	-.126	-.202	.277
.353										.353
.367	.303	.338	.361	.361	.369	.356	.290	.170	.011	.367
.692	-.094	-.095	-.093	-.087	-.109	-.152	-.214	-.207	-.195	.692
.719	-.057	-.045	-.039	-.051	-.101	-.169	-.178	-.088	-.152	.719
.774	-.009	.016	.027	.016	-.011	-.094	-.119	-.153	-.269	.774
.830	.007	.025	.032	.033	.024	-.014	-.136	-.215	-.331	.830
.871	.023	.035	.042	.051	.053	.034	-.071	-.173	-.263	.871
.954	.057	.059	.059	.062	.063	.070	.032	-.063	-.132	.954

TABLE V. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(c) Station C - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 400 \text{ lb/sq ft}$										
.055										.055
.166	.045	.049	.050	.050	.042	.006	-.056	-.109	-.192	.166
.277	-.013	.003	.009	.005	-.006	-.045	-.045	-.077	-.147	.277
.353										.353
.367	.322	.348	.363	.361	.372	.397	.339	.224	.084	.367
.692	-.073	-.063	-.074	-.067	-.072	-.089	-.163	-.182	-.138	.692
.719	-.090	-.072	-.080	-.076	-.084	-.120	-.158	-.158	-.072	.719
.774	-.078	-.049	-.035	-.046	-.066	-.108	-.143	-.073	-.089	.774
.830	-.057	-.047	-.041	-.040	-.058	-.094	-.129	-.147	-.249	.830
.871	-.033	-.029	-.028	-.023	-.038	-.053	-.060	-.138	-.199	.871
.954	-.093	-.085	-.074	-.071	-.084	-.088	-.130	-.209	-.254	.954
$M = 1.125; q = 421 \text{ lb/sq ft}$										
.055										.055
.166	.009	.020	.027	.026	.016	-.024	-.094	-.187	-.291	.166
.277	-.013	-.011	.004	-.004	-.015	-.051	-.127	-.226	-.340	.277
.353										.353
.367	.226	.273	.286	.283	.299	.246	.114	-.035	.089	.367
.692	-.052	-.051	-.045	-.047	-.051	-.060	-.109	-.081	.012	.692
.719	-.065	-.063	-.061	-.065	-.067	-.074	-.089	-.074	.030	.719
.774	-.062	-.058	-.050	-.054	-.060	-.075	-.095	.008	.040	.774
.830	-.044	-.042	-.034	-.035	-.044	-.062	-.089	-.053	-.097	.830
.871	-.013	-.017	-.008	-.008	-.006	-.015	-.017	-.004	-.055	.871
.954	-.030	-.038	-.039	-.049	-.051	-.058	.005	-.065	-.109	.954
$M = 1.200; q = 436 \text{ lb/sq ft}$										
.055										.055
.166	.027	.037	.038	.037	.028	-.013	-.073	-.172	-.276	.166
.277	.003	.005	.003	.003	-.004	-.033	-.104	-.205	-.347	.277
.353										.353
.367	.222	.277	.027	.039	.316	.246	.132	-.064	-.307	.367
.692	-.047	-.041	-.042	-.039	-.035	-.047	-.085	-.084	-.092	.692
.719	-.065	-.059	-.059	-.056	-.053	-.059	-.063	-.083	-.078	.719
.774	-.062	-.057	-.055	-.053	-.057	-.072	-.092	-.108	-.137	.774
.830	-.045	-.040	-.040	-.042	-.049	-.066	-.092	-.151	-.172	.830
.871	-.004	.001	.002	.006	.003	-.013	.035	-.068	-.083	.871
.954	-.076	-.071	-.070	-.072	-.073	-.091	-.114	-.125	-.137	.954

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(d) Station D

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 310 \text{ lb/sq ft}$										
.166	.003	.005	.004	.020	.031	.058	.067	.068	.048	.166
.277										.277
.367	-.010	.023	.054	.081	.103	.145	.178	.220	.240	.367
.387	-.108	-.055	-.003	.045	.086	.163	.233	.296	.346	.387
.443	-.214	-.145	-.080	-.026	.032	.136	.243	.335	.417	.443
.498	-.192	-.134	-.077	-.026	.026	.127	.218	.308	.382	.498
.553	-.148	-.093	-.045	.002	.044	.127	.200	.265	.331	.553
.609	-.130	-.099	-.062	-.026	.006	.070	.123	.163	.211	.609
.664	-.069	-.052	-.032	-.009	.010	.046	.064	.074	.074	.664
.719	-.020	-.018	-.011	.004	.013	.026	.014	-.028	-.124	.719
.774	.001	.004	.008	.020	.022	.030	.015	-.031	-.145	.774
.830	.015	.011	.011	.014	.019	.021	.009	-.020	-.113	.830
.871	-.014	-.016	-.019	-.012	-.013	-.018	-.035	-.053	-.131	.871
$M = 0.900; q = 358 \text{ lb/sq ft}$										
.166	.002	.004	.002	.014	.026	.063	.074	.079	.071	.166
.277										.277
.367	.025	.049	.074	.093	.113	.158	.206	.249	.285	.367
.387	-.084	-.037	.011	.051	.095	.180	.261	.329	.388	.387
.443	-.226	-.157	-.095	-.039	.024	.145	.254	.359	.455	.443
.498	-.218	-.156	-.101	-.044	.013	.125	.226	.324	.419	.498
.553	-.244	-.155	-.084	-.034	.021	.116	.201	.283	.366	.553
.609	-.195	-.133	-.087	-.050	-.011	.067	.120	.183	.252	.609
.664	-.076	-.061	-.042	-.022	.004	.039	.052	.078	.123	.664
.719	-.021	-.016	-.004	.000	.016	.030	-.024	-.098	-.126	.719
.774	.001	.008	.013	.015	.025	.040	-.034	-.138	-.242	.774
.830	.006	.008	.011	.012	.018	.026	-.024	-.102	-.250	.830
.871	-.018	-.021	-.020	-.022	-.017	-.014	-.055	-.116	-.245	.871
$M = 0.940; q = 368 \text{ lb/sq ft}$										
.166	.006	.005	.004	.015	.028	.061	.077	.090	.082	.166
.277										.277
.367	.048	.064	.088	.110	.129	.167	.216	.268	.302	.367
.387	-.055	-.020	.023	.066	.107	.190	.272	.350	.412	.387
.443	-.209	-.158	-.096	-.040	.027	.146	.261	.374	.475	.443
.498	-.217	-.159	-.101	-.046	.011	.125	.229	.338	.441	.498
.553	-.233	-.169	-.131	-.055	.009	.106	.203	.300	.390	.553
.609	-.311	-.241	-.110	-.062	-.021	.048	.123	.201	.279	.609
.664	-.136	-.053	-.040	-.025	-.007	.010	.046	.093	.155	.664
.719	-.002	-.008	-.005	.013	.014	-.017	-.054	-.093	-.095	.719
.774	.011	.011	.014	.026	.037	.030	-.060	-.206	-.245	.774
.830	.005	.007	.010	.016	.024	.024	-.054	-.191	-.308	.830
.871	-.018	-.021	-.023	-.017	-.014	-.020	-.078	-.179	-.427	.871
$M = 0.980; q = 385 \text{ lb/sq ft}$										
.166	.013	.011	.010	.016	.033	.072	.088	.106	.110	.166
.277										.277
.367	.083	.099	.113	.137	.147	.194	.246	.299	.343	.367
.387	-.017	.019	.057	.095	.129	.214	.305	.381	.448	.387
.443	-.175	-.127	-.075	-.021	.039	.165	.289	.404	.510	.443
.498	-.195	-.136	-.079	-.031	.019	.140	.260	.367	.475	.498
.553	-.212	-.161	-.113	-.073	-.015	.111	.224	.331	.428	.553
.609	-.300	-.252	-.199	-.144	-.065	.051	.147	.237	.323	.609
.664	-.323	-.262	-.207	-.150	-.070	.001	.070	.139	.201	.664
.719	-.100	-.071	-.041	-.036	-.087	-.118	-.096	-.029	-.029	.719
.774	.009	.031	.038	.024	-.002	-.070	-.076	-.087	-.158	.774
.830	.021	.033	.038	.036	.026	-.009	-.109	-.162	-.271	.830
.871	.001	.004	.004	-.001	-.006	-.031	-.204	-.316	-.453	.871

TABLE V. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
ON ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(d) Station D - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
M = 1.030; q = 400 lb/sq ft										
.166	.052	.058	.054	.069	.077	.110	.14	.140	.155	.166
.277										.277
.367	.135	.135	.141	.129	.179	.246	.298	.354	.393	.367
.387	.048	.078	.104	.145	.174	.270	.353	.437	.499	.387
.443	-.104	-.068	-.028	.025	.086	.218	.338	.457	.559	.443
.498	-.125	-.080	-.034	.022	.073	.190	.306	.421	.524	.498
.553	-.143	-.105	-.059	-.015	.034	.164	.276	.382	.477	.553
.609	-.228	-.188	-.142	-.092	-.027	.103	.296	.291	.379	.609
.664	-.254	-.203	-.158	-.101	-.041	.061	.226	.198	.267	.664
.719	-.137	-.111	-.100	-.073	-.069	-.062	-.058	-.027	.033	.719
.774	-.062	-.033	-.024	-.032	-.044	-.072	-.070	-.003	.013	.774
.830	-.048	-.035	-.031	-.028	-.041	-.061	-.082	-.062	-.137	.830
.871	-.076	-.077	-.087	-.094	-.114	-.151	-.193	-.271	-.360	.871
M = 1.135; q = 421 lb/sq ft										
.166	.022	.024	.035	.042	.049	.076	.079	.081	.073	.166
.277										.277
.367	.004	-.007	-.007	-.025	-.041	-.066	-.086	.162	.406	.367
.387	.024	.050	.079	.105	.137	.187	.306	.440	.547	.387
.443	-.079	-.047	-.008	.039	.081	.202	.337	.483	.622	.443
.498	-.104	-.059	-.008	.033	.088	.197	.316	.458	.595	.498
.553	-.084	-.054	-.012	.022	.066	.171	.297	.434	.559	.553
.609	-.190	-.151	-.095	-.056	-.011	.121	.239	.364	.470	.609
.664	-.204	-.158	-.109	-.062	-.012	.100	.193	.287	.371	.664
.719	-.123	-.105	-.083	-.065	-.048	-.006	.018	.069	.151	.719
.774	-.052	-.044	-.038	-.035	-.036	-.034	-.034	.076	.128	.774
.830	-.029	-.026	-.017	-.019	-.025	-.029	-.038	.019	-.005	.830
.871	-.056	-.066	-.070	-.085	-.097	-.127	-.150	-.158	-.206	.871
M = 1.200; q = 436 lb/sq ft										
.166	.021	.035	.044	.057	.065	.087	.094	.091	.100	.166
.277										.277
.367	-.025	-.008	.008	.009	-.035	-.054	-.065	-.086	-.098	.367
.387	.037	.046	.012	.030	.140	.162	.208	.314	.467	.387
.443	-.059	-.019	.019	.058	.107	.209	.333	.455	.592	.443
.498	-.074	-.024	.019	.063	.111	.214	.326	.429	.557	.498
.553	-.053	-.013	.017	.055	.097	.195	.291	.410	.531	.553
.609	-.140	-.112	-.072	-.032	.016	.108	.226	.347	.458	.609
.664	-.179	-.138	-.100	-.053	-.001	.104	.216	.300	.377	.664
.719	-.119	-.098	-.078	-.056	-.033	.015	.061	.095	.138	.719
.774	-.062	-.050	-.045	-.039	-.028	-.016	-.012	-.008	.002	.774
.830	-.019	-.013	-.016	-.017	-.015	-.022	-.042	-.054	-.077	.830
.871	-.056	-.058	-.068	-.077	-.094	-.127	-.155	-.207	-.222	.871

TABLE V.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(e) Station E

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 310 \text{ lb/sq ft}$										
.055	.028	.043	.063	.092	.118	.178	.245	.330	.406	.055
.166										.166
.277	-.029	-.032	-.020	-.000	.025	.070	.131	.209	.285	.277
.367	.003	.025	.020	.055	.120	.193	.287	.379	.467	.367
.387	-.084	-.053	-.011	.023	.054	.138	.229	.324	.409	.387
.443	-.185	-.129	-.081	-.032	.021	.118	.217	.306	.394	.443
.498	-.193	-.137	-.087	-.040	.011	.106	.194	.275	.357	.498
.553	-.169	-.122	-.074	-.033	.011	.094	.168	.238	.299	.553
.609	-.127	-.094	-.059	-.024	.008	.071	.128	.175	.217	.609
.664	-.058	-.038	-.016	.007	.031	.070	.094	.111	.127	.664
.719	-.036	-.028	-.020	.007	.006	.029	.026	-.002	-.044	.719
.774	-.001	-.003	.005	.010	.017	.029	.018	-.020	-.086	.774
.830	.003	-.004	.001	.004	.006	.013	.010	-.052	-.130	.830
.871	-.020	-.025	-.027	-.027	-.031	-.036	-.049	-.062	-.104	.871
.954	.060	.055	.052	.052	.048	.038	.030	.030	.012	.954
$M = 0.900; q = 358 \text{ lb/sq ft}$										
.055	.032	.047	.072	.089	.121	.185	.259	.344	.423	.055
.166										.166
.277	-.028	-.030	-.024	-.014	.020	.069	.134	.215	.303	.277
.367	.035	.048	.030	.090	.127	.208	.303	.403	.501	.367
.387	-.062	-.036	.001	.029	.065	.148	.247	.345	.444	.387
.443	-.196	-.140	-.093	-.044	.015	.122	.228	.328	.434	.443
.498	-.230	-.172	-.111	-.060	-.001	.103	.203	.297	.393	.498
.553	-.270	-.181	-.111	-.061	-.011	.086	.171	.257	.341	.553
.609	-.192	-.131	-.085	-.048	-.009	.066	.123	.186	.261	.609
.664	-.064	-.048	-.023	-.004	.023	.068	.087	.115	.167	.664
.719	-.030	-.025	-.015	-.008	.004	.028	-.014	-.052	-.043	.719
.774	-.001	-.002	.003	.005	.020	.035	-.029	-.114	-.172	.774
.830	-.004	-.002	-.002	-.001	.007	.017	-.027	-.130	-.200	.830
.871	-.023	-.027	-.030	-.037	-.035	-.034	-.074	-.122	-.237	.871
.954	.059	.053	.055	.049	.051	.045	.030	.013	-.033	.954
$M = 0.940; q = 368 \text{ lb/sq ft}$										
.055	.038	.053	.075	.097	.126	.185	.259	.354	.436	.055
.166										.166
.277	-.026	-.031	-.025	-.011	.018	.063	.134	.223	.316	.277
.367	.057	.065	.037	.101	.143	.213	.308	.414	.518	.367
.387	-.040	-.018	.009	.042	.076	.158	.256	.356	.462	.387
.443	-.186	-.139	-.091	-.040	.015	.126	.237	.344	.451	.443
.498	-.227	-.170	-.121	-.066	-.008	.100	.207	.313	.411	.498
.553	-.257	-.215	-.155	-.084	-.023	.078	.174	.272	.361	.553
.609	-.305	-.247	-.113	-.062	-.020	.052	.126	.207	.285	.609
.664	-.132	-.042	-.023	-.005	.014	.039	.082	.135	.195	.664
.719	-.014	-.018	-.013	.000	.005	-.010	-.032	-.049	-.007	.719
.774	.005	.002	.005	.016	.028	.018	-.057	-.165	-.162	.774
.830	-.003	-.004	-.002	.004	.014	.010	-.058	-.169	-.195	.830
.871	-.026	-.031	-.030	-.032	-.028	-.042	-.098	-.221	-.367	.871
.954	.059	.058	.056	.057	.052	.044	.032	.006	-.040	.954
$M = 0.980; q = 385 \text{ lb/sq ft}$										
.055	.050	.064	.087	.114	.138	.205	.277	.363	.443	.055
.166										.166
.277	-.017	-.025	-.020	-.007	.019	.073	.152	.242	.346	.277
.367	.097	.100	.067	.131	.161	.237	.339	.445	.554	.367
.387	-.003	.024	.048	.068	.097	.181	.284	.387	.494	.387
.443	-.157	-.108	-.073	-.025	.030	.144	.267	.370	.485	.443
.498	-.208	-.150	-.099	-.055	-.001	.117	.236	.340	.448	.498
.553	-.238	-.190	-.139	-.102	-.046	.086	.200	.301	.400	.553
.609	-.293	-.248	-.196	-.148	-.066	.053	.150	.240	.328	.609
.664	-.298	-.240	-.187	-.128	-.043	.027	.104	.176	.244	.664
.719	-.119	-.081	-.044	-.036	-.082	-.095	-.055	.011	.047	.719
.774	.012	.030	.032	.016	-.009	-.077	-.069	-.071	-.082	.774
.830	.015	.025	.024	.020	.014	-.017	-.102	-.115	-.132	.830
.871	-.004	-.005	-.010	-.018	-.023	-.055	-.233	-.290	-.333	.871
.954	.081	.074	.074	.066	.066	.058	.007	-.209	-.311	.954

TABLE V. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
0.5 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Concluded

(e) Station E - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.050; q = 400 \text{ lb/sq ft}$										
.055	.096	.113	.131	.151	.176	.243	.318	.406	.498	.055
.166										.166
.277	-.009	-.002	.005	.016	.036	.072	.180	.284	.385	.277
.367	.156	.108	.044	.130	.191	.289	.388	.499	.600	.367
.387	.066	.088	.116	.119	.140	.232	.331	.440	.543	.387
.443	-.083	-.052	-.021	.022	.074	.197	.315	.429	.535	.443
.498	-.138	-.096	-.055	-.001	.049	.169	.283	.396	.501	.498
.553	-.163	-.127	-.085	-.043	.009	.133	.248	.354	.452	.553
.609	-.216	-.182	-.138	-.093	-.028	.103	.201	.299	.385	.609
.664	-.225	-.177	-.134	-.079	-.018	.084	.159	.238	.305	.664
.719	-.173	-.129	-.118	-.079	-.068	-.041	-.009	.049	.115	.719
.774	-.062	-.039	-.026	-.040	-.049	-.073	-.056	.021	.057	.774
.830	-.059	-.047	-.040	-.037	-.049	-.062	-.068	-.023	-.040	.830
.871	-.088	-.090	-.101	-.114	-.139	-.170	-.191	-.217	-.248	.871
.954	-.042	-.049	-.053	-.073	-.091	-.107	-.141	-.183	-.213	.954
$M = 1.125; q = 421 \text{ lb/sq ft}$										
.055	.060	.077	.103	.123	.148	.209	.275	.364	.442	.055
.166										.166
.277	-.012	-.014	-.002	.006	.021	.062	.114	.169	.239	.277
.367	-.015	-.014	-.019	-.013	-.005	.045	.088	.219	.596	.367
.387	.021	.014	.025	.021	.020	.050	.215	.409	.579	.387
.443	-.061	-.030	.002	.038	.070	.179	.310	.451	.597	.443
.498	-.099	-.068	-.024	.015	.060	.176	.294	.434	.570	.498
.553	-.131	-.091	-.043	-.008	.036	.147	.271	.409	.535	.553
.609	-.173	-.136	-.091	-.049	-.006	.120	.240	.384	.472	.609
.664	-.182	-.138	-.083	-.042	.006	.122	.220	.321	.405	.664
.719	-.173	-.141	-.104	-.072	-.043	.026	.070	.143	.228	.719
.774	-.054	-.056	-.049	-.048	-.044	-.030	-.014	.081	.169	.774
.830	-.033	-.034	-.027	-.029	-.032	-.021	-.011	.073	.068	.830
.871	-.064	-.081	-.092	-.107	-.122	-.131	-.131	-.105	-.107	.871
.954	.030	.002	.019	-.043	-.056	-.071	-.039	-.058	-.071	.954
$M = 1.200; q = 436 \text{ lb/sq ft}$										
.055	.077	.098	.116	.139	.170	.231	.293	.373	.464	.055
.166										.166
.277	-.005	.005	.013	.023	.040	.078	.134	.183	.257	.277
.367	-.019	-.005	.001	.001	.012	.041	.109	.158	.235	.367
.387	.010	.012	.019	.021	.018	.046	.078	.124	.178	.387
.443	-.029	.001	.031	.066	.104	.209	.305	.417	.552	.443
.498	-.082	-.034	.003	.036	.084	.185	.303	.412	.537	.498
.553	-.102	-.056	-.018	.017	.067	.165	.271	.392	.511	.553
.609	-.139	-.101	-.071	-.028	.020	.122	.224	.359	.464	.609
.664	-.153	-.111	-.061	-.014	.033	.128	.241	.333	.414	.664
.719	-.172	-.137	-.101	-.065	-.025	.049	.122	.169	.229	.719
.774	-.060	-.059	-.056	-.047	-.039	-.011	.018	.034	.082	.774
.830	-.017	-.016	-.015	-.011	-.004	.006	.008	.056	.076	.830
.871	-.067	-.078	-.090	-.095	-.105	-.115	-.110	-.111	-.097	.871
.954	-.031	-.040	-.053	-.058	-.065	-.082	-.087	-.099	-.097	.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE
OF 1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING

(a) Station A

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 627 \text{ lb/sq ft}$										
.055										.055
.166	.046	.026	.010	-.003	-.017	-.029	-.031	-.030	-.044	.166
.277	.029	.009	-.005	-.018	-.031	-.036	-.023	-.010	-.013	.277
.367	.091	.062	.036	.010	-.015	-.060	-.102	-.137	-.160	.367
.387	.103	.064	.027	-.006	-.045	-.107	-.170	-.255	-.281	.387
.415	.075	.028	-.018	-.062	-.109	-.202	-.304	-.394	-.439	.415
.443	.049	-.002	-.052	-.100	-.154	-.262	-.386	-.437	-.472	.443
.498	.038	-.015	-.068	-.120	-.174	-.266	-.346	-.376	-.378	.498
.553	.012	-.034	-.081	-.128	-.176	-.244	-.269	-.331	-.304	.553
.581										.581
.609	-.009	-.034	-.059	-.110	-.144	-.189	-.221	-.300	-.305	.609
.636	-.013	-.042	-.068	-.092	-.117	-.139	-.192	-.285	-.328	.636
.664	-.018	-.038	-.057	-.073	-.090	-.103	-.154	-.262	-.361	.664
.692	-.003	-.018	-.030	-.040	-.052	-.050	-.094	-.191	-.327	.692
.719	.019	.008	-.002	-.010	-.016	-.002	-.039	-.120	-.268	.719
.774	.019	.014	.011	.008	.005	.017	-.006	-.062	-.187	.774
.830	.001	-.000	.002	.003	.002	.009	.000	-.034	-.106	.830
.871	.011	.011	.014	.015	.015	.023	.017	-.004	-.037	.871
.954	.020	.026	.032	.038	.039	.038	.036	.025	.043	.954
$M = 0.900; q = 713 \text{ lb/sq ft}$										
.055										.055
.166	.043	.022	.006	-.008	-.017	-.025	-.027	-.019	-.025	.166
.277	.021	.001	-.014	-.024	-.030	-.025	-.004	.025	.031	.277
.367	.104	.074	.051	.030	.015	-.011	-.034	-.045	-.082	.367
.387	.117	.077	.043	.012	-.014	-.057	-.105	-.174	-.225	.387
.415	.085	.035	-.009	-.053	-.091	-.161	-.234	-.337	-.417	.415
.443	.050	-.004	-.054	-.104	-.150	-.240	-.326	-.419	-.411	.443
.498	.026	-.032	-.088	-.145	-.195	-.280	-.391	-.472	-.417	.498
.553	-.011	-.069	-.131	-.207	-.265	-.347	-.454	-.514	-.424	.553
.581										.581
.609	-.027	-.059	-.093	-.163	-.214	-.299	-.468	-.400	-.360	.609
.636	-.034	-.067	-.099	-.132	-.151	-.244	-.432	-.454	-.385	.636
.664	-.032	-.055	-.074	-.091	-.094	-.142	-.121	-.486	-.393	.664
.692	-.010	-.024	-.035	-.044	-.044	-.019	-.087	-.431	-.418	.692
.719	.014	.004	-.004	-.010	-.006	.029	-.055	-.128	-.279	.719
.774	.015	.012	.009	.008	.013	.041	-.030	-.114	-.272	.774
.830	-.006	-.004	-.002	-.001	.006	.021	-.017	-.069	-.183	.830
.871	.006	.007	.009	.011	.017	.030	.008	-.023	-.103	.871
.954	.018	.025	.032	.038	.042	.041	.033	.023	-.000	.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Continued

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.940; q = 743 \text{ lb/sq ft}$										
.055										.055
.166	.044	.020	.003	-.010	-.017	-.027	-.022	-.009	-.013	.166
.277	.021	-.003	-.018	-.029	-.030	-.024	.007	.041	.054	.277
.367	.117	.085	.063	.045	.036	.014	.003	-.004	-.035	.367
.387	.131	.089	.056	.028	.008	-.029	-.068	-.128	-.177	.387
.415	.096	.043	-.000	-.039	-.070	-.131	-.194	-.292	-.372	.415
.443	.058	-.001	-.050	-.096	-.133	-.216	-.284	-.379	-.461	.443
.498	.025	-.037	-.090	-.141	-.189	-.267	-.364	-.437	-.342	.498
.553	-.028	-.105	-.166	-.215	-.254	-.333	-.419	-.456	-.414	.553
.581										.581
.609	-.041	-.087	-.154	-.269	-.315	-.411	-.499	-.276	-.489	.609
.636	-.051	-.094	-.132	-.287	-.343	-.442	-.511	-.465	-.512	.636
.664	-.042	-.065	-.078	-.167	-.341	-.468	-.509	-.438	-.479	.664
.692	-.010	-.023	-.030	-.029	-.087	-.426	-.467	-.443	-.455	.692
.719	.019	.008	.001	.006	.010	-.013	-.039	-.319	-.365	.719
.774	.019	.013	.011	.016	.032	.055	-.008	-.214	-.273	.774
.830	-.005	-.006	-.004	.002	.018	.041	-.017	-.096	-.254	.830
.871	.006	.006	.007	.011	.025	.044	.005	-.049	-.150	.871
.954	.023	.027	.032	.038	.048	.054	.039	.017	-.033	.954
$M = 0.980; q = 771 \text{ lb/sq ft}$										
.055										.055
.166	.048	.028	.014	-.001	-.011	-.018	-.010			.166
.277	.023	.001	-.012	-.023	-.026	-.012	.027			.277
.367	.139	.112	.094	.078	.067	.052	.046			.367
.387	.154	.118	.090	.063	.043	.012	-.023			.387
.415	.117	.071	.032	-.004	-.036	-.084	-.151			.415
.443	.076	.024	-.021	-.062	-.102	-.168	-.233			.443
.498	.037	-.014	-.063	-.119	-.163	-.233	-.320			.498
.553	-.044	-.095	-.138	-.188	-.230	-.297	-.373			.553
.581										.581
.609	-.069	-.125	-.211	-.258	-.299	-.385	-.461			.609
.636	-.112	-.177	-.235	-.286	-.331	-.409	-.491			.636
.664	-.145	-.203	-.253	-.308	-.356	-.436	-.519			.664
.692	-.138	-.201	-.254	-.301	-.345	-.444	-.541			.692
.719	-.012	-.017	-.062	-.108	-.181	-.336	-.500			.719
.774	.013	.037	.047	.041	.025	-.054	-.091			.774
.830	-.003	.017	.033	.040	.043	.027	-.012			.830
.871	.012	.026	.036	.043	.051	.061	.020			.871
.954	.032	.043	.057	.065	.075	.091	.075			.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Continued

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 803 \text{ lb/sq ft}$										
.055										.055
.166	.089	.068	.056	.041	.032	.014	.016			.166
.277	.033	.013	.007	-.008	-.014	-.026	.067			.277
.367	.189	.152	.128	.113	.107	.115	.114			.367
.387	.208	.166	.136	.112	.095	.078	.047			.387
.415	.174	.122	.081	.048	.022	-.012	-.079			.415
.443	.134	.074	.030	-.008	-.042	-.094	-.157			.443
.498	.098	.038	-.019	-.068	-.105	-.162	-.250			.498
.553	.019	-.035	-.086	-.131	-.167	-.226	-.298			.553
.581										.581
.609	-.033	-.077	-.153	-.201	-.232	-.309	-.392			.609
.636	-.061	-.121	-.184	-.227	-.264	-.338	-.414			.636
.664	-.091	-.145	-.204	-.249	-.287	-.365	-.440			.664
.692	-.106	-.153	-.204	-.244	-.281	-.377	-.462			.692
.719	-.078	-.106	-.138	-.160	-.190	-.305	-.444			.719
.774	-.043	-.038	-.025	-.039	-.053	-.087	-.116			.774
.830	-.069	-.063	-.049	-.053	-.058	-.070	-.072			.830
.871	-.054	-.049	-.041	-.044	-.046	-.046	-.030			.871
.954	-.141	-.124	-.089	-.066	-.050	-.038	-.049			.954
$M = 1.125; q = 856 \text{ lb/sq ft}$										
.055										.055
.166	.058	.044	.034	.018	.002	-.009	-.015			.166
.277	.028	.017	.006	-.007	-.015	-.025	-.023			.277
.367	-.013	-.019	-.024	-.026	-.026	-.016	.007			.367
.387	.113	.086	.070	.056	.047	.032	.045			.387
.415	.164	.124	.096	.063	.032	-.021	-.052			.415
.443	.132	.087	.053	.017	-.017	-.076	-.111			.443
.498	.099	.047	.007	-.038	-.078	-.130	-.189			.498
.553	.039	-.013	-.052	-.093	-.127	-.184	-.231			.553
.581										.581
.609	-.015	-.052	-.120	-.166	-.191	-.247	-.297			.609
.636	-.047	-.099	-.139	-.181	-.214	-.273	-.322			.636
.664	-.061	-.117	-.156	-.196	-.232	-.297	-.351			.664
.692	-.066	-.112	-.153	-.199	-.238	-.307	-.370			.692
.719	-.063	-.103	-.134	-.168	-.198	-.277	-.360			.719
.774	-.027	-.033	-.038	-.040	-.046	-.054	-.077			.774
.830	-.051	-.045	-.043	-.038	-.037	-.034	-.030			.830
.871	-.036	-.031	-.027	-.021	-.018	-.009	.000			.871
.954	-.080	-.076	-.059	-.037	-.019	-.000	.019			.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station A - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.200; q = 888 \text{ lb/sq ft}$										
.055										.055
.166	.075	.057	.044	.032	.016	-.001	-.004			.166
.277	.040	.023	.011	.007	.005	-.012	-.008			.277
.367	.004	-.006	-.016	-.020	-.016	-.017	-.022			.367
.387	.038	.029	.028	.034	.032	.029	.043			.387
.415	.169	.131	.101	.069	.039	-.004	-.038			.415
.443	.154	.111	.070	.039	.008	-.053	-.098			.443
.498	.126	.076	.031	-.013	-.054	-.108	-.163			.498
.553	.070	.023	-.022	-.059	-.097	-.157	-.206			.553
.581										.581
.609	.006	-.028	-.062	-.092	-.159	-.219	-.278			.609
.636	-.024	-.068	-.107	-.139	-.179	-.240	-.294			.636
.664	-.037	-.083	-.130	-.171	-.206	-.260	-.311			.664
.692	-.054	-.096	-.134	-.172	-.207	-.270	-.335			.692
.719	-.054	-.097	-.134	-.168	-.205	-.269	-.340			.719
.774	-.048	-.057	-.059	-.064	-.069	-.069	-.083			.774
.830	-.046	-.050	-.050	-.044	-.040	-.028	-.017			.830
.871	-.043	-.037	-.028	-.018	-.013	.000	.004			.871
.954	-.098	-.086	-.072	-.056	-.042	-.035	-.042			.954

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(b) Station B

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 627 \text{ lb/sq ft}$										
.166	.030	.022	.012	-.001	-.016	-.045	-.077	-.101	-.122	.166
.277	.005	-.002	-.009	-.020	-.035	-.059	-.076	-.086	-.100	.277
.367	.108	.084	.057	.029	-.008	-.083	-.163	-.235	-.265	.367
.387	.158	.114	.068	.020	-.035	-.147	-.270	-.405	-.444	.387
.443	.070	.011	-.046	-.105	-.169	-.306	-.466	-.547	-.629	.443
.498	.012	-.041	-.093	-.146	-.206	-.341	-.465	-.560	-.587	.498
.553	-.040	-.086	-.131	-.177	-.230	-.351	-.397	-.514	-.614	.553
.609	-.029	-.062	-.094	-.127	-.163	-.235	-.314	-.433	-.607	.609
.664	-.021	-.039	-.055	-.071	-.088	-.113	-.191	-.349	-.649	.664
.719	.005	-.001	-.005	-.010	-.016	-.015	-.070	-.180	-.378	.719
.774	.016	.013	.013	.011	.008	.010	-.007	-.051	-.150	.774
.830	-.001	-.000	.002	.003	.003	.007	-.000	-.021	-.073	.830
.871	-.010	-.009	-.005	-.004	-.003	.007	-.001	-.007	-.040	.871
$M = 0.900; q = 713 \text{ lb/sq ft}$										
.166	.027	.018	.007	-.005	-.016	-.041	-.072	-.087	-.103	.166
.277	-.000	-.010	-.018	-.027	-.034	-.048	-.057	-.053	-.059	.277
.367	.120	.095	.071	.048	.024	-.029	-.085	-.125	-.173	.367
.387	.177	.130	.086	.041	-.001	-.089	-.191	-.291	-.375	.387
.443	.071	.010	-.048	-.107	-.161	-.270	-.394	-.508	-.510	.443
.498	.002	-.057	-.113	-.169	-.220	-.341	-.473	-.557	-.580	.498
.553	-.065	-.124	-.186	-.269	-.331	-.445	-.563	-.670	-.628	.553
.609	-.053	-.094	-.137	-.185	-.292	-.477	-.520	-.501	-.605	.609
.664	-.036	-.056	-.073	-.089	-.092	-.170	-.207	-.560	-.640	.664
.719	.003	-.003	-.006	-.008	-.005	.010	-.082	-.232	-.421	.719
.774	.012	.011	.011	.011	.014	.027	-.038	-.124	-.222	.774
.830	-.008	-.006	-.003	.000	.005	.016	-.017	-.059	-.155	.830
.871	-.016	-.012	-.010	-.007	-.001	.013	-.006	-.024	-.105	.871
$M = 0.940; q = 743 \text{ lb/sq ft}$										
.166	.029	.016	.005	-.006	-.015	-.042	-.066	-.080	-.091	.166
.277	-.001	-.014	-.023	-.031	-.035	-.047	-.045	-.036	-.037	.277
.367	.135	.106	.083	.061	.043	-.003	-.045	-.078	-.121	.367
.387	.191	.143	.101	.060	.023	-.059	-.148	-.238	-.324	.387
.443	.078	.013	-.043	-.097	-.140	-.243	-.345	-.459	-.568	.443
.498	.000	-.061	-.112	-.163	-.213	-.322	-.431	-.533	-.516	.498
.553	-.085	-.165	-.228	-.275	-.316	-.424	-.520	-.563	-.591	.553
.609	-.072	-.129	-.213	-.298	-.346	-.464	-.563	-.666	-.674	.609
.664	-.046	-.065	-.076	-.153	-.343	-.494	-.519	-.534	-.669	.664
.719	.009	.003	-.001	.008	.009	-.059	-.116	-.302	-.369	.719
.774	.018	.013	.013	.019	.032	.033	-.032	-.211	-.236	.774
.830	-.008	-.007	-.004	.001	.016	.034	-.024	-.101	-.207	.830
.871	-.015	-.013	-.011	-.006	.008	.018	-.007	-.049	-.154	.871
$M = 0.980; q = 771 \text{ lb/sq ft}$										
.166	.035	.025	.016	-.003	-.008	-.033	-.054			.166
.277	.002	-.009	-.016	-.024	-.031	-.037	-.026			.277
.367	.158	.134	.115	.094	.075	.036	.000			.367
.387	.216	.172	.135	.095	.059	-.015	-.098			.387
.443	.094	.036	-.013	-.061	-.108	-.197	-.294			.443
.498	.012	-.038	-.083	-.138	-.186	-.282	-.378			.498
.553	-.107	-.157	-.195	-.244	-.290	-.381	-.468			.553
.609	-.107	-.181	-.231	-.281	-.330	-.427	-.517			.609
.664	-.157	-.216	-.272	-.319	-.363	-.466	-.574			.664
.719	-.036	-.028	-.052	-.084	-.148	-.262	-.331			.719
.774	.012	.036	.045	.037	.018	-.076	-.141			.774
.830	-.006	.016	.031	.036	.039	.017	-.043			.830
.871	-.007	.008	.020	.027	.036	.021	-.034			.871

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(b) Station B - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 803 \text{ lb/sq ft}$										
.166	.076	.065	.059	.045	.035	.001	-.027			.166
.277	.014	.004	.003	-.009	-.018	-.048	.015			.277
.367	.207	.171	.148	.126	.115	.099	.069			.367
.387	.268	.218	.177	.142	.111	.052	-.025			.387
.443	.151	.085	.035	-.010	-.047	-.121	-.217			.443
.498	.073	.016	-.039	-.087	-.125	-.207	-.297			.498
.553	-.043	-.094	-.142	-.184	-.223	-.303	-.387			.553
.609	-.061	-.121	-.178	-.222	-.262	-.351	-.437			.609
.664	-.106	-.160	-.217	-.257	-.297	-.395	-.493			.664
.719	-.088	-.099	-.114	-.127	-.149	-.221	-.291			.719
.774	-.050	-.041	-.026	-.041	-.057	-.109	-.159			.774
.830	-.074	-.067	-.051	-.056	-.062	-.083	-.089			.830
.871	-.066	-.064	-.057	-.061	-.065	-.096	-.090			.871
$M = 1.125; q = 856 \text{ lb/sq ft}$										
.166	.047	.041	.036	.024	.006	-.021	-.058			.166
.277	.012	.010	.006	-.004	-.017	-.043	-.074			.277
.367	-.032	-.019	-.012	-.014	-.020	-.016	-.003			.367
.387	.218	.174	.142	.106	.076	.009	-.033			.387
.443	.143	.096	.060	.015	-.027	-.106	-.180			.443
.498	.075	.019	-.020	-.064	-.102	-.178	-.242			.498
.553	-.017	-.065	-.102	-.140	-.176	-.252	-.323			.553
.609	-.043	-.093	-.132	-.175	-.217	-.297	-.360			.609
.664	-.079	-.135	-.179	-.214	-.251	-.330	-.420			.664
.719	-.067	-.087	-.106	-.124	-.142	-.167	-.191			.719
.774	-.029	-.029	-.034	-.037	-.047	-.075	-.095			.774
.830	-.058	-.048	-.044	-.039	-.042	-.050	-.043			.830
.871	-.044	-.038	-.036	-.032	-.036	-.082	-.053			.871
$M = 1.200; q = 888 \text{ lb/sq ft}$										
.166	.062	.054	.045	.036	.019	-.014	-.045			.166
.277	.020	.013	.009	.005	-.002	-.030	-.053			.277
.367	-.042	-.036	-.034	-.031	-.033	-.037	-.033			.367
.387	.202	.167	.134	.104	.078	.017	-.039			.387
.443	.158	.112	.067	.027	-.012	-.088	-.168			.443
.498	.099	.035	.012	-.026	-.070	-.146	-.216			.498
.553	.023	-.024	-.065	-.102	-.142	-.216	-.282			.553
.609	-.018	-.055	-.092	-.128	-.169	-.244	-.324			.609
.664	-.066	-.112	-.149	-.189	-.227	-.296	-.378			.664
.719	-.068	-.088	-.107	-.121	-.139	-.158	-.181			.719
.774	-.043	-.048	-.052	-.057	-.070	-.096	-.125			.774
.830	-.064	-.059	-.057	-.053	-.052	-.050	-.053			.830
.871	-.044	-.041	-.036	-.030	-.035	-.051	-.042			.871

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued
(c) Station C

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 627 \text{ lb/sq ft}$										
.055										.055
.166	-.004	.005	.009	.004	-.008	-.046	-.109	-.193	-.304	.166
.277	-.023	-.013	-.009	-.013	-.027	-.063	-.122	-.199	-.289	.277
.353										.353
.367	.223	.278	.313	.330	.335	.287	.143	-.068	-.300	.367
.692	.039	.040	.044	.048	.051	.050	.009	-.027	-.168	.692
.719	.014	.014	.015	.018	.020	.026	.007	-.064	-.230	.719
.774	-.001	.000	.002	.002	.005	.010	-.008	-.064	-.178	.774
.830	.019	.021	.018	.022	.028	.038	.033	.008	-.073	.830
.871	.025	.026	.028	.031	.035	.045	.040	.034	-.004	.871
.954	.039	.040	.042	.041	.039	.037	.041	.049	.041	.954
$M = 0.900; q = 713 \text{ lb/sq ft}$										
.055										.055
.166	-.007	.001	.004	.000	-.008	-.041	-.104	-.181	-.281	.166
.277	-.026	-.019	-.017	-.020	-.028	-.056	-.107	-.169	-.246	.277
.353										.353
.367	.257	.298	.320	.337	.349	.326	.227	.057	-.137	.367
.692	.039	.039	.044	.047	.055	.043	-.048	-.113	-.159	.692
.719	.014	.014	.015	.020	.030	.048	-.018	-.150	-.265	.719
.774	-.004	-.001	.001	.004	.011	.030	-.047	-.159	-.310	.774
.830	.015	.017	.014	.019	.029	.049	.008	-.066	-.201	.830
.871	.021	.023	.025	.028	.035	.051	.027	-.007	-.080	.871
.954	.039	.041	.042	.043	.043	.043	.044	.047	.021	.954
$M = 0.940; q = 743 \text{ lb/sq ft}$										
.055										.055
.166	-.007	.000	.001	-.003	-.008	-.043	-.096	-.173	-.276	.166
.277	-.025	-.023	-.022	-.025	-.029	-.056	-.096	-.153	-.226	.277
.353										.353
.367	.276	.310	.327	.344	.358	.341	.260	.101	-.079	.367
.692	.041	.045	.047	.048	.019	-.073	-.159	-.154	-.152	.692
.719	.028	.021	.021	.034	.036	-.016	-.062	-.182	-.238	.719
.774	.004	.000	.003	.011	.026	.031	-.060	-.260	-.323	.774
.830	.016	.015	.013	.020	.037	.056	-.016	-.155	-.282	.830
.871	.022	.023	.023	.028	.042	.058	.014	-.049	-.167	.871
.954	.042	.043	.043	.043	.048	.048	.046	.038	-.001	.954
$M = 0.980; q = 771 \text{ lb/sq ft}$										
.055										.055
.166	-.001	.008	.011	.007	-.001	-.033	-.084			.166
.277	-.021	-.017	-.015	-.019	-.025	-.045	-.079			.277
.353										.353
.367	.301	.332	.350	.363	.375	.365	.294			.367
.692	-.090	-.084	-.080	-.078	-.098	-.147	-.222			.692
.719	-.048	-.023	-.024	-.038	-.084	-.170	-.190			.719
.774	-.001	.026	.035	.024	.004	-.087	-.137			.774
.830	.023	.041	.043	.043	.043	.011	-.103			.830
.871	.032	.042	.050	.053	.059	.047	-.024			.871
.954	.058	.061	.063	.064	.067	.072	.053			.954

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued
(c) Station C - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 803 \text{ lb/sq ft}$										
.055	.042	.049	.055	.050	.042	.002	-.016			.055
.166										.166
.277	-.009	-.004	.005	-.000	-.008	-.050	-.042			.277
.353										.353
.367	.323	.333	.350	.361	.377	.403	.347			.367
.692	-.069	-.062	-.067	-.062	-.061	-.091	-.160			.692
.719	-.085	-.073	-.073	-.073	-.078	-.122	-.154			.719
.774	-.078	-.060	-.039	-.051	-.064	-.111	-.150			.774
.830	-.047	-.043	-.034	-.040	-.046	-.084	-.125			.830
.871	-.031	-.032	-.025	-.029	-.032	-.052	-.056			.871
.954	-.092	-.090	-.077	-.076	-.078	-.089	-.113			.954
$M = 1.125; q = 856 \text{ lb/sq ft}$										
.055	.016	.024	.030	.028	.016	-.022	-.086			.055
.166										.166
.277	-.004	.006	.010	.007	-.006	-.045	-.119			.277
.353										.353
.367	.207	.253	.271	.281	.281	.242	.102			.367
.692	-.045	-.043	-.040	-.039	-.040	-.050	-.091			.692
.719	-.061	-.057	-.059	-.059	-.061	-.070	-.080			.719
.774	-.056	-.046	-.044	-.046	-.051	-.072	-.095			.774
.830	-.030	-.022	-.025	-.025	-.027	-.049	-.082			.830
.871	-.008	-.006	-.005	-.002	-.003	-.015	-.022			.871
.954	-.040	-.050	-.052	-.056	-.058	-.068	-.052			.954
$M = 1.200; q = 888 \text{ lb/sq ft}$										
.055	.032	.038	.041	.041	.026	-.014	-.077			.055
.166										.166
.277	.006	.011	.010	.011	.001	-.033	-.107			.277
.353										.353
.367	.207	.236	.257	.277	.275	.238	.116			.367
.692	-.046	-.045	-.040	-.034	-.033	-.034	-.069			.692
.719	-.062	-.061	-.061	-.058	-.058	-.059	-.062			.719
.774	-.064	-.060	-.055	-.054	-.059	-.072	-.092			.774
.830	-.037	-.033	-.036	-.037	-.043	-.063	-.097			.830
.871	-.002	-.004	-.003	.000	-.002	-.016	-.036			.871
.954	-.078	-.073	-.072	-.072	-.078	-.096	-.121			.954

TABLE VI.- PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(a) Station D

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 6^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 627 \text{ lb/sq ft}$										
.166	.012	.026	.037	.046	.053	.067	.078	.078	.075	.166
.277										.277
.367	-.004	.029	.061	.085	.106	.148	.189	.221	.250	.367
.387	-.104	-.049	.003	.046	.084	.161	.235	.292	.347	.387
.443	-.204	-.135	-.073	-.020	.031	.141	.244	.332	.422	.443
.498	-.186	-.123	-.069	-.020	.026	.128	.222	.302	.384	.498
.553	-.164	-.117	-.070	-.032	.005	.089	.168	.234	.301	.553
.609	-.127	-.091	-.056	-.024	.005	.072	.124	.166	.213	.609
.664	-.085	-.046	-.026	-.010	.007	.047	.067	.074	.081	.664
.719	-.015	-.007	.001	.008	.014	.033	.024	-.018	-.095	.719
.774	.009	.013	.019	.022	.025	.036	.024	-.021	-.123	.774
.830	.018	.021	.023	.026	.025	.031	.024	.000	-.083	.830
.871	-.007	-.009	-.010	-.012	-.013	-.015	-.029	-.029	-.096	.871
$M = 0.900; q = 713 \text{ lb/sq ft}$										
.166	.011	.024	.033	.043	.054	.072	.083	.093	.098	.166
.277										.277
.367	.028	.052	.076	.099	.121	.166	.211	.253	.289	.367
.387	-.080	-.032	.013	.057	.098	.179	.259	.328	.387	.387
.443	-.217	-.149	-.087	-.029	.028	.145	.256	.356	.453	.443
.498	-.212	-.148	-.090	-.034	.018	.127	.228	.320	.415	.498
.553	-.248	-.169	-.107	-.057	-.012	.083	.164	.247	.333	.553
.609	-.175	-.124	-.081	-.043	-.007	.065	.120	.178	.248	.609
.664	-.074	-.055	-.035	-.016	.004	.044	.052	.073	.120	.664
.719	-.015	-.008	.000	.008	.019	.041	-.009	-.082	-.105	.719
.774	.007	.012	.016	.022	.029	.049	-.015	-.114	-.214	.774
.830	.012	.017	.020	.022	.026	.039	-.005	-.072	-.200	.830
.871	-.014	-.013	-.016	-.015	-.014	-.011	-.048	-.104	-.184	.871
$M = 0.940; q = 743 \text{ lb/sq ft}$										
.166	.013	.023	.033	.041	.054	.071	.088	.100	.109	.166
.277										.277
.367	.031	.070	.087	.108	.133	.176	.227	.272	.313	.367
.387	-.035	-.015	.024	.065	.109	.190	.275	.348	.413	.387
.443	-.208	-.148	-.092	-.034	.028	.148	.266	.373	.476	.443
.498	-.212	-.147	-.098	-.046	.014	.124	.234	.336	.437	.498
.553	-.250	-.208	-.157	-.084	-.027	.071	.167	.262	.354	.553
.609	-.312	-.241	-.106	-.063	-.023	.046	.120	.195	.276	.609
.664	-.142	-.049	-.039	-.024	-.014	.005	.043	.091	.152	.664
.719	.002	-.000	.003	.013	.017	-.011	-.044	-.087	-.071	.719
.774	.014	.014	.018	.026	.040	.039	-.041	-.191	-.222	.774
.830	.012	.016	.018	.023	.035	.041	-.031	-.140	-.269	.830
.871	-.013	-.016	-.017	-.016	-.010	-.014	-.070	-.153	-.406	.871
$M = 0.980; q = 771 \text{ lb/sq ft}$										
.166	.019	.033	.043	.052	.062	.079	.099			.166
.277										.277
.367	.084	.102	.119	.137	.156	.199	.253			.367
.387	-.018	.021	.058	.095	.133	.219	.302			.387
.443	-.175	-.122	-.068	-.014	.043	.165	.288			.443
.498	-.192	-.130	-.073	-.027	.021	.136	.254			.498
.553	-.233	-.183	-.140	-.101	-.048	.072	.182			.553
.609	-.301	-.245	-.195	-.141	-.066	.041	.136			.609
.664	-.320	-.263	-.207	-.150	-.071	-.011	.056			.664
.719	-.093	-.047	-.028	-.028	-.071	-.121	-.107			.719
.774	.020	.040	.045	.034	.015	-.070	-.090			.774
.830	.027	.042	.047	.044	.039	.006	-.070			.830
.871	.008	.010	.009	.004	.001	-.026	-.143			.871

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(d) Station D - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 803 \text{ lb/sq ft}$										
.166	.061	.072	.086	.093	.102	.114	.127			.166
.277										.277
.367	.138	.137	.146	.162	.186	.249	.303			.367
.387	.048	.073	.105	.139	.178	.267	.353			.387
.443	-.102	-.067	-.018	.032	.091	.215	.337			.443
.498	-.124	-.082	-.030	.024	.076	.186	.303			.498
.553	-.169	-.136	-.093	-.050	.001	.120	.230			.553
.609	-.226	-.189	-.143	-.087	-.025	.090	.187			.609
.664	-.254	-.200	-.158	-.098	-.048	.046	.115			.664
.719	-.140	-.107	-.091	-.075	-.063	-.066	-.160			.719
.774	-.060	-.045	-.021	-.033	-.041	-.075	-.184			.774
.830	-.044	-.038	-.025	-.028	-.034	-.054	-.075			.830
.871	-.073	-.084	-.085	-.099	-.116	-.156	-.196			.871
$M = 1.125; q = 856 \text{ lb/sq ft}$										
.166	.025	.042	.055	.067	.076	.085	.098			.166
.277										.277
.367	.008	.006	.003	-.006	-.022	-.056	-.075			.367
.387	.027	.055	.077	.102	.125	.189	.311			.387
.443	-.069	-.030	.003	.049	.091	.199	.342			.443
.498	-.097	-.050	-.012	.039	.089	.196	.318			.498
.553	-.131	-.082	-.056	-.010	.031	.125	.257			.553
.609	-.182	-.139	-.099	-.052	-.004	.115	.235			.609
.664	-.193	-.144	-.106	-.059	-.008	.090	.190			.664
.719	-.116	-.095	-.079	-.061	-.042	-.003	.023			.719
.774	-.045	-.034	-.031	-.027	-.026	-.033	-.035			.774
.830	-.020	-.011	-.008	-.009	-.011	-.023	-.036			.830
.871	-.057	-.064	-.073	-.083	-.096	-.130	-.161			.871
$M = 1.200; q = 888 \text{ lb/sq ft}$										
.166	.042	.055	.067	.077	.083	.093	.101			.166
.277										.277
.367	-.006	-.011	-.019	-.022	-.029	-.044	-.057			.367
.387	.038	.062	.081	.100	.123	.165	.215			.387
.443	-.055	-.018	.018	.057	.104	.205	.337			.443
.498	-.078	-.035	.007	.052	.102	.211	.328			.498
.553	-.109	-.068	-.030	.012	.057	.162	.262			.553
.609	-.139	-.113	-.070	-.028	.013	.104	.223			.609
.664	-.180	-.141	-.101	-.054	-.007	.094	.204			.664
.719	-.115	-.097	-.075	-.055	-.035	.013	.064			.719
.774	-.059	-.051	-.045	-.038	-.032	-.020	-.018			.774
.830	-.016	-.014	-.012	-.014	-.018	-.024	-.040			.830
.871	-.055	-.060	-.069	-.082	-.099	-.135	-.166			.871

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Continued

(c) Station E

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 0.800; q = 627 \text{ lb/sq ft}$										
.055	.027	.045	.065	.088	.113	.175	.248	.321	.406	.055
.166										.166
.277	-.023	-.016	-.004	.009	.025	.074	.140	.210	.294	.277
.367	-.002	.029	.065	.102	.138	.225	.317	.399	.490	.367
.387	-.084	-.048	-.013	.022	.055	.138	.232	.319	.414	.387
.443	-.175	-.120	-.070	-.025	.020	.120	.222	.305	.397	.443
.498	-.187	-.131	-.080	-.035	.007	.104	.195	.273	.356	.498
.553	-.164	-.114	-.069	-.028	.011	.096	.174	.236	.304	.553
.609	-.118	-.084	-.049	-.019	.011	.079	.135	.178	.228	.609
.664	-.046	-.026	-.003	.016	.036	.082	.112	.122	.142	.664
.719	-.027	-.020	-.011	-.001	.006	.031	.034	.007	-.031	.719
.774	.002	.005	.010	.013	.017	.032	.026	-.008	-.070	.774
.830	.007	.007	.009	.010	.011	.020	.016	.000	-.043	.830
.871	-.017	-.018	-.022	-.027	-.032	-.036	-.046	-.062	-.100	.871
.954	.058	.057	.055	.051	.047	.040	.034	.039	.024	.954
$M = 0.900; q = 713 \text{ lb/sq ft}$										
.055	.031	.049	.069	.094	.121	.183	.256	.335	.422	.055
.166										.166
.277	-.023	-.019	-.012	.003	.021	.072	.139	.218	.308	.277
.367	.029	.053	.080	.115	.152	.237	.332	.420	.516	.367
.387	-.062	-.034	-.004	.030	.066	.151	.247	.341	.441	.387
.443	-.191	-.134	-.084	-.035	.017	.125	.232	.327	.427	.443
.498	-.225	-.160	-.104	-.052	-.002	.103	.201	.292	.386	.498
.553	-.237	-.169	-.108	-.054	-.005	.091	.173	.250	.336	.553
.609	-.170	-.118	-.076	-.037	-.001	.073	.130	.191	.263	.609
.664	-.056	-.036	-.013	.010	.033	.080	.099	.128	.178	.664
.719	-.028	-.021	-.012	-.002	.010	.035	.001	-.045	-.035	.719
.774	.002	.004	.008	.014	.021	.040	-.013	-.093	-.153	.774
.830	.003	.003	.005	.007	.013	.027	-.012	-.068	-.158	.830
.871	-.022	-.024	-.027	-.031	-.032	-.034	-.070	-.122	-.195	.871
.954	.060	.058	.056	.053	.051	.048	.034	.024	-.012	.954
$M = 0.940; q = 743 \text{ lb/sq ft}$										
.055	.034	.052	.073	.094	.126	.187	.262	.343	.437	.055
.166										.166
.277	-.023	-.022	-.015	-.004	.019	.070	.142	.225	.320	.277
.367	.056	.073	.095	.124	.163	.245	.342	.437	.536	.367
.387	-.039	-.018	.006	.037	.077	.160	.259	.359	.463	.387
.443	-.180	-.134	-.086	-.038	.019	.129	.242	.340	.451	.443
.498	-.225	-.163	-.118	-.066	-.008	.101	.208	.307	.409	.498
.553	-.258	-.210	-.150	-.084	-.022	.080	.178	.268	.359	.553
.609	-.300	-.237	-.105	-.040	-.017	.055	.132	.206	.288	.609
.664	-.135	-.031	-.017	.001	.018	.048	.091	.143	.207	.664
.719	-.007	-.013	-.009	.001	.008	-.005	-.027	-.039	-.002	.719
.774	.009	.006	.010	.017	.031	.029	-.040	-.151	-.151	.774
.830	.003	.002	.004	.008	.020	.026	-.039	-.156	-.189	.830
.871	-.024	-.026	-.030	-.033	-.030	-.037	-.091	-.176	-.370	.871
.954	.061	.059	.058	.055	.055	.047	.034	.012	-.023	.954
$M = 0.980; q = 771 \text{ lb/sq ft}$										
.055	.048	.067	.089	.112	.138	.200	.277			.055
.166										.166
.277	-.016	-.016	-.008	.004	.022	.075	.155			.277
.367	.096	.110	.131	.156	.186	.266	.365			.367
.387	-.002	.017	.040	.067	.099	.181	.285			.387
.443	-.149	-.106	-.062	-.016	.033	.145	.265			.443
.498	-.205	-.151	-.096	-.050	-.002	.111	.229			.498
.553	-.235	-.184	-.138	-.096	-.042	.081	.195			.553
.609	-.287	-.237	-.189	-.138	-.083	.048	.147			.609
.664	-.285	-.228	-.174	-.117	-.034	.032	.103			.664
.719	-.110	-.058	-.032	-.028	-.071	-.103	-.070			.719
.774	.022	.037	.038	.024	.006	-.082	-.090			.774
.830	.024	.032	.033	.029	.023	-.006	-.057			.830
.871	.002	.002	-.004	-.014	-.020	-.049	-.169			.871
.954	.081	.079	.076	.071	.068	.062	.028			.954

TABLE VI. - PRESSURE COEFFICIENTS AT STAGNATION PRESSURE OF
1.0 ATMOSPHERE FOR BODY IN PRESENCE OF WING - Concluded
(e) Station E - Concluded

x/l	$\alpha = -4^\circ$	$\alpha = -2^\circ$	$\alpha = 0^\circ$	$\alpha = 2^\circ$	$\alpha = 4^\circ$	$\alpha = 8^\circ$	$\alpha = 12^\circ$	$\alpha = 16^\circ$	$\alpha = 20^\circ$	x/l
$M = 1.030; q = 803 \text{ lb/sq ft}$										
.055	.093	.106	.128	.150	.177	.239	.315			.055
.166										.166
.277	-.007	-.003	.014	.022	.039	.073	.184			.277
.367	.153	.147	.156	.175	.210	.314	.412			.367
.387	.064	.070	.088	.111	.144	.234	.334			.387
.443	-.079	-.052	-.012	.030	.083	.196	.315			.443
.498	-.136	-.099	-.053	-.001	.052	.161	.278			.498
.553	-.163	-.128	-.086	-.040	.012	.129	.244			.553
.609	-.213	-.179	-.134	-.084	-.024	.098	.199			.609
.664	-.220	-.169	-.126	-.063	-.014	.088	.162			.664
.719	-.174	-.130	-.112	-.084	-.062	-.046	-.013			.719
.774	-.060	-.052	-.027	-.041	-.050	-.079	-.068			.774
.830	-.055	-.053	-.041	-.041	-.046	-.058	-.063			.830
.871	-.086	-.100	-.106	-.124	-.144	-.179	-.194			.871
.934	-.040	-.055	-.055	-.073	-.089	-.106	-.126			.934
$M = 1.125; q = 856 \text{ lb/sq ft}$										
.055	.062	.083	.103	.126	.149	.208	.285			.055
.166										.166
.277	-.003	.002	.012	.027	.041	.075	.126			.277
.367	.002	.007	.014	.028	.041	.078	.139			.367
.387	.019	.024	.027	.030	.032	.046	.210			.387
.443	-.049	-.027	.000	.040	.080	.181	.315			.443
.498	-.098	-.057	-.019	.028	.072	.172	.299			.498
.553	-.125	-.081	-.044	-.000	.043	.143	.276			.553
.609	-.164	-.120	-.083	-.037	.009	.118	.246			.609
.664	-.164	-.119	-.079	-.030	.019	.124	.231			.664
.719	-.168	-.130	-.103	-.070	-.039	.028	.074			.719
.774	-.050	-.045	-.043	-.038	-.036	-.034	-.014			.774
.830	-.027	-.024	-.022	-.020	-.020	-.021	-.006			.830
.871	-.069	-.082	-.097	-.110	-.121	-.141	-.138			.871
.934	.020	-.014	-.027	-.043	-.055	-.074	-.077			.934
$M = 1.200; q = 888 \text{ lb/sq ft}$										
.055	.078	.095	.115	.137	.164	.226	.300			.055
.166										.166
.277	.009	.016	.024	.034	.048	.089	.140			.277
.367	.009	.015	.021	.038	.057	.093	.150			.367
.387	.009	.009	.010	.007	.010	.039	.085			.387
.443	-.035	-.009	.019	.050	.093	.191	.314			.443
.498	-.081	-.043	-.003	.040	.087	.190	.308			.498
.553	-.100	-.063	-.022	.020	.066	.167	.280			.553
.609	-.133	-.107	-.071	-.027	.023	.124	.233			.609
.664	-.146	-.105	-.058	-.007	.040	.136	.239			.664
.719	-.167	-.134	-.101	-.067	-.031	.044	.124			.719
.774	-.061	-.061	-.059	-.053	-.043	-.017	.013			.774
.830	-.016	-.017	-.013	-.011	-.007	.006	.013			.830
.871	-.067	-.079	-.091	-.102	-.113	-.128	-.121			.871
.934	-.034	-.044	-.054	-.062	-.070	-.082	-.088			.934

TABLE VII.- WING SECTION DATA

a, deg	$\frac{y}{b/2} = 0.12$				$\frac{y}{b/2} = 0.25$				$\frac{y}{b/2} = 0.40$							
	c_n		c_m		$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m	
	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm
M = 0.800																
-4	-0.2066	-0.1973	0.0076	0.0075	0.03	0.05	-0.2268	-0.2262	-0.0076	-0.0069	0.06	0.13	-0.2825	-0.2828	-0.0241	-0.0257
-2	-0.0946	-0.0879	-0.0056	-0.0064	-0.01	-0.05	-0.0989	-0.0874	-0.0149	-0.0136	0.04	0.08	-0.1271	-0.1185	-0.0241	-0.0249
0	-0.0221	-0.0258	-0.0186	-0.0185	0	-0.01	-0.0366	-0.0346	-0.0214	-0.0215	0	0	-0.0263	-0.0310	-0.0284	-0.0292
2	-0.1276	-0.1358	-0.0302	-0.0300	-0.01	-0.05	-0.1544	-0.1600	-0.0289	-0.0287	-0.03	-0.07	-0.1613	-0.1714	-0.0339	-0.0350
4	-0.2459	-0.2430	-0.0433	-0.0416	-0.02	-0.09	-0.2858	-0.2836	-0.0364	-0.0358	-0.06	-0.13	-0.3167	-0.3114	-0.0399	-0.0393
8	-0.4710	-0.4733	-0.0661	-0.0651	-0.05	-0.09	-0.5379	-0.5446	-0.0481	-0.0449	-0.12	-0.24	-0.6183	-0.6338	-0.0589	-0.0589
12	-0.7776	-0.6881	-0.0850	-0.0846	-0.06	-0.11	-0.7886	-0.7900	-0.0661	-0.0604	-0.14	-0.28	-1.0187	-1.0301	-0.1371	-0.1391
16	-0.9219	-0.9067	-0.1198	-0.1141	-0.06	-0.12	-1.1074	-1.0970	-0.1423	-0.1279	-0.15	-0.30	-1.0446	-1.0509	-0.1859	-0.1821
20	-1.1304	-1.1340	-0.1572	-0.1480	-0.07	-0.13	-1.1800	-1.1670	-0.1968	-0.1920	-0.17	-0.33	-1.0240	-1.0222	-0.1879	-0.1865
M = 0.900																
-4	-0.2283	-0.2252	0.0155	0.0155	0.03	0.06	-0.2579	-0.2435	-0.0003	-0.0016	0.09	0.17	-0.3279	-0.3134	-0.0133	-0.0210
-2	-0.1039	-0.0948	-0.0032	-0.0041	-0.02	-0.05	-0.1065	-0.0909	-0.0156	-0.0128	-0.09	-0.10	-0.1388	-0.1257	-0.0251	-0.0253
0	-0.0256	-0.0273	-0.0217	-0.0212	0	-0.01	-0.0390	-0.0416	-0.0248	-0.0242	0	-0.01	-0.0294	-0.0335	-0.0326	-0.0329
2	-0.1458	-0.1486	-0.0393	-0.0377	-0.02	-0.05	-0.1768	-0.1762	-0.0380	-0.0356	-0.09	-0.09	-0.1876	-0.1896	-0.0415	-0.0404
4	-0.2705	-0.2682	-0.0581	-0.0559	-0.03	-0.06	-0.3153	-0.3104	-0.0504	-0.0479	-0.09	-0.17	-0.3513	-0.3454	-0.0495	-0.0478
8	-0.5270	-0.5234	-0.1050	-0.1014	-0.06	-0.12	-0.6030	-0.6078	-0.0850	-0.0815	-0.16	-0.33	-0.6831	-0.6849	-0.0737	-0.0733
12	-0.7846	-0.7887	-0.1195	-0.1170	-0.07	-0.14	-0.8322	-0.8328	-0.1056	-0.0989	-0.17	-0.34	-1.0447	-1.0574	-0.1657	-0.1612
16	-0.9371	-0.9257	-0.1534	-0.1504	-0.08	-0.14	-1.1119	-1.1228	-0.1706	-0.1546	-0.19	-0.37	-1.0513	-1.0236	-0.1993	-0.1942
20	-1.1366	-1.1361	-0.1805	-0.1730	-0.08	-0.16	-1.1865	-1.1848	-0.2171	-0.2103	-0.21	-0.41	-1.0802	-1.0761	-0.2068	-0.2054
M = 0.940																
-4	-0.2479	-0.2491	0.0324	0.0341	0.04	0.07	-0.2674	-0.2689	0.0117	0.0102	0.09	0.20	-0.3333	-0.3411	0.0033	-0.0021
-2	-0.1200	-0.1015	-0.0035	-0.0009	-0.02	-0.04	-0.1302	-0.1041	-0.0074	-0.0089	-0.07	-0.12	-0.1691	-0.1359	-0.0182	-0.0230
0	-0.0276	-0.0302	-0.0238	-0.0241	0	-0.01	-0.0435	-0.0440	-0.0285	-0.0276	0	-0.01	-0.0360	-0.0338	-0.0356	-0.0364
2	-0.1536	-0.1645	-0.0506	-0.0521	-0.02	-0.04	-0.1798	-0.1920	-0.0472	-0.0481	-0.05	-0.11	-0.2000	-0.2106	-0.0528	-0.0534
4	-0.2907	-0.2951	-0.0809	-0.0818	-0.04	-0.08	-0.3352	-0.3361	-0.0693	-0.0680	-0.10	-0.21	-0.3818	-0.3808	-0.0739	-0.0734
8	-0.5324	-0.5405	-0.1252	-0.1278	-0.07	-0.14	-0.5919	-0.6090	-0.0988	-0.1006	-0.19	-0.38	-0.6870	-0.7000	-0.1011	-0.0965
12	-0.7318	-0.7432	-0.1427	-0.1437	-0.07	-0.15	-0.8216	-0.8302	-0.1221	-0.1168	-0.19	-0.39	-1.0207	-1.0641	-0.1685	-0.1678
16	-0.9284	-0.9269	-0.1561	-0.1587	-0.08	-0.16	-1.1347	-1.1301	-0.1701	-0.1560	-0.21	-0.42	-1.0804	-1.0666	-0.2073	-0.2022
20	-1.1483	-1.1497	-0.1957	-0.1940	-0.09	-0.18	-1.2858	-1.2859	-0.2250	-0.2229	-0.24	-0.47	-1.1590	-1.1599	-0.2308	-0.2287
M = 0.980																
-4	-0.2365	-0.2275	0.0332	0.0312	0.04	0.08	-0.2703	-0.2632	0.0237	0.0216	0.12	0.23	-0.3335	-0.3253	0.0187	0.0135
-2	-0.1066	-0.0993	-0.0041	-0.0030	-0.02	-0.04	-0.1142	-0.1038	-0.0049	-0.0052	0.07	0.11	-0.1499	-0.1325	-0.0136	-0.0168
0	-0.0189	-0.0211	-0.0215	-0.0215	0	-0.01	-0.0349	-0.0342	-0.0291	-0.0274	0	0	-0.0334	-0.0287	-0.0427	-0.0433
2	-0.1339	-0.1380	-0.0440	-0.0450	-0.02	-0.04	-0.1697	-0.1737	-0.0521	-0.0510	-0.06	-0.11	-0.1892	-0.1936	-0.0666	-0.0676
4	-0.2615	-0.2631	-0.0731	-0.0731	-0.04	-0.09	-0.3187	-0.3196	-0.0770	-0.0758	-0.13	-0.24	-0.3685	-0.3640	-0.0905	-0.0875
8	-0.5039	-0.5021	-0.1181	-0.1170	-0.08	-0.16	-0.5876	-0.5859	-0.1105	-0.1089	-0.23	-0.44	-0.6780	-0.6784	-0.1165	-0.1133
12	-0.7341	-0.7362	-0.1571	-0.1560	-0.09	-0.20	-0.8416	-0.8418	-0.1496	-0.1406	-0.24	-0.53	-0.9915	-1.0182	-0.1692	-0.1693
16	-0.9285	-0.9287	-0.1887	-0.1910	-0.10	-0.20	-1.0829	-1.0829	-0.1577	-0.1506	-0.26	-0.53	-1.3347	-1.3641	-0.2582	-0.2598
20	-1.1325	-1.1325	-0.1975	-0.1975	-0.11	-0.22	-1.2897	-1.2897	-0.2042	-0.2042	-0.28	-0.53	-1.3431	-1.3606	-0.2598	-0.2598
M = 1.030																
-4	-0.2132	-0.2116	0.0269	0.0269	0.04	0.09	-0.2376	-0.2432	0.0173	0.0173	0.12	0.24	-0.2871	-0.2930	0.0104	0.0099
-2	-0.1097	-0.0990	-0.0039	-0.0033	-0.02	-0.04	-0.1209	-0.1032	-0.0017	-0.0051	-0.07	-0.12	-0.1503	-0.1301	-0.0138	-0.0183
0	-0.0169	-0.0198	-0.0204	-0.0204	0	-0.01	-0.0309	-0.0337	-0.0280	-0.0274	0	-0.01	-0.0271	-0.0259	-0.0414	-0.0429
2	-0.1234	-0.1321	-0.0437	-0.0437	-0.02	-0.05	-0.1592	-0.1671	-0.0499	-0.0506	-0.06	-0.13	-0.1767	-0.1863	-0.0644	-0.0659
4	-0.2427	-0.2428	-0.0665	-0.0654	-0.04	-0.08	-0.2982	-0.2967	-0.0723	-0.0699	-0.12	-0.23	-0.3449	-0.3371	-0.0875	-0.0845
8	-0.4728	-0.4743	-0.1116	-0.1109	-0.08	-0.16	-0.5565	-0.5578	-0.1076	-0.1078	-0.22	-0.43	-0.6412	-0.6500	-0.1165	-0.1147
12	-0.7067	-0.7023	-0.1516	-0.1497	-0.11	-0.21	-0.8401	-0.8410	-0.1451	-0.1377	-0.29	-0.59	-0.9279	-0.9472	-0.1602	-0.1508
16	-0.9371	-0.9374	-0.1874	-0.1874	-0.12	-0.22	-1.0666	-1.0666	-0.1807	-0.1807	-0.31	-0.59	-1.3614	-1.3614	-0.2514	-0.2514
20	-1.1422	-1.1422	-0.2204	-0.2204	-0.12	-0.22	-1.2849	-1.2849	-0.2032	-0.2032	-0.32	-0.59	-1.4526	-1.4526	-0.2948	-0.2948
M = 1.125																
-4	-0.2012	-0.1861	0.0241	0.0206	0.04	0.08	-0.2234	-0.2080	0.0181	0.0147	0.12	0.23	-0.2713	-0.2578	0.0117	0.0044
-2	-0.0967	-0.0687	-0.0031	-0.0026	-0.02	-0.05	-0.1042	-0.0735	-0.0035	-0.0100	-0.07	-0.10	-0.1349	-0.0919	-0.0167	-0.0257
0	-0.0146	-0.0204	-0.0194	-0.0206	0	-0.01	-0.0294	-0.0354	-0.0244	-0.0266	0	-0.01	-0.0258	-0.0212	-0.0416	-0.0450
2	-0.1130	-0.1268	-0.0391	-0.0416	-0.02	-0.05	-0.1433	-0.1600	-0.0440	-0.0462	-0.06	-0.12	-0.1620	-0.1793	-0.0639	-0.0665
4	-0.2335	-0.2473	-0.0612	-0.0615	-0.04	-0.08	-0.2748	-0.2761	-0.0669	-0.0660	-0.11	-0.22	-0.3220	-0.3199	-0.0868	-0.0866
8	-0.4408	-0.4422	-0.1035	-0.1026	-0.08	-0.16	-0.5280	-0.5357	-0.1049	-0.1034	-0.22	-0.43	-0.6178	-0.6055	-0.1220	-0.1213
12	-0.6996	-0.6605	-0.1428	-0.1422	-0.11	-0.22	-0.7692	-0.7736	-0.1424	-0.1386	-0.30	-0.59	-0.8921	-0.9022	-0.1546	-0.1551
16	-0.8990	-0.8819	-0.1819	-0.1819	-0.12	-0.22	-1.0907	-1.0907	-0.1894	-0.1894	-0.31	-0.59	-1.2932	-1.2932	-0.2651	-0.2651
20	-1.0610	-1.0610	-0.2101	-0.2101	-0.12	-0.22	-1.2092	-1.2092	-0.1932	-0.1932	-0.32	-0.59	-1.3606	-1.3606	-0.2770	-0.2770
M = 1.200																
-4	-0.1923	-0.1850	0.0236	0.0219	0.04	0.08	-0.2131	-0.2062	0.0147	0.0123	0.12	0.24	-0.2582	-0.2490	0.0089	0.0031
-2	-0.0906	-0.0607	-0.0022	-0.0007	-0.02	-0.04	-0.0975	-0.0883	-0.0048	-0.0069	-0.07	-0.13	-0.1311	-0.1136	-0.0166	-0.0204
0	-0.0081	-0.0150	-0.0156	-0.0162	0	0	-0.0210	-0.0297	-0.0246	-0.0254	-0.01	-0.01	-0.0104	-0.0209	-0.0371	-0.0400
2	-0.1013	-0.1074	-0.0320	-0.0339	-0.02	-0.04	-0.1338	-0.1445	-0.0430	-0.0454	-0.05	-0.11	-0.1448	-0.1574	-0.0566	-0.0593
4	-0.2003	-0.2077	-0.0516	-0.0534	-0.04	-0.08	-0.2535	-0.2629	-0.0636	-0.0661	-0.11	-0.21	-0.2896	-0.2950	-0.0765	-0.0783
8	-0.4045	-0.4122	-0.0924	-0.0924	-0.07	-0.15	-0.4941	-0.5063	-0.1007	-0.1009	-0.21	-0.41	-0.5667	-0.5753	-0.1162	-0.1153
12	-0.6195	-0.6275	-0.1333	-0.1342	-0.11	-0.21	-0.7509	-0.7265	-0.1412	-0.1379	-0.29	-0.58	-0.8460	-0.8588	-0.1584	-0.1567
16	-0.8195	-0.8195	-0.1720	-0.1720	-0.13	-0.22	-0.9459	-0.9459	-0.1843	-0.1843	-0.31	-0.58	-1.0588	-1.0588	-0.2089	-0.2089
20	-1.0172	-1.0172	-0.2062	-0.2062	-0.13	-0.22	-1.1739	-1.1739	-0.2264	-0.2264	-0.36	-0.58	-1.2701	-1.2701	-0.2638	-0.2638

TABLE VII.- WING SECTION DATA - Concluded

a, deg	$\frac{y}{b/2} = 0.60$						$\frac{y}{b/2} = 0.80$						$\frac{y}{b/2} = 0.90$					
	$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m		$\Delta\alpha$, deg		c_n		c_m	
	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm	0.5 atm	1.0 atm
M = 0.800																		
-4	0.17	0.35	-0.4025	-0.4006	-0.0025	0.0031	0.29	0.60	-0.4790	-0.4909	0.0759	-0.0787	0.55	0.75	-0.1956	-0.1875	-0.0049	-0.0036
-2	.11	.21	-.1905	-.1855	-.0551	-.0381	.18	.34	-.5851	-.5456	.0249	.0055	.22	.48	-.2197	-.2776	.0087	.0294
0	-.01	-.02	.0168	.0188	-.0522	-.0528	-.04	-.09	-.0673	-.0645	-.0485	-.0518	-.13	-.25	-.1557	-.1508	-.0462	-.0397
2	-.09	-.19	.1660	.1759	-.0385	-.0387	-.17	-.36	.1568	.1429	-.0490	-.0496	-.26	-.55	.0497	.0586	-.0350	-.0374
4	-.17	-.34	.5442	.5529	-.0416	-.0418	-.29	-.57	.5383	.5292	-.0515	-.0496	-.40	-.78	.2218	.2097	-.0350	-.0354
8	-.50	-.60	.7952	.7876	-.0526	-.0505	-.48	-.99	.5589	.5488	-.0858	-.0866	-.62	-.129	.5089	.5407	-.0540	-.0594
12	-.75	-.71	.8527	.8527	-.1448	-.1406	-.57	-1.14	.5957	.5435	-.0931	-.0910	-.72	-.146	.5261	.5554	-.0425	-.0465
16	-.95	-.76	.8060	.7895	-.1591	-.1352	-.65	-1.24	.5989	.5875	-.1054	-.1012	-.81	-.159	.5862	.5774	-.0510	-.0516
20	-.94	-.86	.8584	.8597	-.1522	-.1492	-.72	-1.42	.6805	.6730	-.1210	-.1202	-.94	-.185	.4537	.4461	-.0626	-.0618
M = 0.900																		
-4	0.23	0.45	-0.4590	-0.4581	-0.0041	-0.0001	0.41	0.78	-0.5684	-0.5519	0.1025	-.0972	0.50	0.96	-0.2004	-0.1966	-0.0045	-0.0057
-2	.15	.26	-.2105	-.1984	-.0520	-.0273	.27	.44	-.4555	-.3691	.0548	.0170	.36	.65	-.2375	-.2865	.0154	.0513
0	-.01	-.03	.0187	.0216	-.0581	-.0557	-.06	-.15	-.0668	-.0600	-.0546	-.0552	-.15	-.35	-.1694	-.1472	-.0428	-.0417
2	-.13	-.25	.2014	.1987	-.0440	-.0428	-.25	-.47	.1756	.1688	-.0568	-.0552	-.37	-.71	.0822	.0775	-.0406	-.0396
4	-.23	-.45	.5979	.5954	-.0442	-.0421	-.38	-.73	.5951	.5715	-.0544	-.0545	-.50	-.97	.2680	.2581	-.0271	-.0320
8	-.42	-.87	.7828	.7820	-.0573	-.0457	-.70	-1.42	.8012	.8788	-.1256	-.1171	-.92	-1.88	.3907	.4366	-.0513	-.0572
12	-.45	-.88	.8256	.8528	-.1507	-.1447	-.73	-1.44	.5955	.5890	-.1090	-.1078	-.95	-1.86	.3699	.5742	-.0486	-.0532
16	-.50	-.96	.8647	.8569	-.1597	-.1512	-.85	-1.57	.6752	.6476	-.1245	-.1199	-1.06	-2.04	.4295	.4164	-.0559	-.0563
20	-.56	-1.08	.9506	.8966	-.1766	-.1681	-.95	-1.79	.7822	.7515	-.1459	-.1396	-1.21	-2.33	.5004	.4846	-.0671	-.0662
M = 0.940																		
-4	0.25	0.54	-0.4519	-0.4435	0.0111	0.0202	0.42	0.94	-0.5511	-0.5681	0.0875	0.1029	0.52	1.17	-0.2485	-0.2459	-0.0024	0.0004
-2	.20	.52	-.2576	-.2128	-.0194	-.0235	.39	.57	-.4590	-.4154	.0794	.0562	.55	.81	-.3095	-.2976	-.0373	.0547
0	-.02	-.04	.0252	.0248	-.0587	-.0563	-.07	-.15	-.0597	-.0602	-.0555	-.0555	-.17	-.36	-.1602	-.1480	-.0406	-.0435
2	-.14	-.30	.2105	.2215	-.0485	-.0478	-.26	-.55	.1855	.1947	-.0542	-.0574	-.38	-.80	.0828	.0927	-.0401	-.0410
4	-.28	-.55	.4277	.4326	-.0650	-.0645	-.46	-.90	.4454	.4272	-.0595	-.0595	-.57	-1.14	.3616	.2758	-.0170	-.0242
8	-.51	-1.00	.8160	.8295	-.1178	-.0859	-.82	-1.65	.9120	.9169	-.1341	-.1298	-1.04	-2.11	.3615	.4218	-.0545	-.0555
12	-.50	-1.00	.8776	.9015	-.1576	-.1554	-.82	-1.67	.6613	.6473	-.1221	-.1248	-1.05	-2.17	.4102	.4245	-.0546	-.0608
16	-.56	-1.10	.9198	.8977	-.1761	-.1681	-.95	-1.85	.7478	.7214	-.1446	-.1413	-1.21	-2.38	.4825	.4607	-.0644	-.0625
20	-.65	-1.24	1.0020	.9712	-.1955	-.1866	-1.07	-2.08	.8458	.8057	-.1651	-.1585	-1.40	-2.74	.5748	.5464	-.0825	-.0785
M = 0.980																		
-4	0.35	0.67	-0.4971	-0.4876	0.0434	0.0419	0.58	1.22	-0.6175	-0.6255	0.1155	0.1202	0.75	1.65	-0.3165	-0.3597	0.0187	0.0560
-2	.19	.26	-.2452	-.2205	-.0086	-.0129	.51	.28	-.4576	-.5577	.0245	-.0536	.44	.58	-.3078	-.2976	.0452	.0585
0	-.01	-.04	.0145	.0118	-.0472	-.0459	-.05	-.15	-.0778	-.0490	-.0634	-.0601	-.05	-.20	-.2262	-.1969	-.0255	.0002
2	-.19	-.35	.2112	.2122	-.0775	-.0726	-.35	-.65	.2550	.2059	-.1057	-.0769	-.59	-.77	.0070	.0440	-.0520	.0041
4	-.39	-.75	.4405	.4145	-.1089	-.0945	-.75	-1.50	.4960	.4864	-.1452	-.1528	-1.15	-2.30	.4124	.4059	-.1071	-.1216
8	-.68	-1.29	.8606	.8514	-.1495	-.1382	-1.25	-2.35	1.0161	.9597	-.2221	-.1857	-1.75	-3.53	.7699	.7850	-.1071	-.1351
12	-.67	-1.44	1.0689	1.1779	-.1965	-.1907	-1.35	-2.56	.9065	.8735	-.1781	-.1701	-1.55	-5.49	.5892	.9278	-.0933	-.1165
16	-.70	-1.68	1.0856		-.2072		-1.20		.8696		-.1851		-1.60		.6289		-.0980	
20	-.77		1.0955		-.2256		-1.55		.9699		-.2015		-1.79		.7157		-.1175	
M = 1.050																		
-4	0.54	0.71	-0.4244	-0.4554	0.0522	0.0400	0.62	1.26	-0.6247	-0.6560	0.0970	0.1002	0.82	1.69	-0.4222	-0.4085	0.0565	0.0408
-2	.20	.30	-.2365	-.2092	-.0156	-.0174	.34	.41	-.4590	-.5654	.0509	-.0274	.45	.49	-.3441	-.3375	.0194	.0175
0	-.02	-.07	.0205	.0225	-.0798	-.0598	-.11	-.30	-.0837	-.0867	-.0840	-.0877	-.25	-.75	-.2460	-.1825	-.0521	-.0908
2	-.21	-.44	.2105	.2166	-.0891	-.0881	-.46	-.95	.1820	.1955	-.1158	-.1121	-.78	-1.58	.1147	.1216	-.1090	-.1100
4	-.57	-.70	.4167	.5992	-.1154	-.1086	-.70	-1.36	.4512	.5982	-.1557	-.1540	-1.05	-2.06	.5136	.2902	-.0995	-.1045
8	-.67	-1.26	.8029	.7824	-.1479	-.1327	-1.25	-2.52	.9191	.8680	-.2040	-.1725	-1.79	-3.36	.7645	.7427	-.1469	-.1491
12	-.85	-1.68	1.1585	1.1545	-.2058	-.1956	-1.52	-5.02	1.1250	1.1015	-.2349	-.2028	-2.11	-4.35	.9718	1.0141	-.1552	-.1950
16	-.85		1.1777		-.2352		-1.42		.9816		-.2026		-1.92		.6970		-.1258	
20	-.86		1.2555		-.2472		-1.48		.9697		-.2105		-2.01		.7569		-.1545	
M = 1.125																		
-4	0.56	0.71	-0.5932	-0.5749	0.0565	0.0555	0.66	1.50	-0.5831	-0.5687	0.0802	0.0758	0.95	1.82	-0.5250	-0.5209	0.0625	0.0613
-2	.22	.26	-.2050	-.1487	-.0128	-.0258	.41	.56	-.4158	-.2857	.0284	-.0537	.59	.18	-.4825	-.4094	.0489	-.0555
0	-.02	-.07	.0060	.0159	-.0538	-.0555	-.10	-.30	-.0585	-.0901	-.0690	-.0755	-.29	-.91	-.1975	-.1595	-.0771	-.1515
2	-.18	-.39	.1726	.1930	-.0786	-.0796	-.41	-.85	.1216	.1527	-.1044	-.1045	-.76	-1.57	.0480	.0435	-.1282	-.1285
4	-.56	-.68	.5716	.5612	-.1088	-.1042	-.70	-1.34	.5825	.5504	-.1555	-.1267	-1.08	-2.11	.2785	.2515	-.1120	-.1145
8	-.66	-1.28	.7316	.7240	-.1464	-.1356	-1.25	-2.40	.8967	.8127	-.1922	-.1957	-1.76	-3.46	.6842	.6559	-.1559	-.1559
12	-.88	-1.75	1.0691	1.0566	-.2224	-.1961	-1.60	-5.19	1.0469	1.0587	-.2162	-.2345	-2.28	-4.56	.9495	.8926	-.1809	-.1725
16	-.85		1.1245		-.2259		-1.46		.9866		-.1958		-1.98		.7009		-.1257	
20	-.88		1.1881		-.2385		-1.55		.9532		-.2062		-2.11		.7629		-.1409	
M = 1.200																		
-4	0.55	0.72	-0.5484	-0.5554	0.0247	0.0185	0.65	1.34	-0.5100	-0.5559	0.0525	0.0414	0.99	2.05	-0.6956	-0.6919	0.1086	0.1052
-2	.20	.35	-.1858	-.1667	-.0250	-.0304	.55	.57	-.5601	-.5310	-.0091	-.0279	.50	.75	-.5557	-.5251	.0401	.0248
0	0	0	-.0004	.0148	-.0540	-.0558	-.05	-.15	-.1307	-.1109	-.0551	-.0627	-.21	-.52	-.2546	-.2549	-.0705	-.0753
2	-.17	-.35	.1688	.1792	-.0818	-.0818	-.37	-.77	.0858	.0951	-.0917	-.0909	-.75	-1.47	.0124	.0275	-.1306	-.1255
4	-.55	-.66	.5444	.5454	-.1085	-.1058	-.67	-1.31	.5145	.5045	-.1215	-.1185	-1.07	-2.11	.2482	.2537	-.1260	-.1202
8	-.62	-1.25	.6807	.6757	-.1491	-.1411	-1.17	-2.35	.7272	.7125	-.1785	-.1855	-1.69	-3.58	.6155	.5651	-.1312	-.1279
12	-.87	-1.70	1.0067	.9749	-.2250	-.1954	-1.60	-5.14	.9836	.9764	-.2215	-.2267	-2.28	-4.50	.9254	.8298	-.1794	-.1657
16	-.80		1.1540		-.2248		-1.80		1.1027		-.2375		-2.54		.9254		-.1794	
20	-.81		1.2121		-.2700		-1.74		1.1768		-.2284		-2.36		.7468		-.1427	

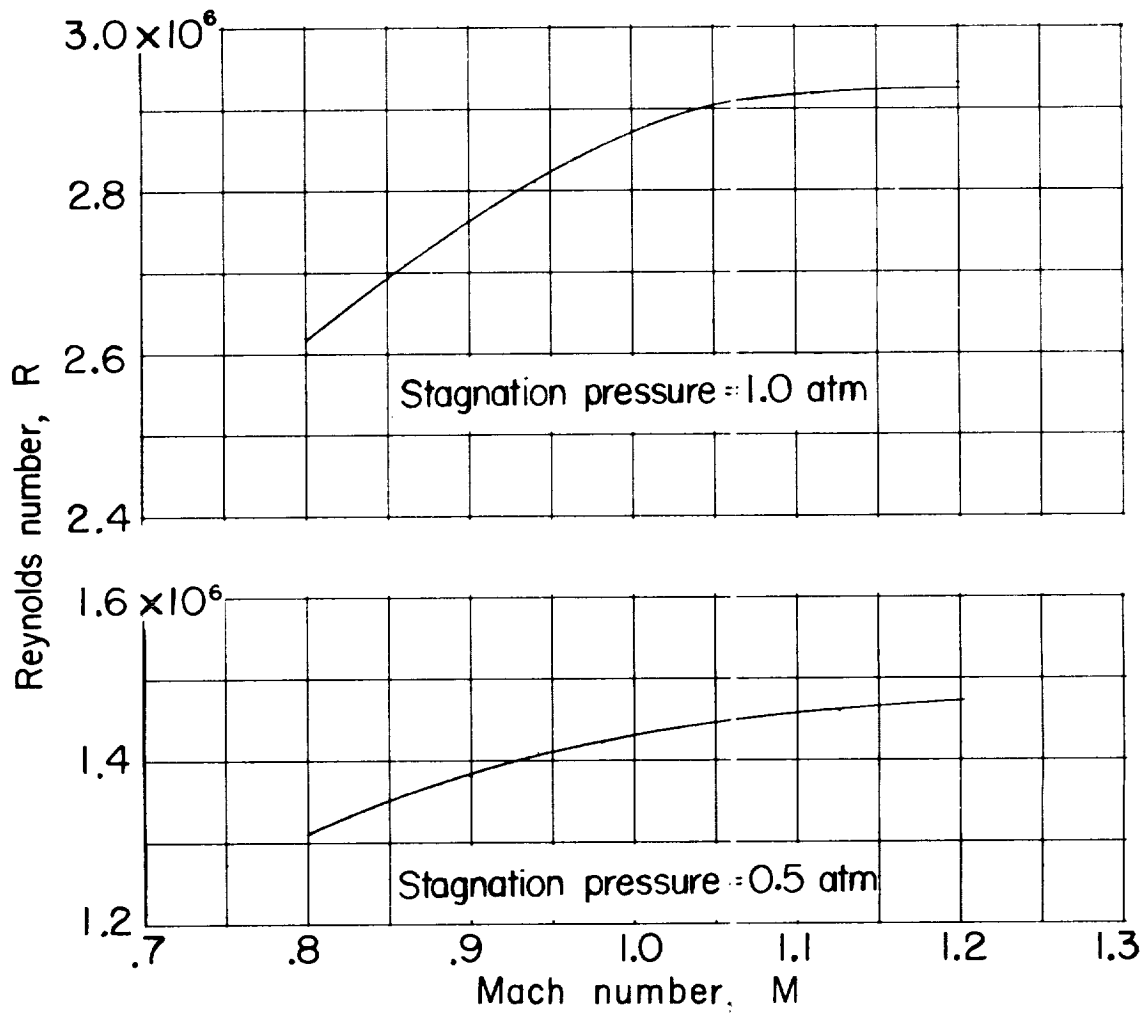


Figure 2.- Variation with Mach number of average Reynolds number based on wing mean aerodynamic chord.

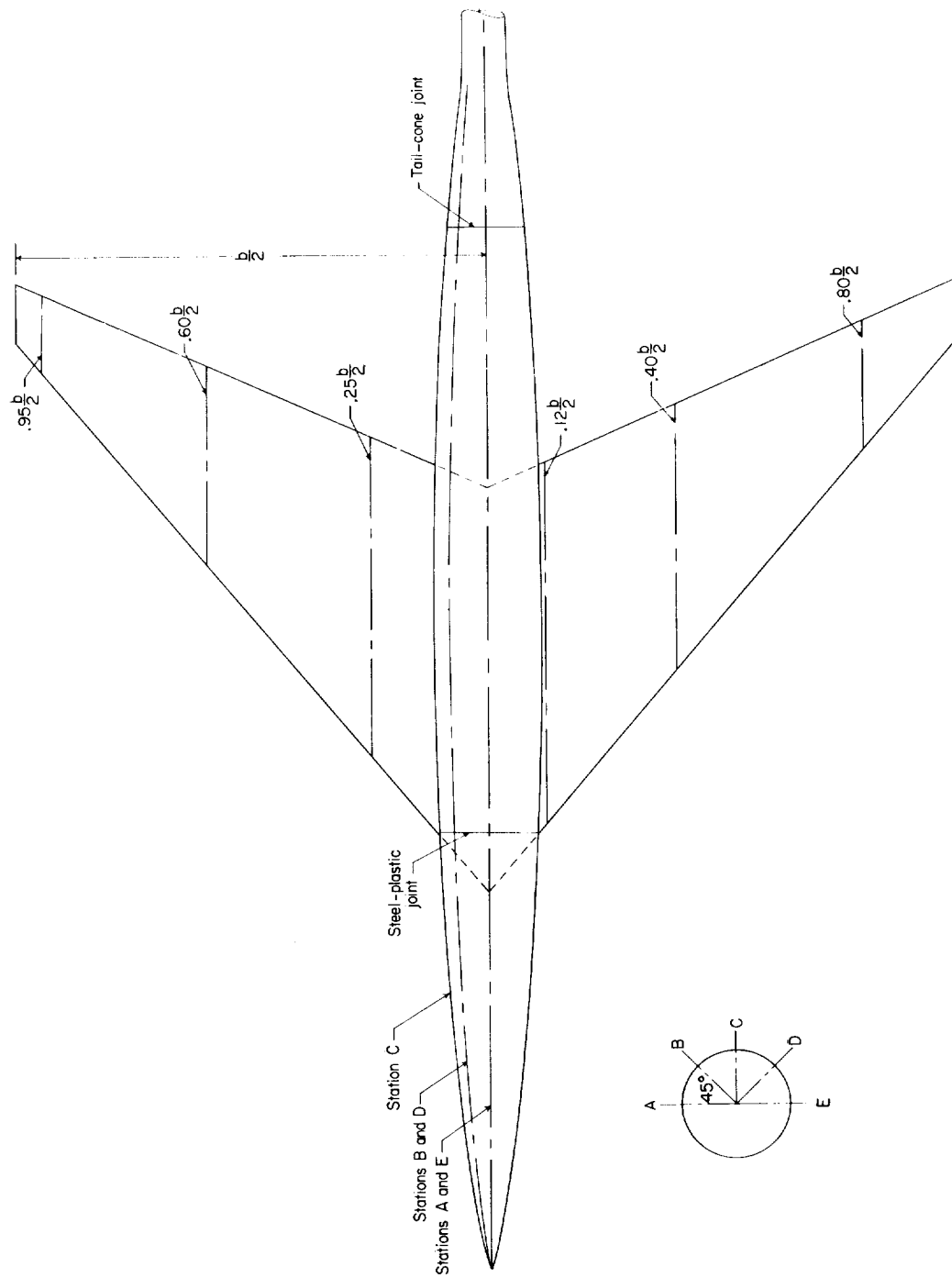
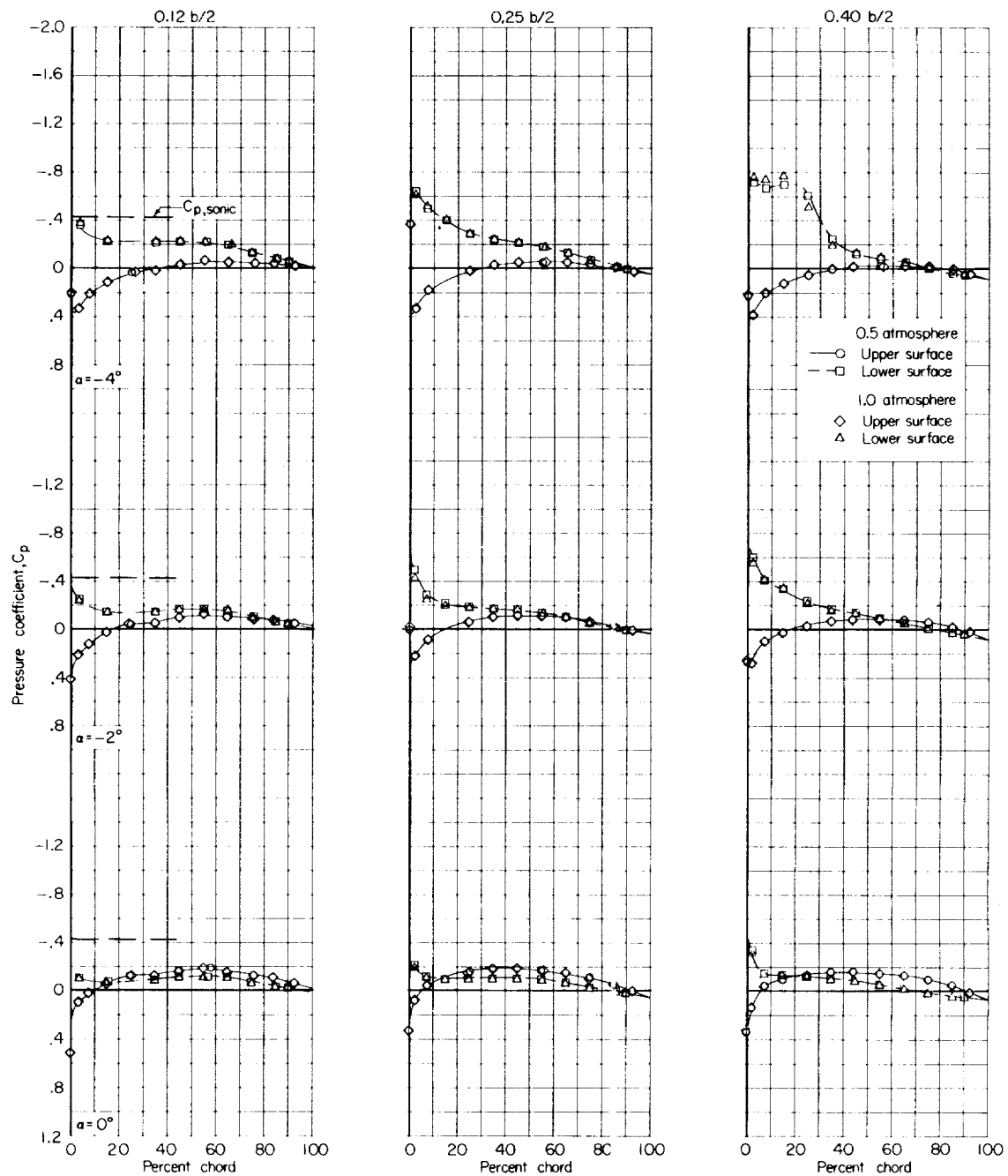
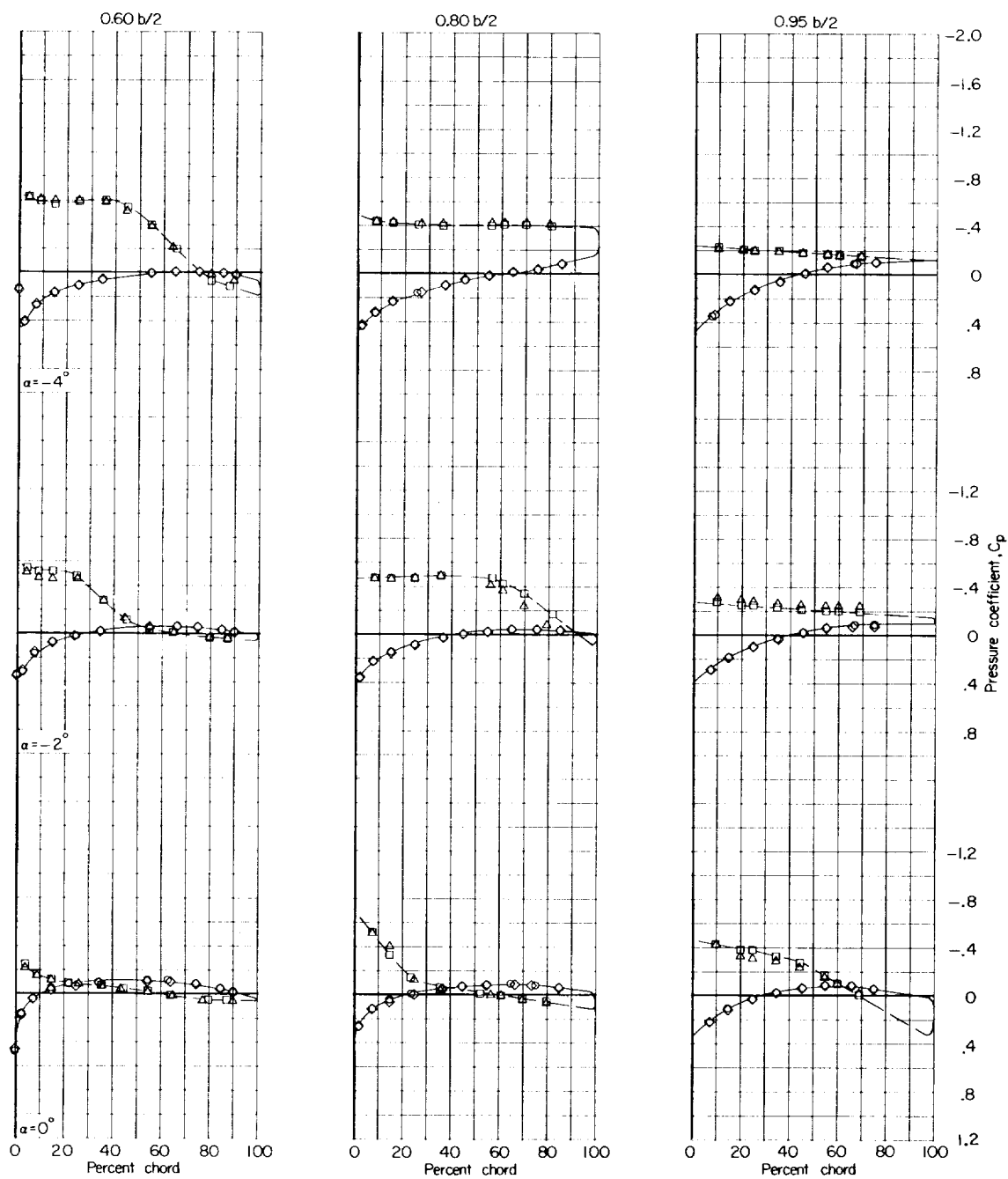


Figure 3.- A sketch of the location of pressure orifices on the wing and body.



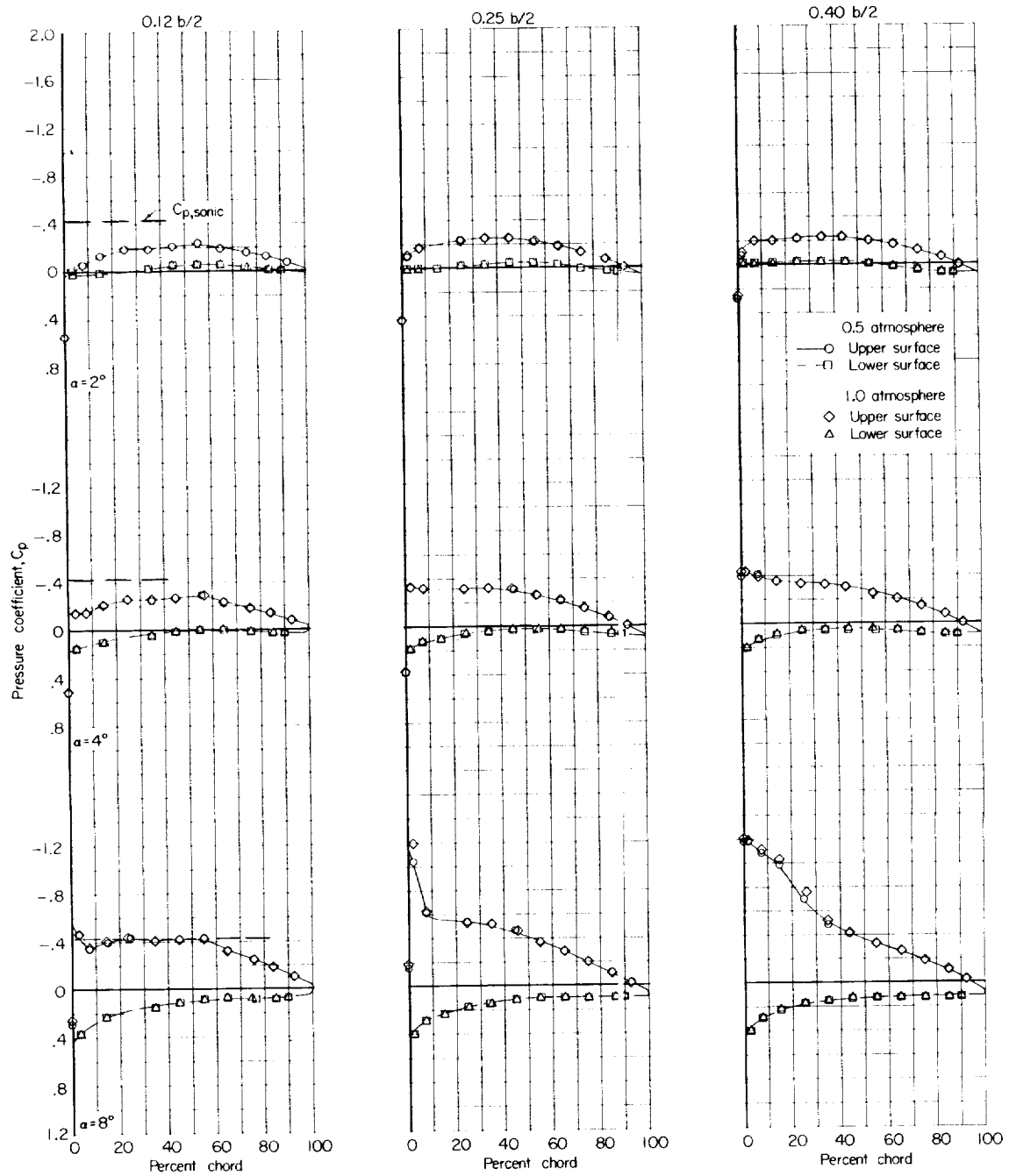
(a) $M = 0.800$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Pressure measurements on the wing in the presence of the body.



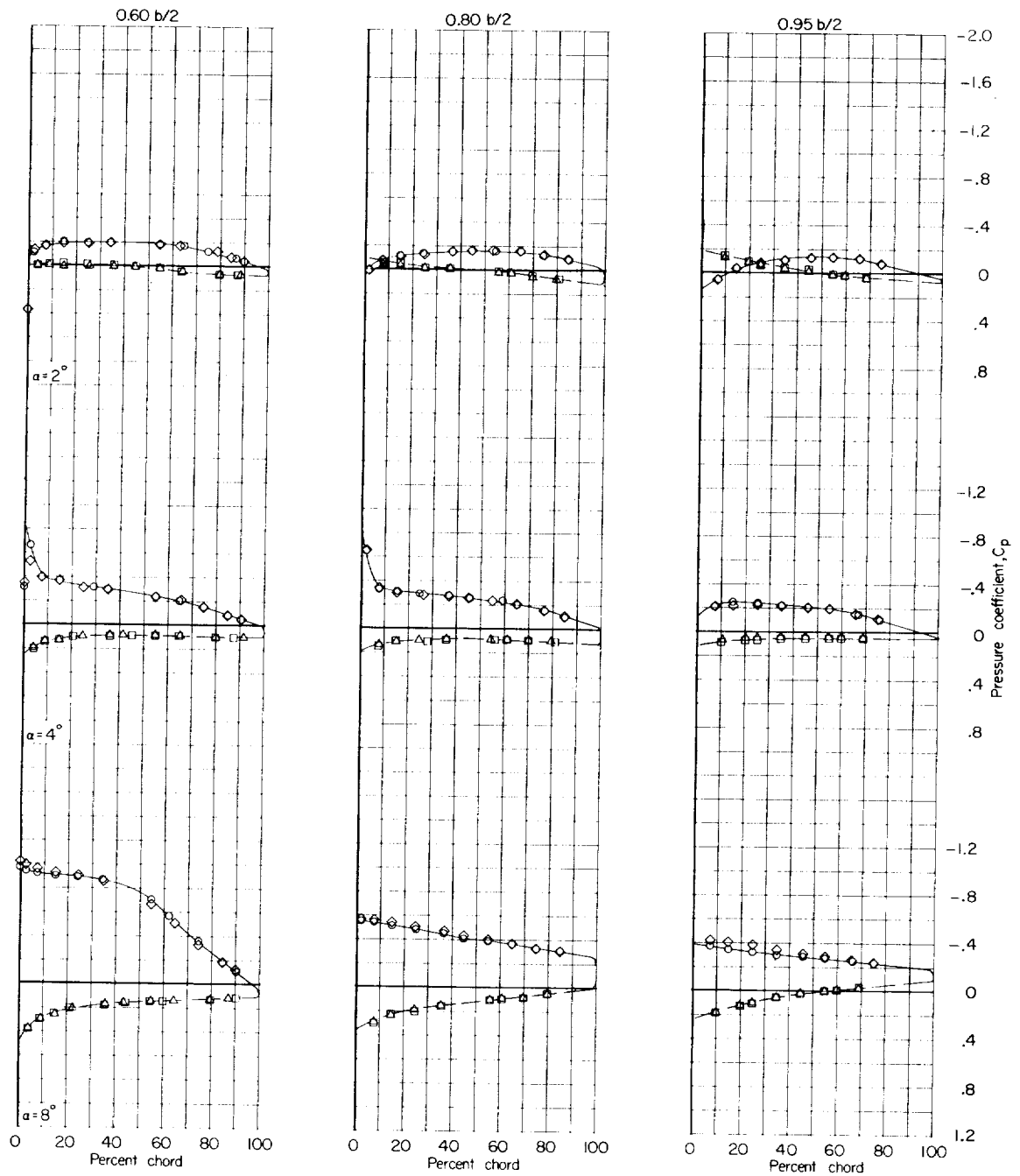
(a) Concluded.

Figure 4.- Continued.



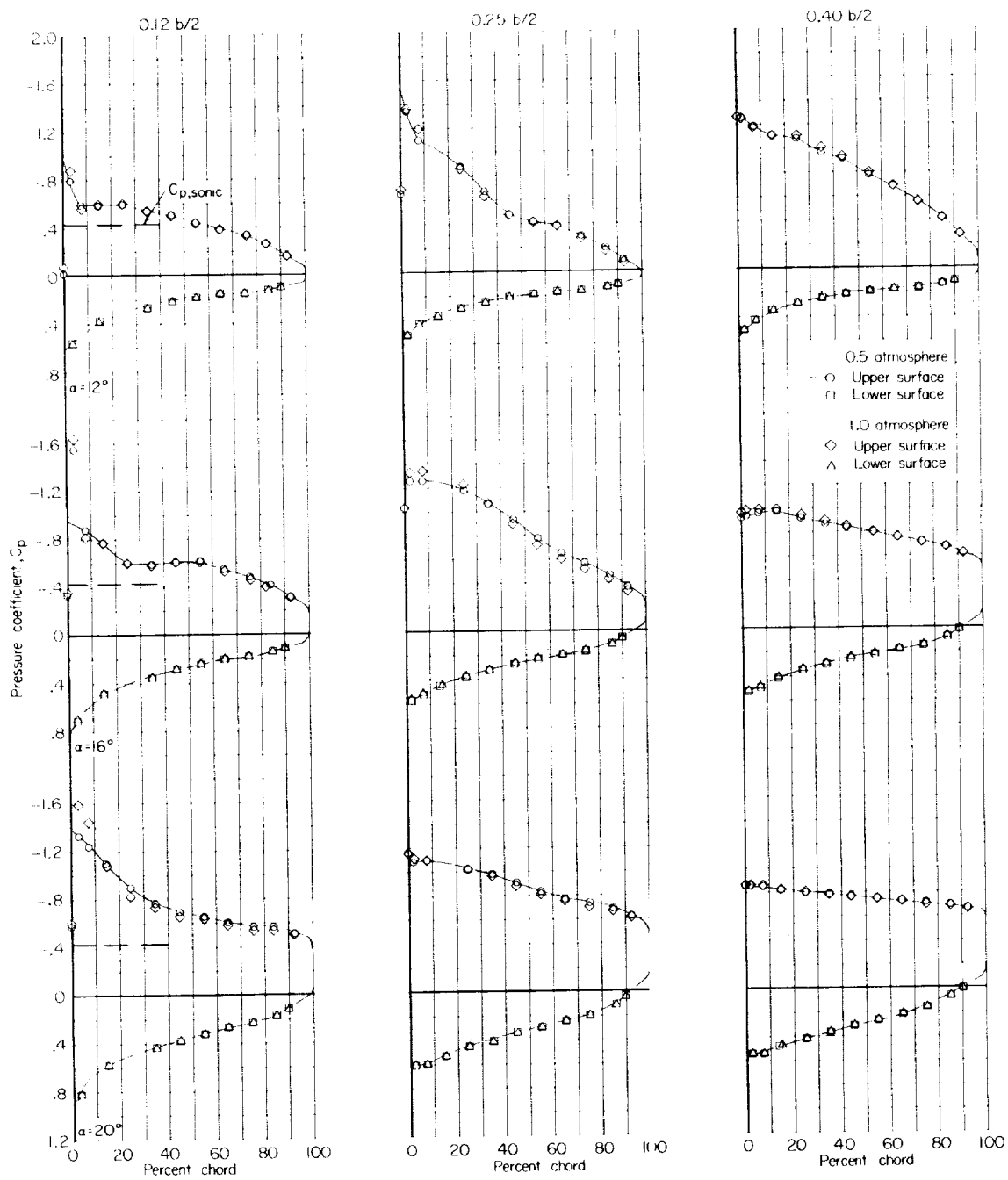
(b) $M = 0.800$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



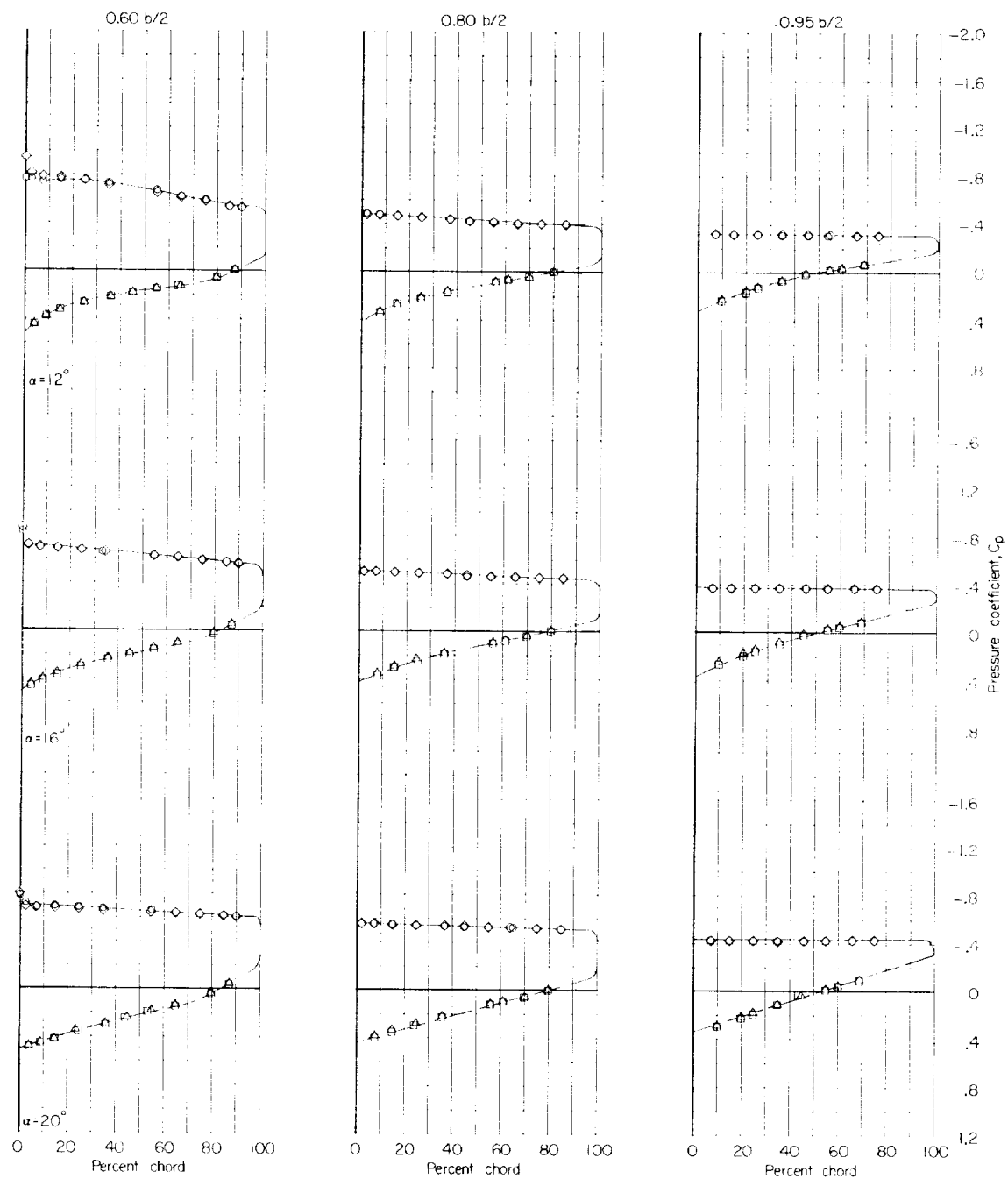
(b) Concluded.

Figure 4.- Continued.



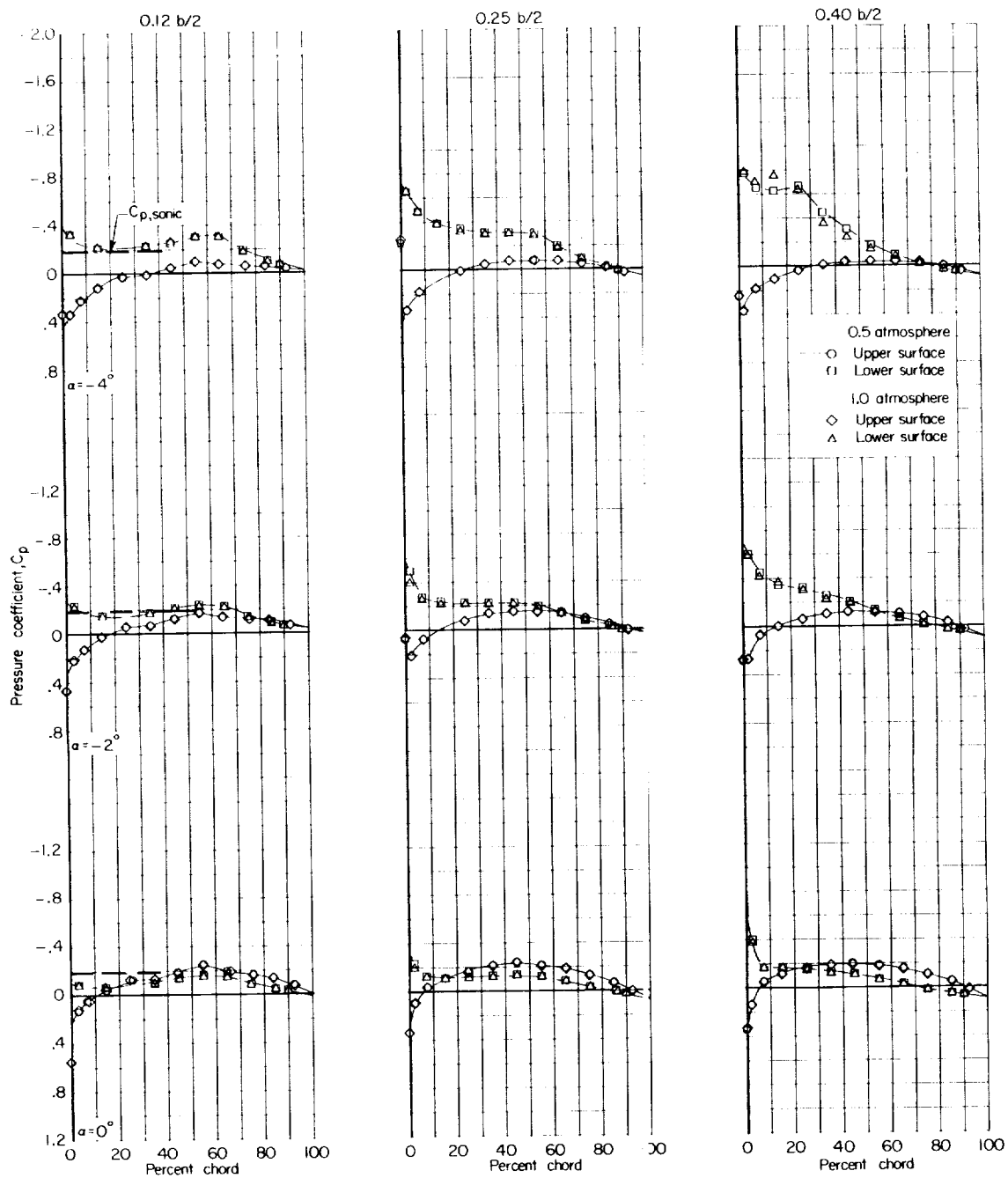
(c) $M = 0.800$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



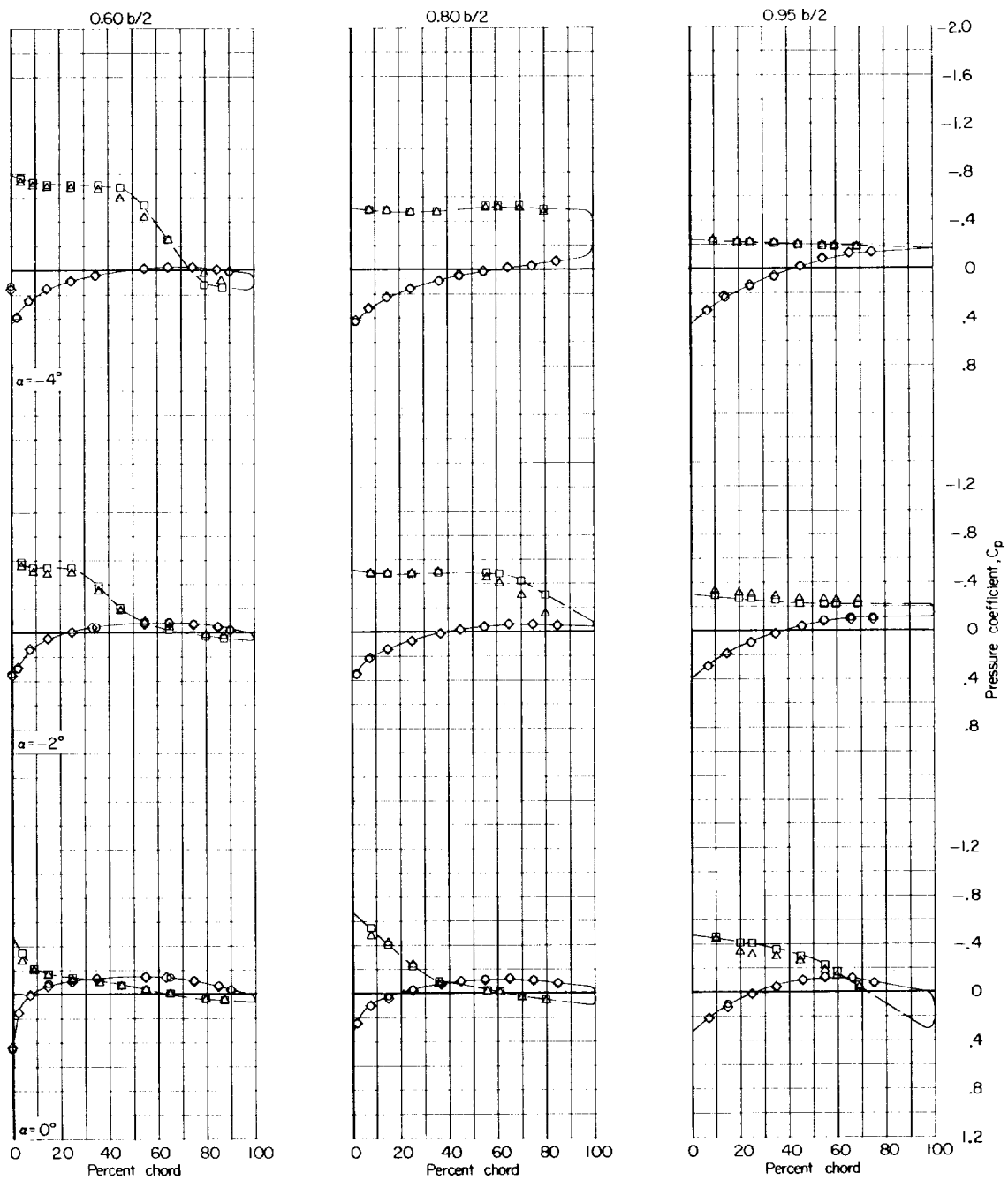
(c) Concluded.

Figure 4.- Continued.



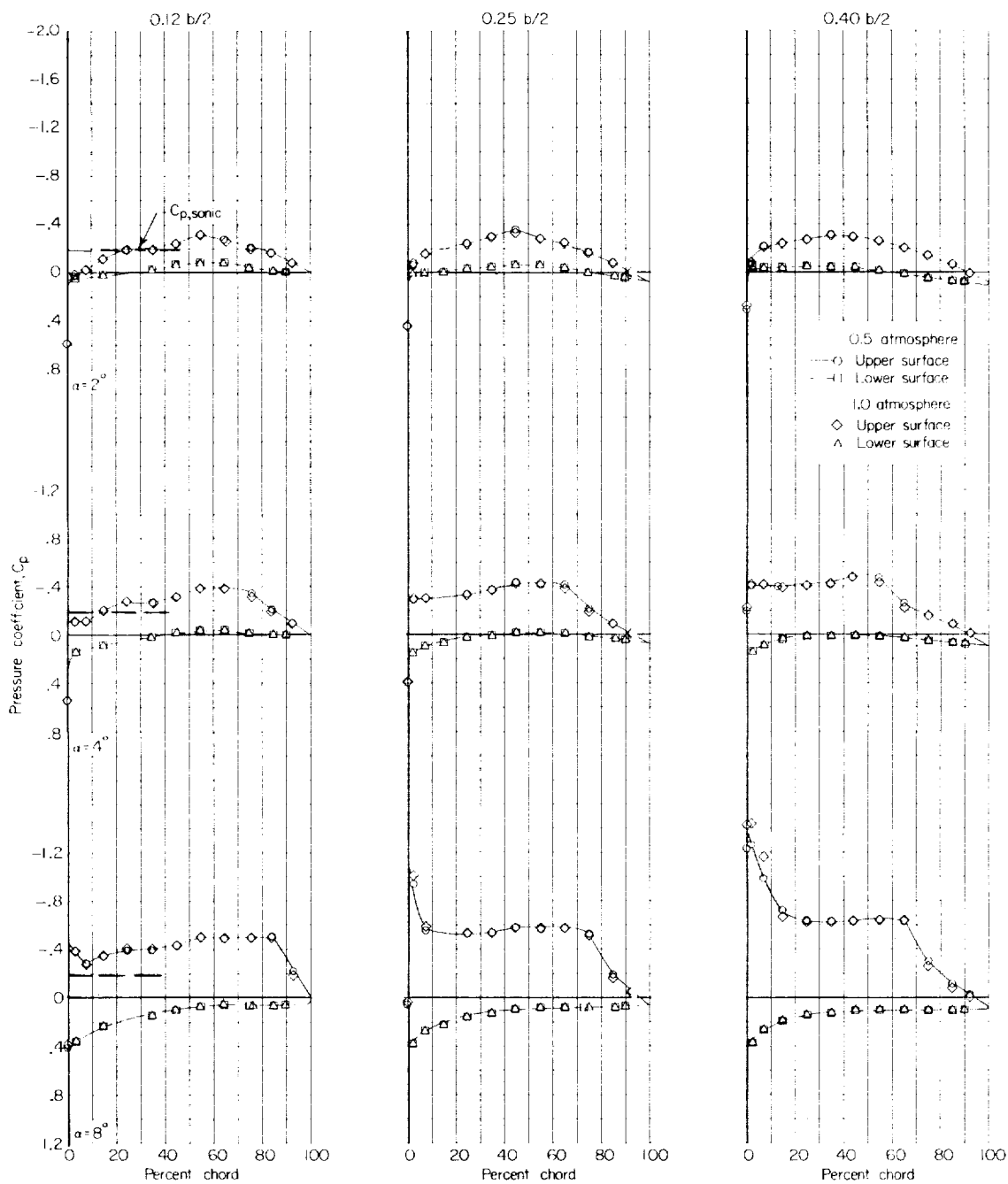
(d) $M = 0.900$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continuel.



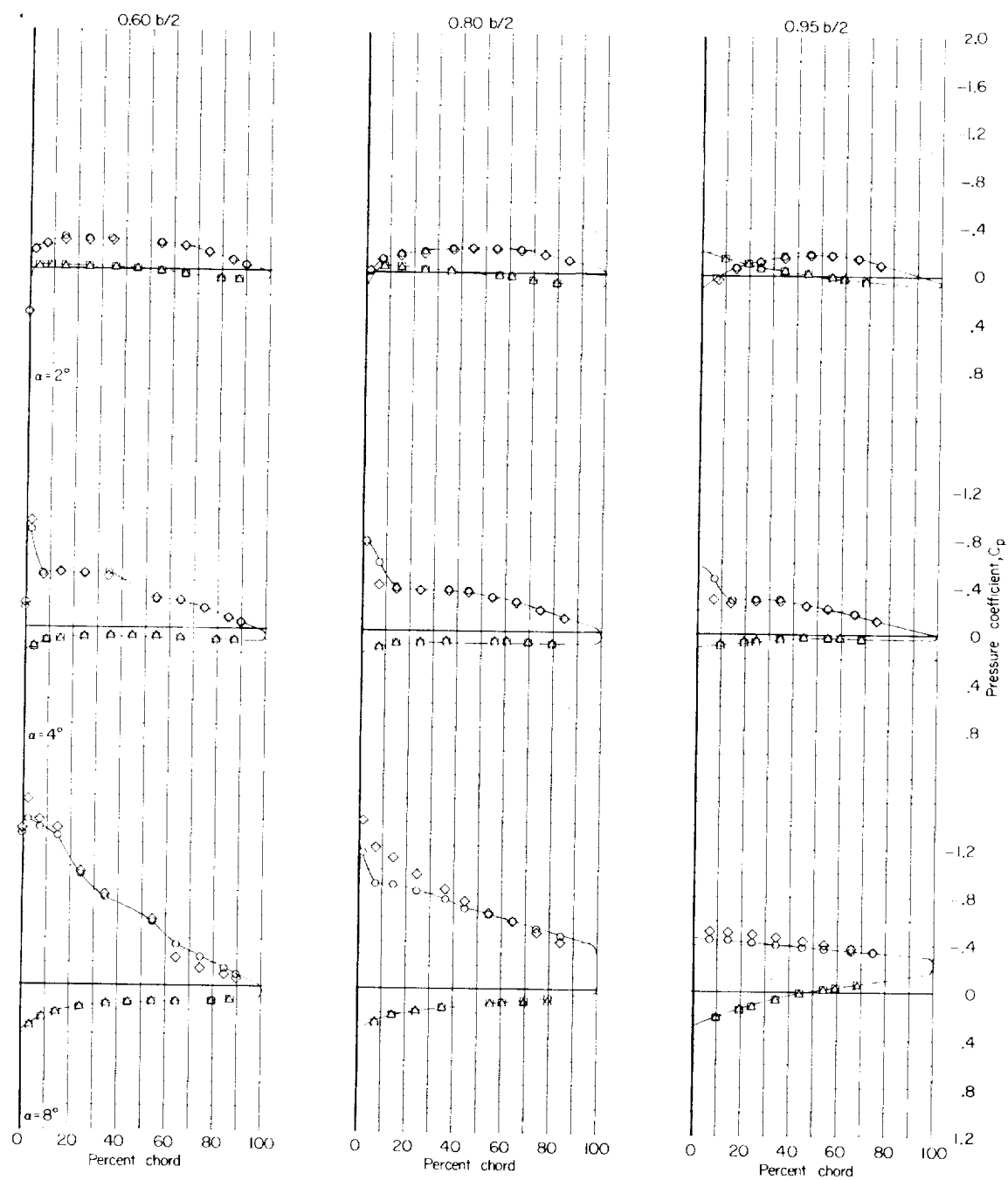
(d) Concluded.

Figure 4.- Continued.



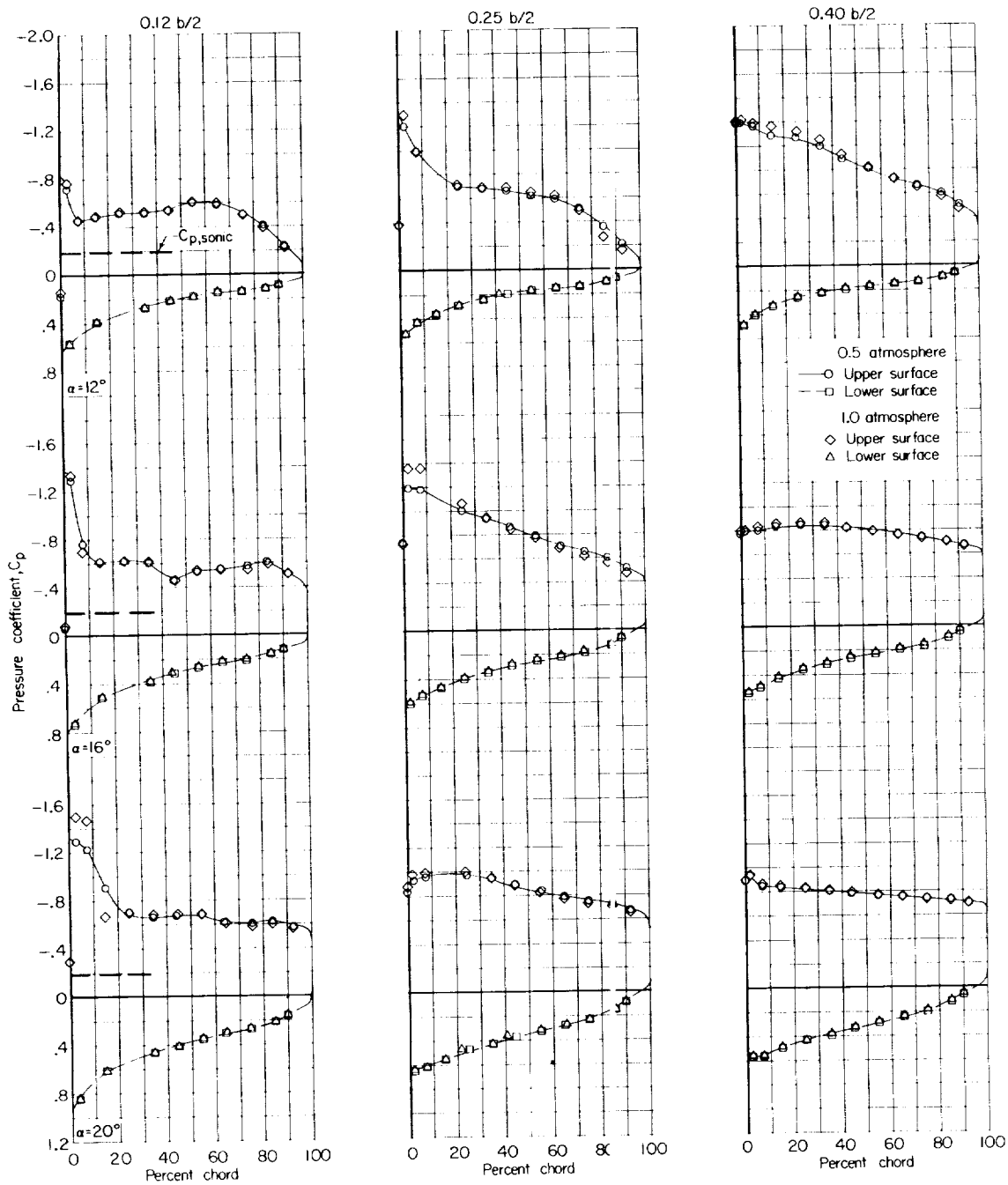
(e) $M = 0.900$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



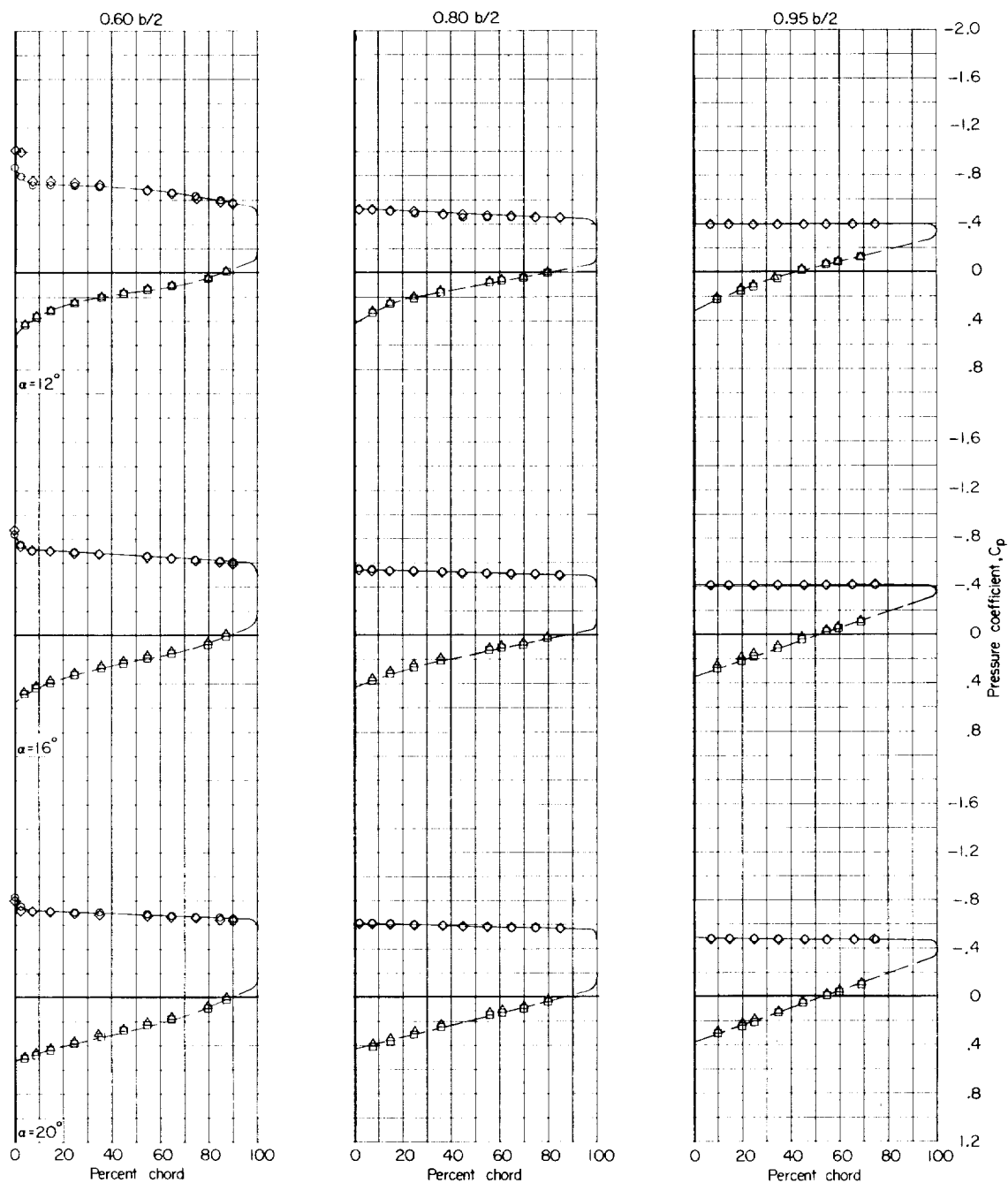
(e) Concluded.

Figure 4.- Continued.



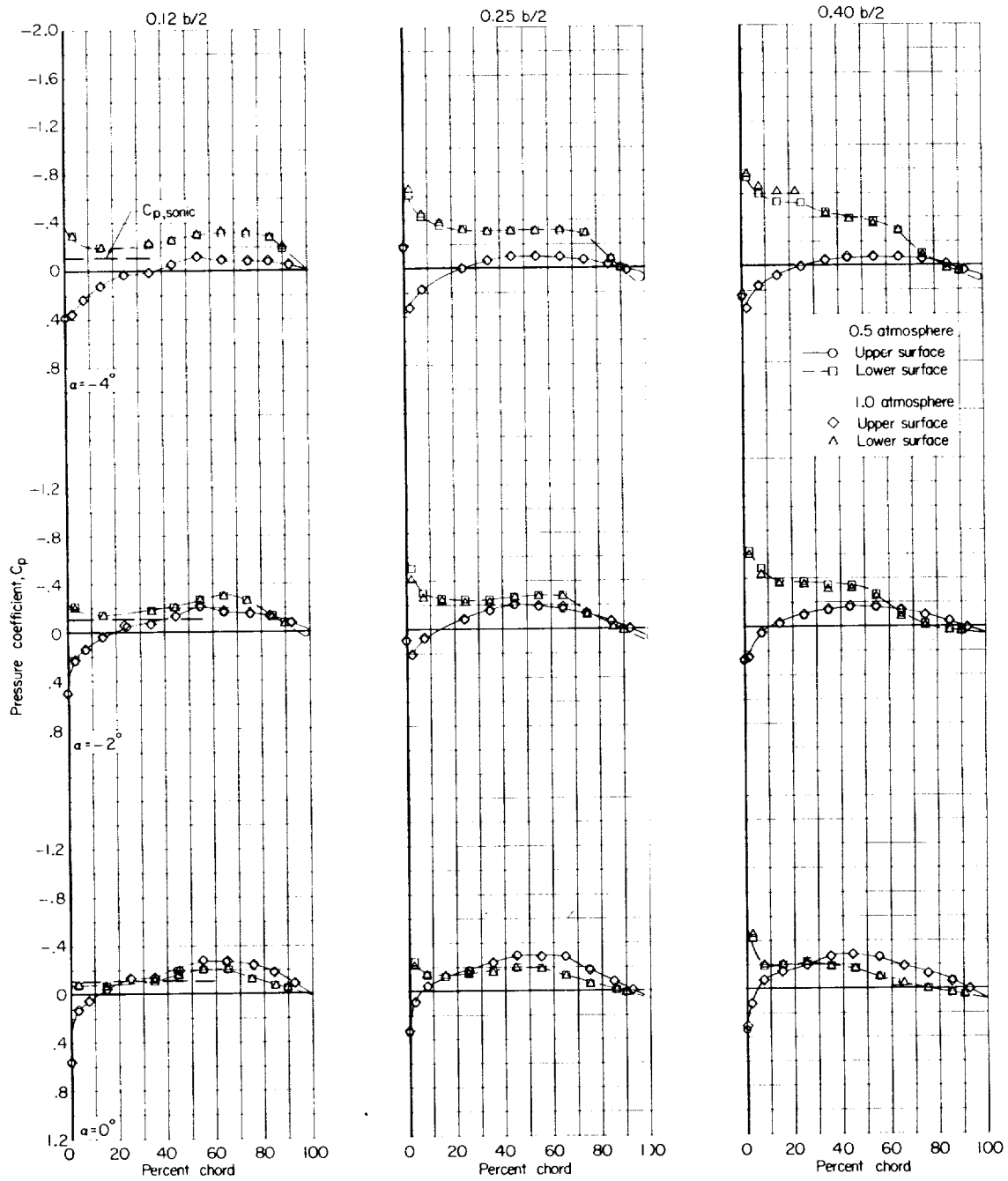
(f) $M = 0.900$; $\alpha = 12^\circ, 16^\circ$, and 20° .

Figure 4.- Continued.



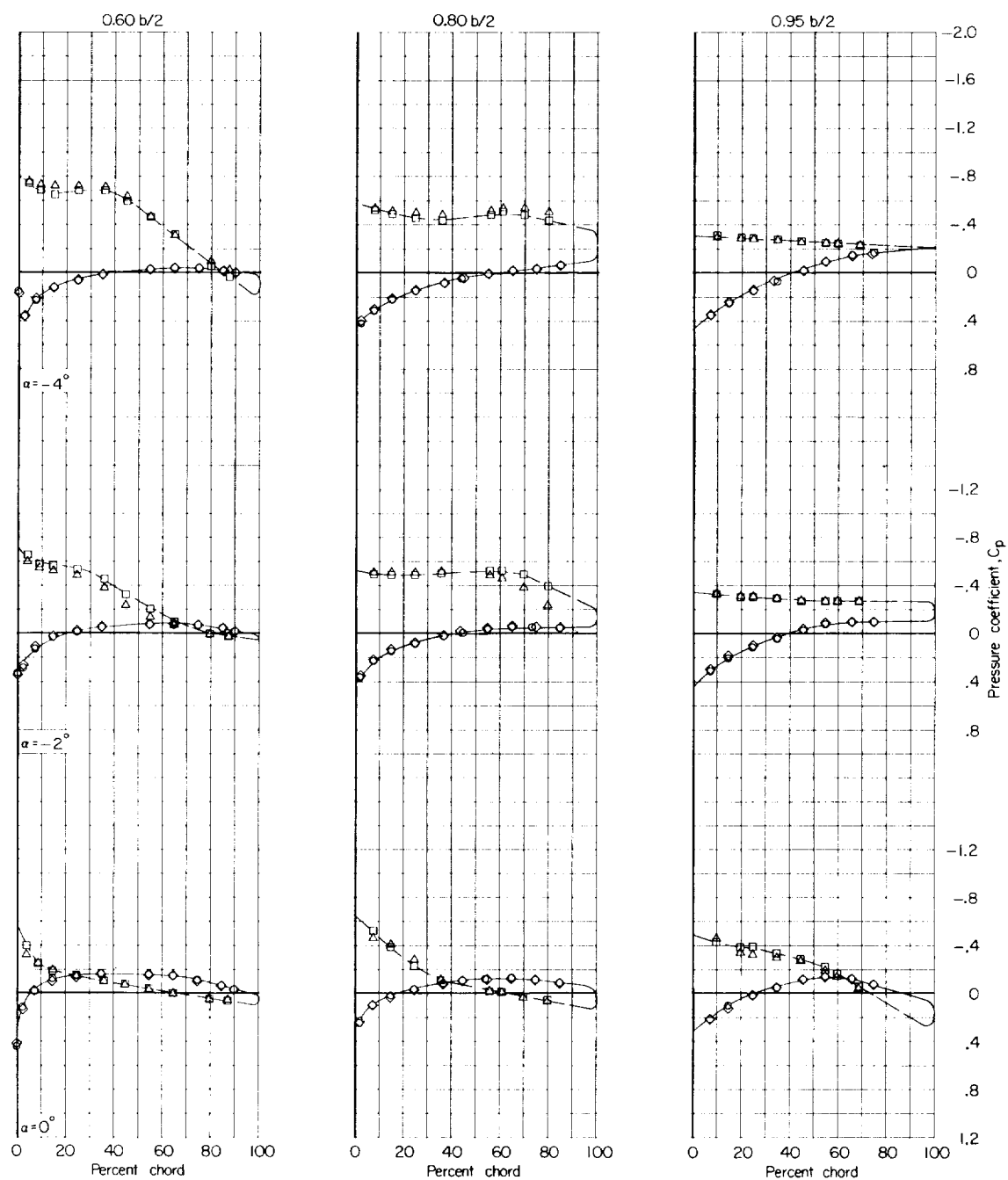
(f) Concluded.

Figure 4.- Continued.



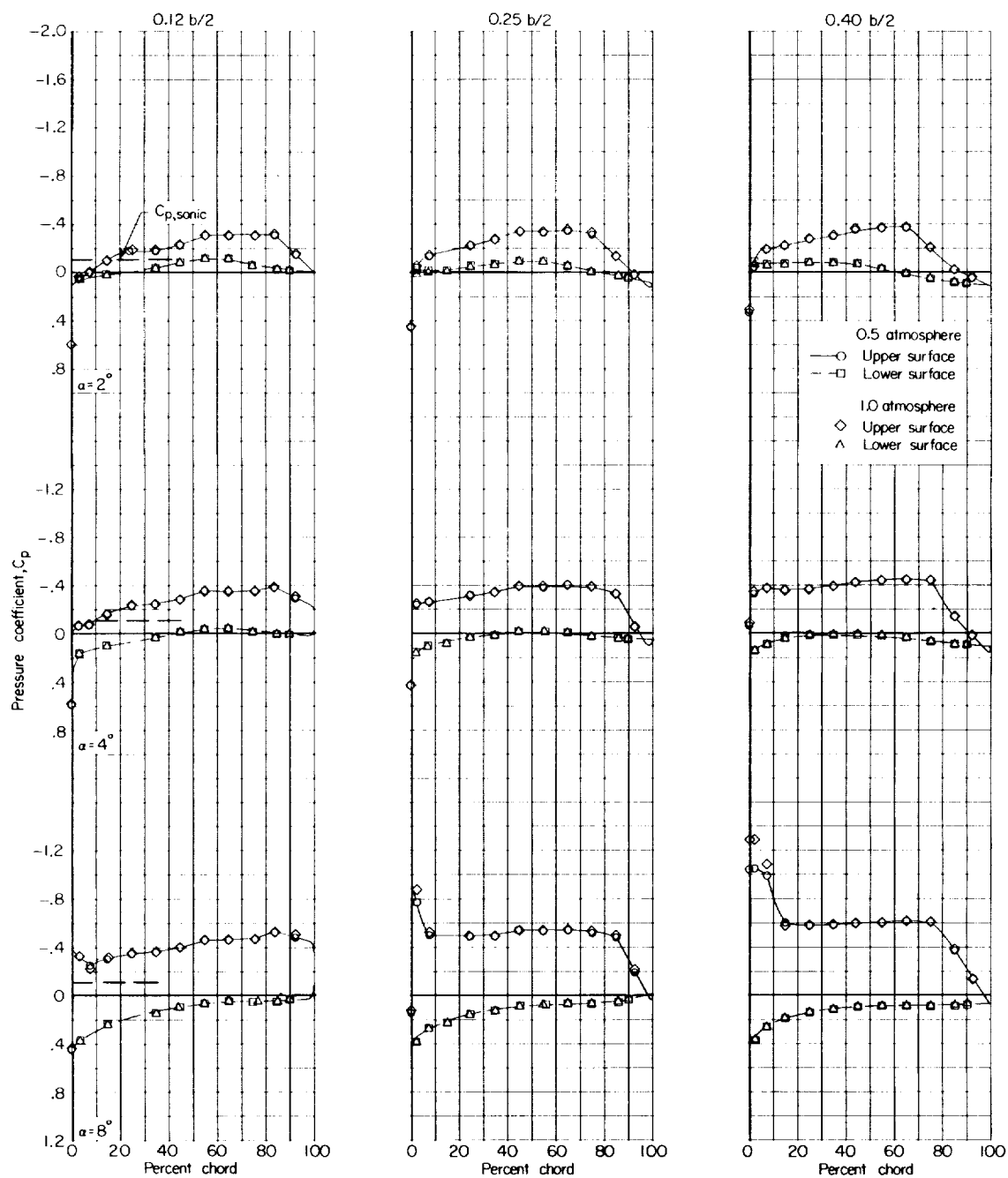
(g) $M = 0.940$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



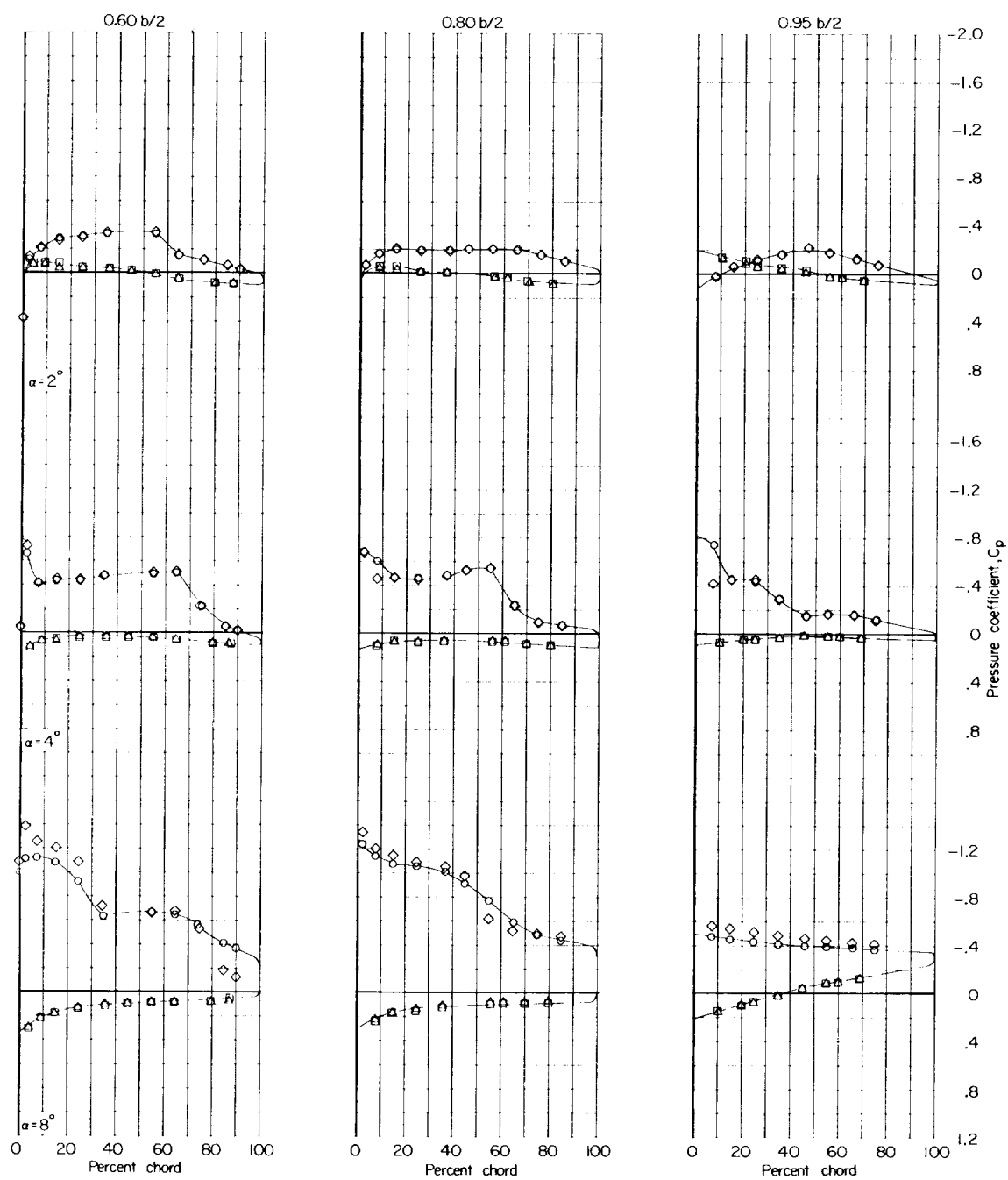
(g) Concluded.

Figure 4.- Continued.



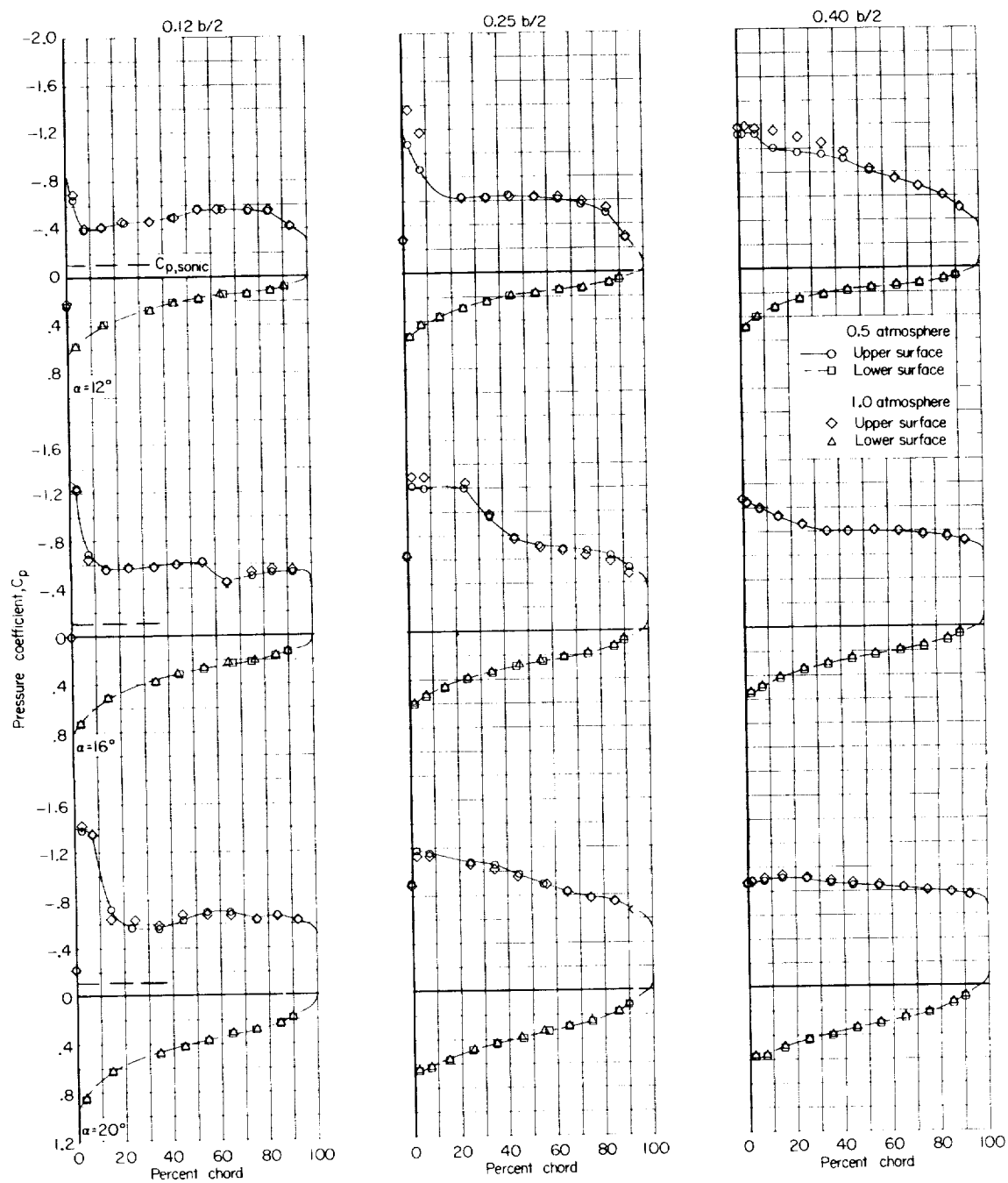
(h) $M = 0.940$; $\alpha = 2^\circ, 4^\circ$, and 8° .

Figure 4.- Continued.



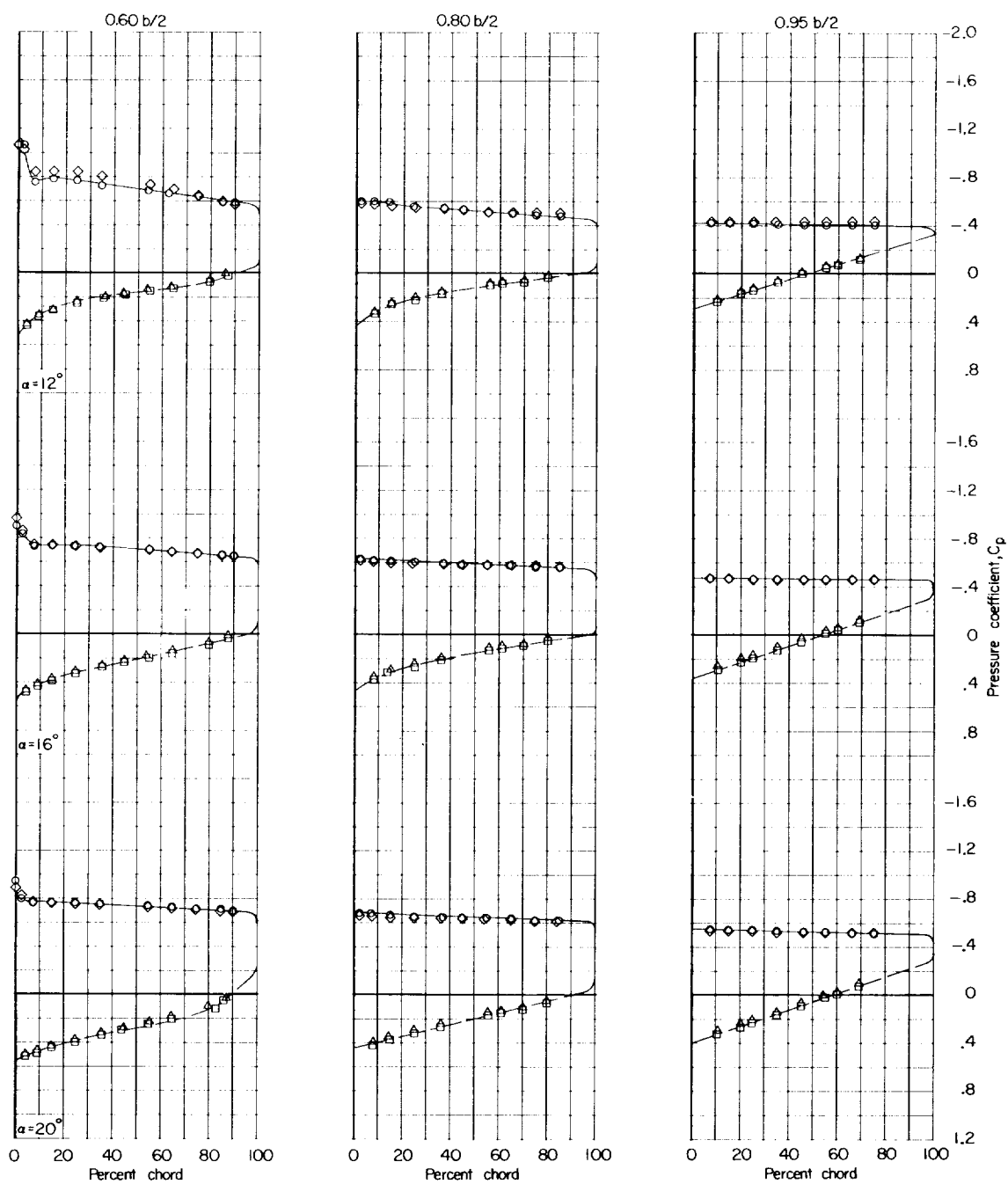
(h) Concluded.

Figure 4.- Continued.



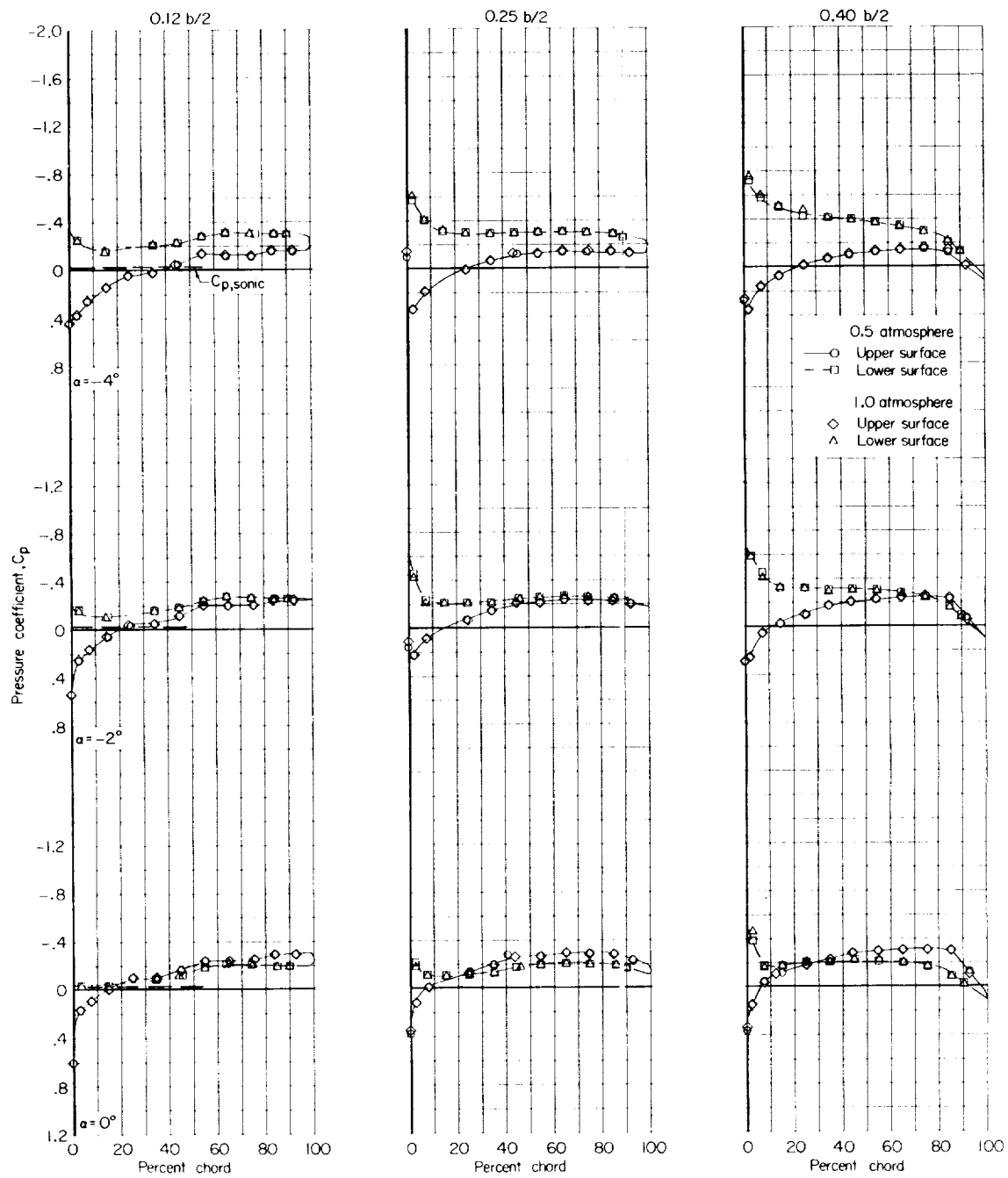
(i) $M = 0.940$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



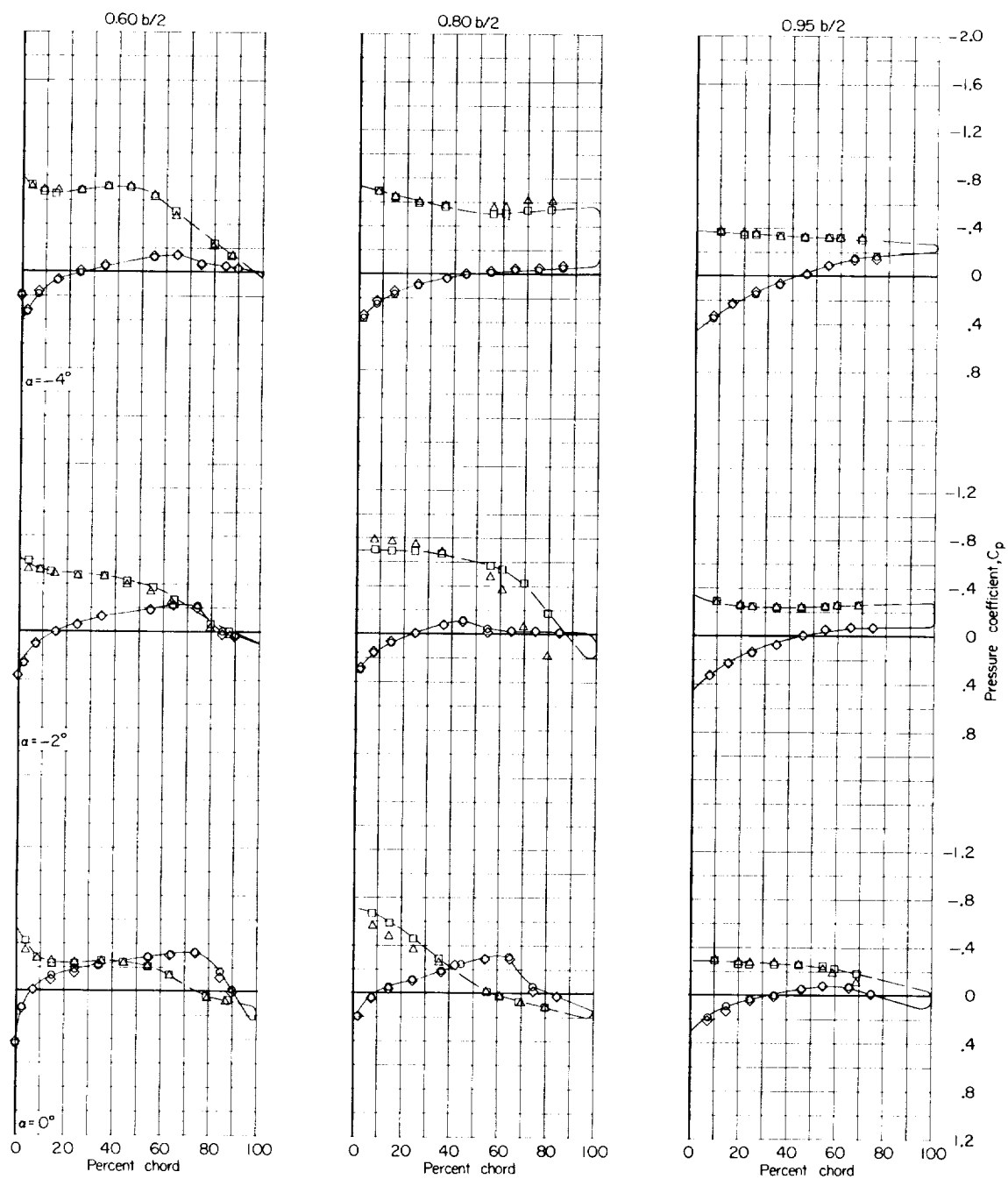
(i) Concluded.

Figure 4.- Continued.



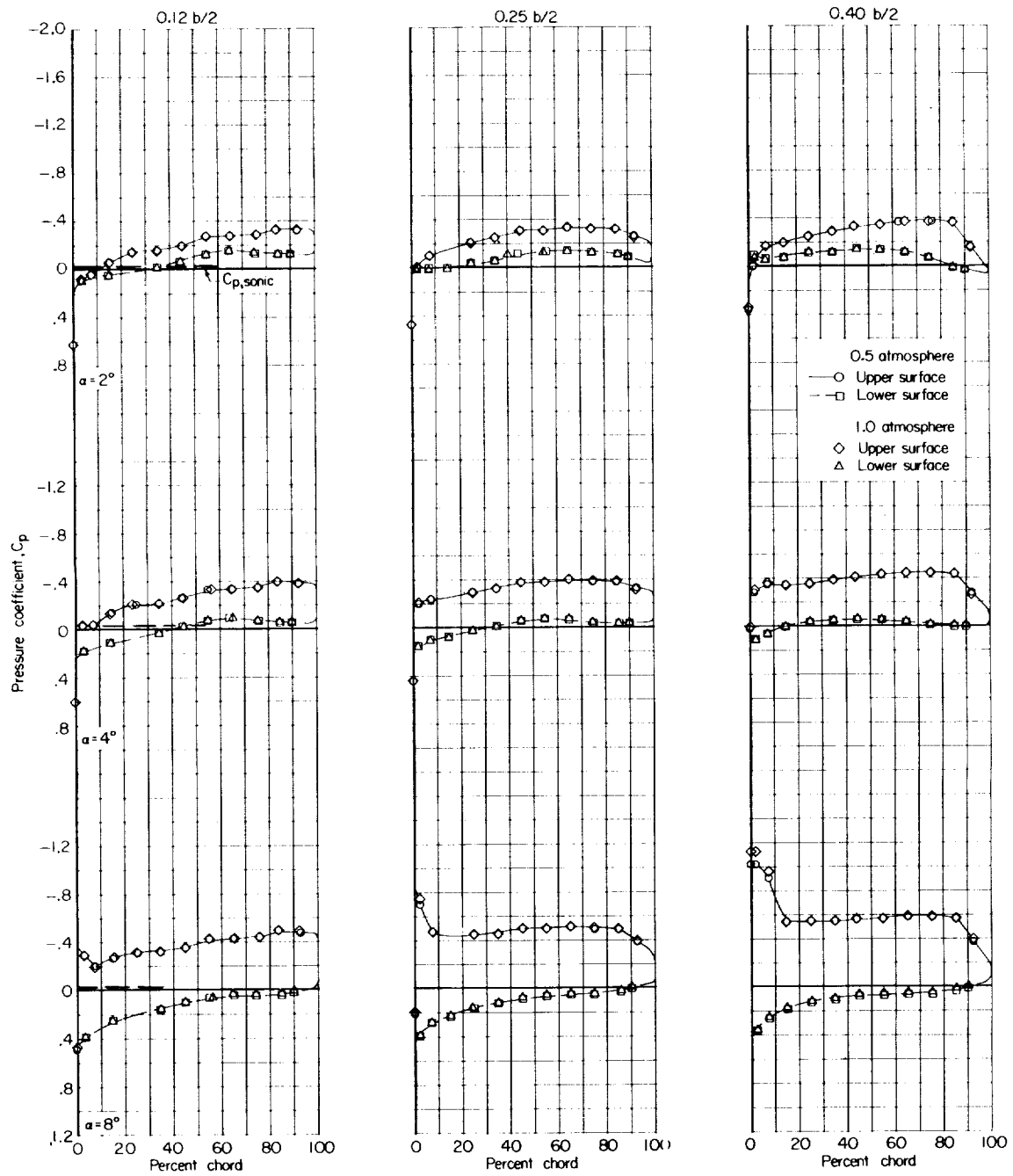
(j) $M = 0.980$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



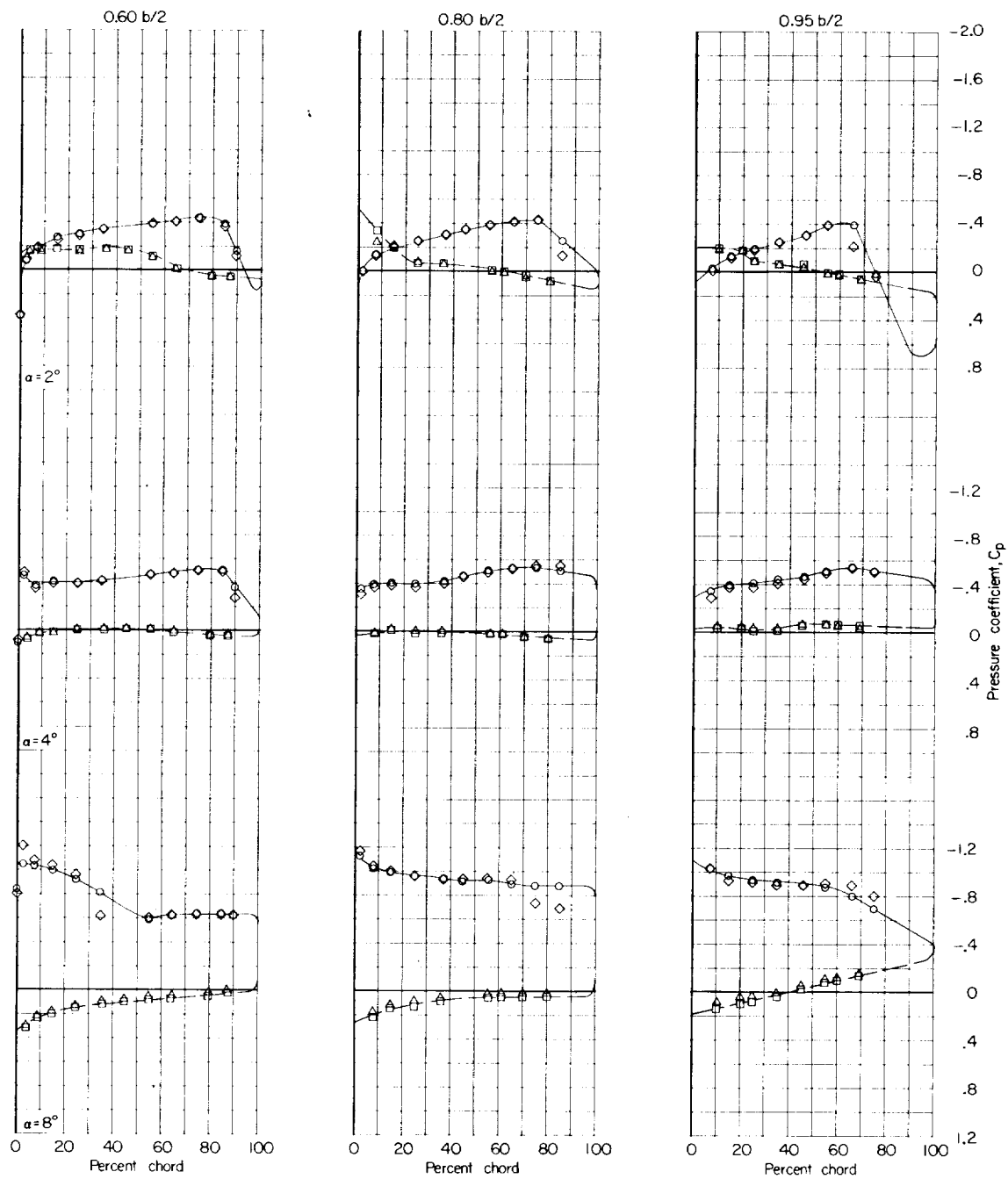
(j) Concluded.

Figure 4.- Continued.



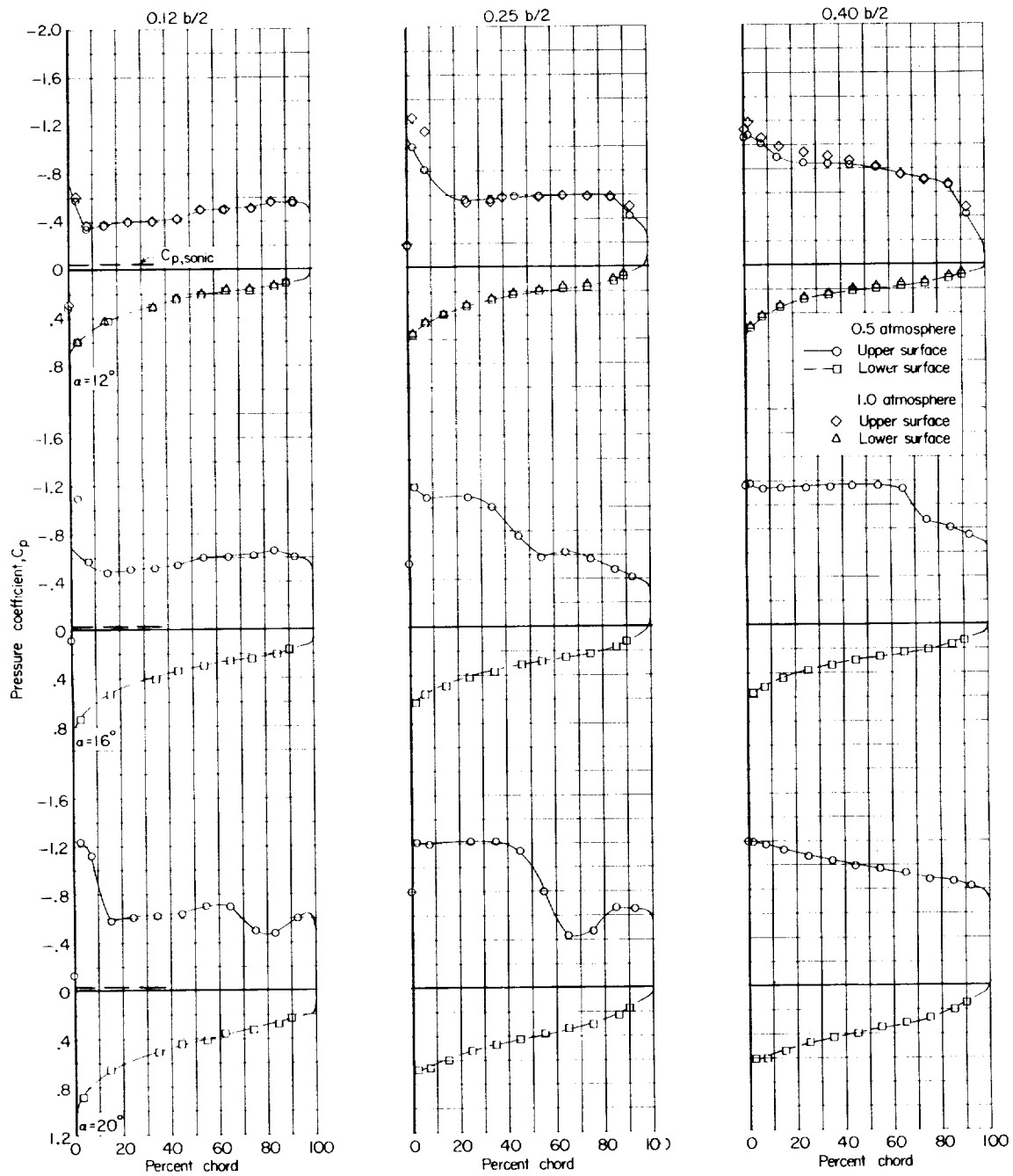
(k) $M = 0.980$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



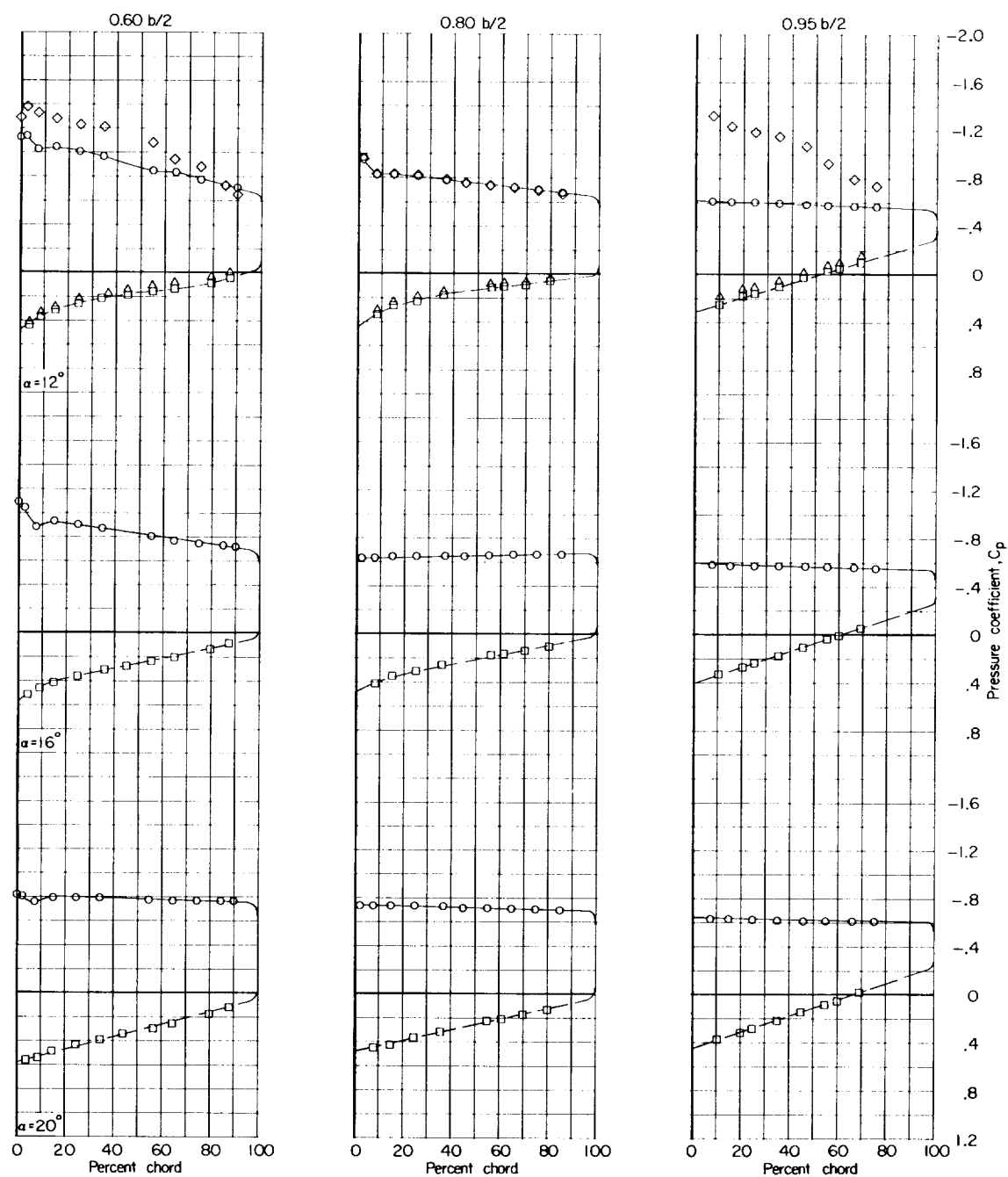
(k) Concluded.

Figure 4.- Continued.



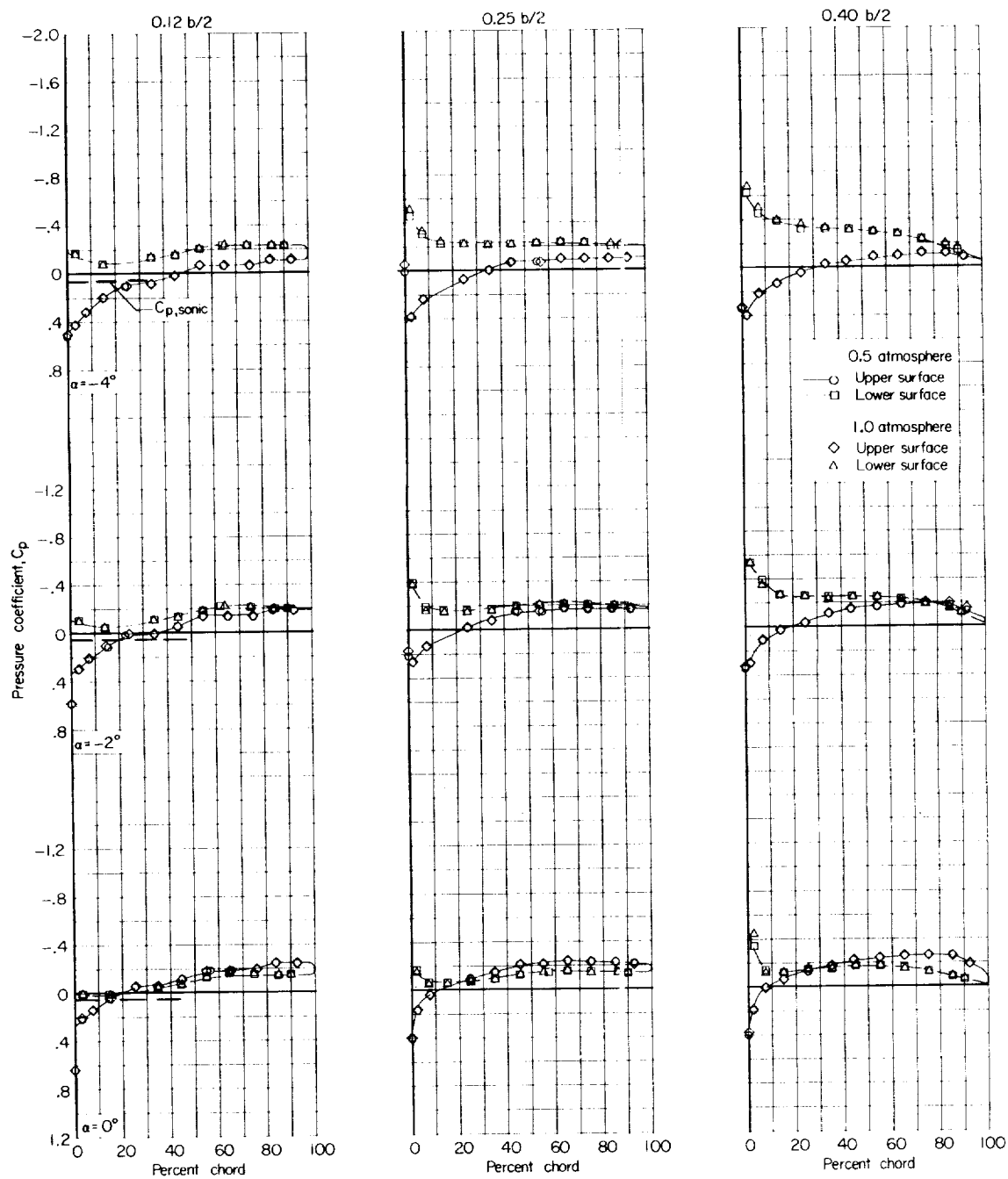
(1) $M = 0.980$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



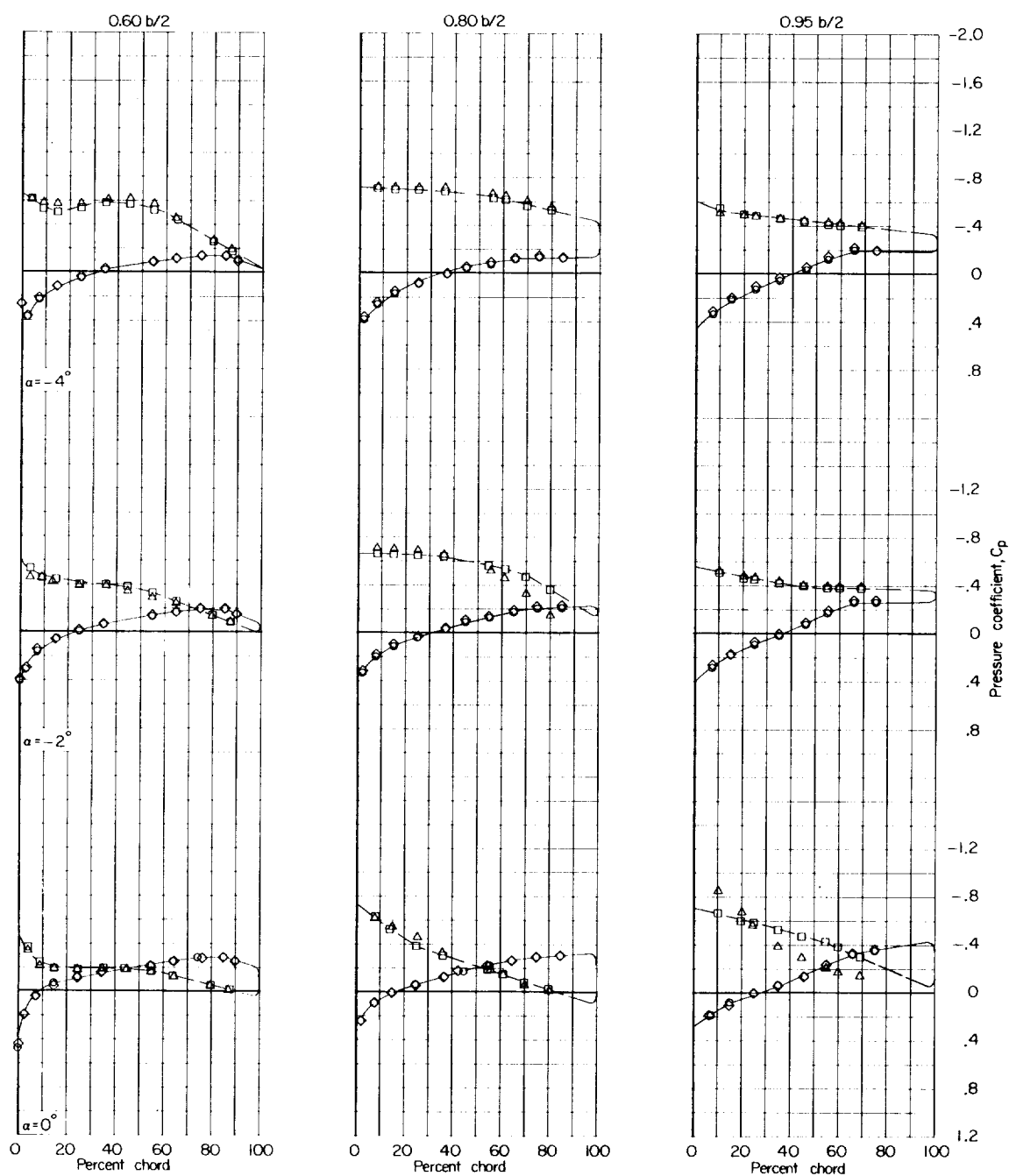
(1) Concluded.

Figure 4.- Continued.



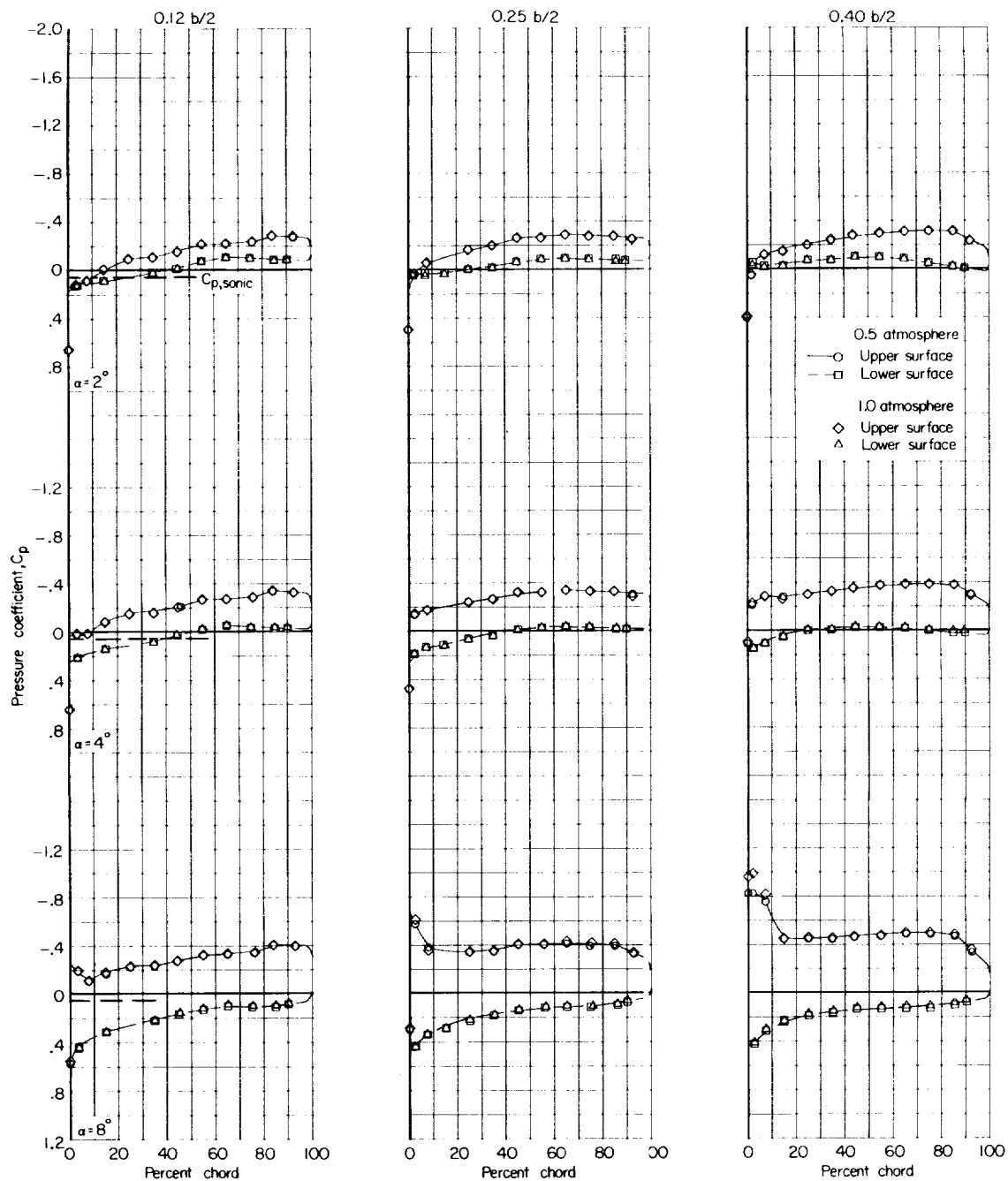
(m) $M = 1.030$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continuel.



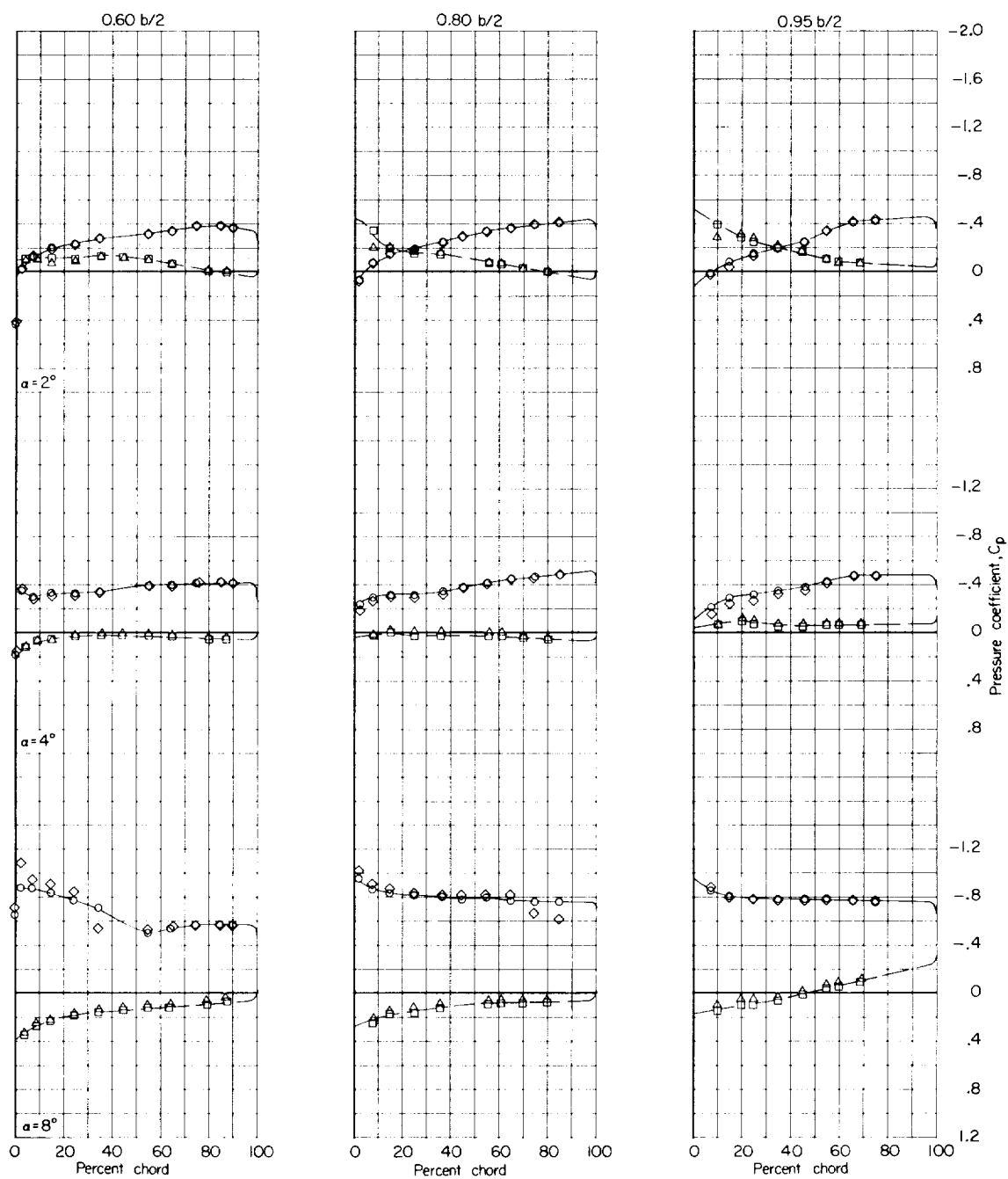
(m) Concluded.

Figure 4.- Continued.



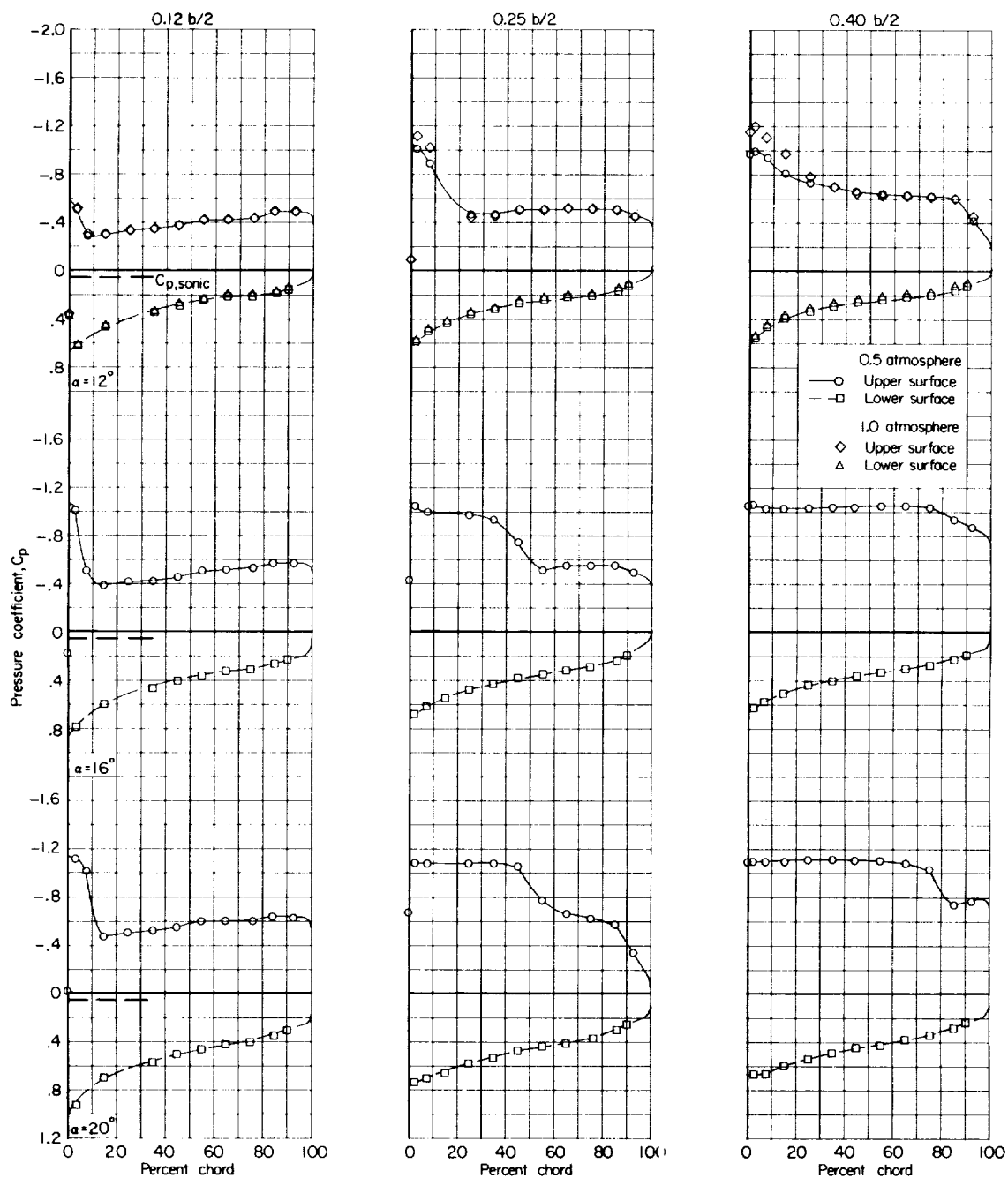
(n) $M = 1.030$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



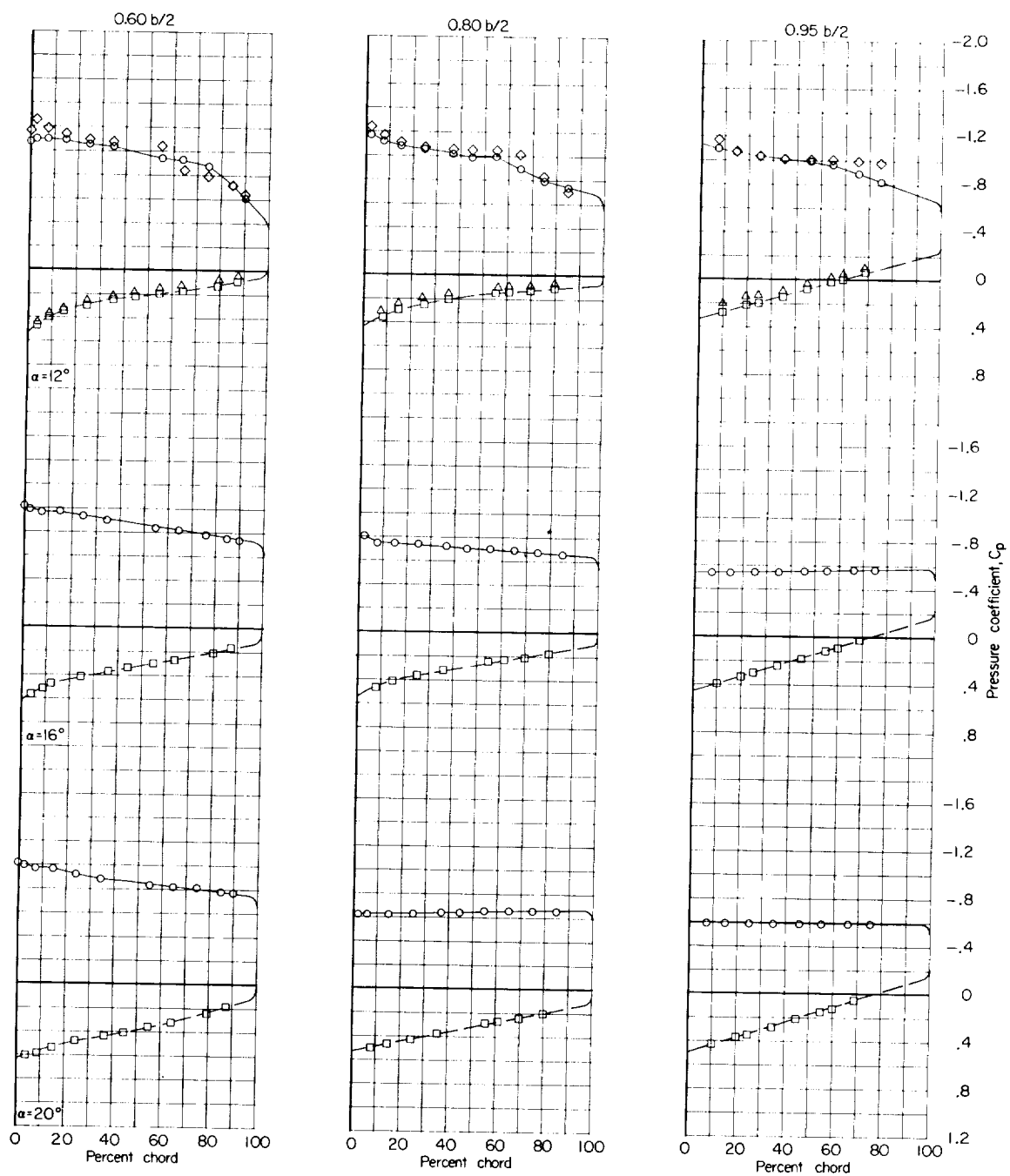
(n) Concluded.

Figure 4.- Continued.



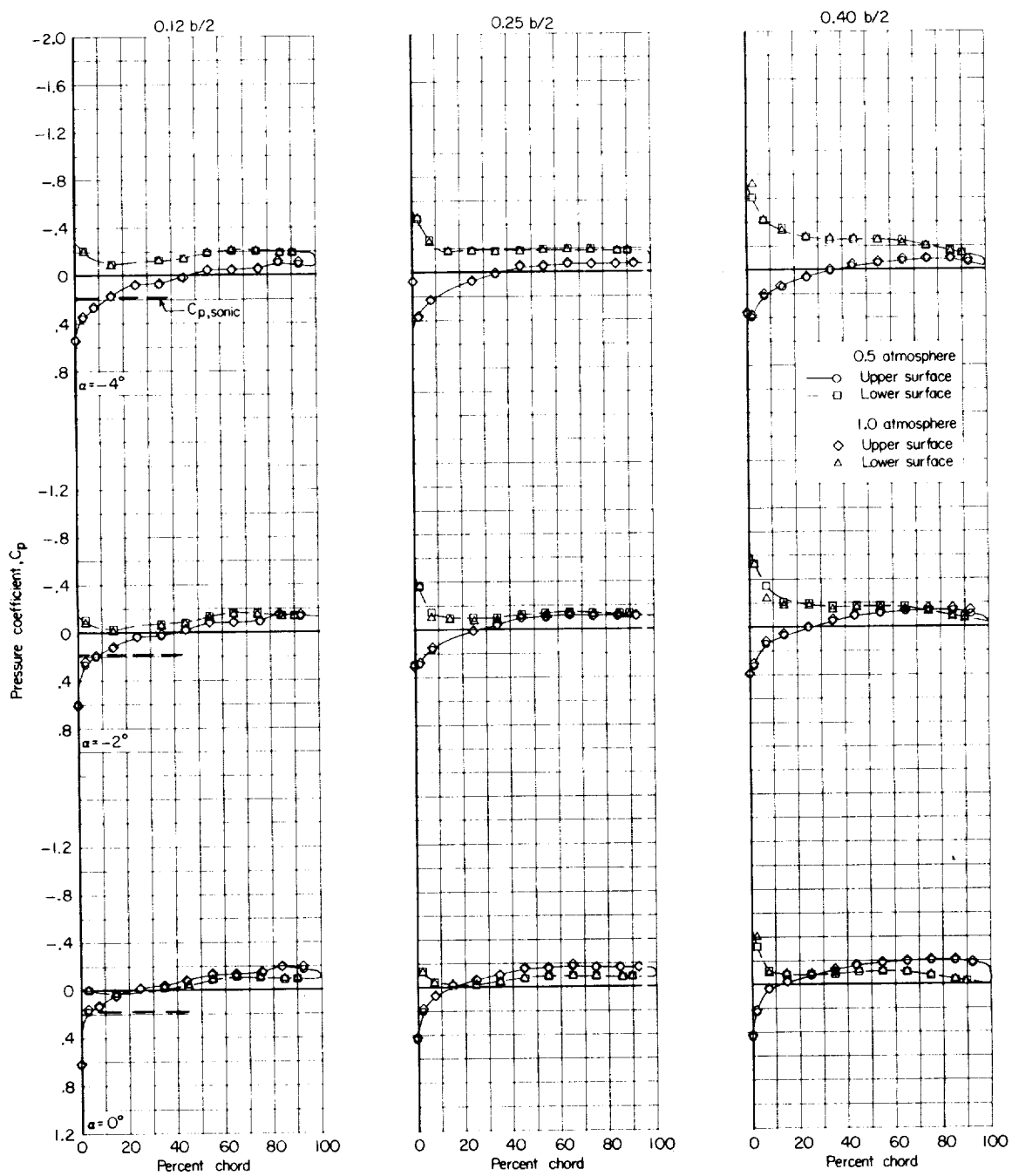
(o) $M = 1.030$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



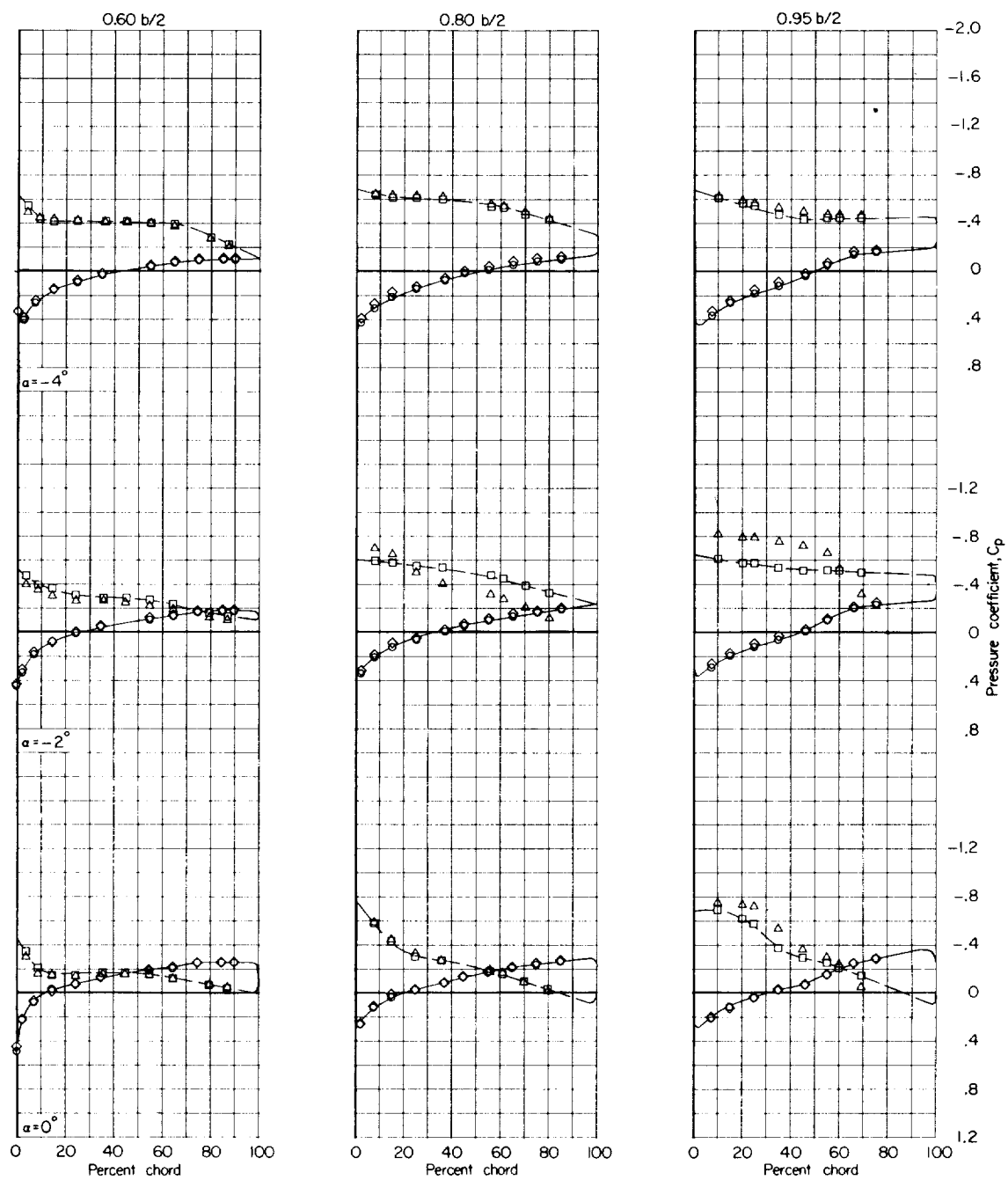
(o) Concluded.

Figure 4.- Continued.



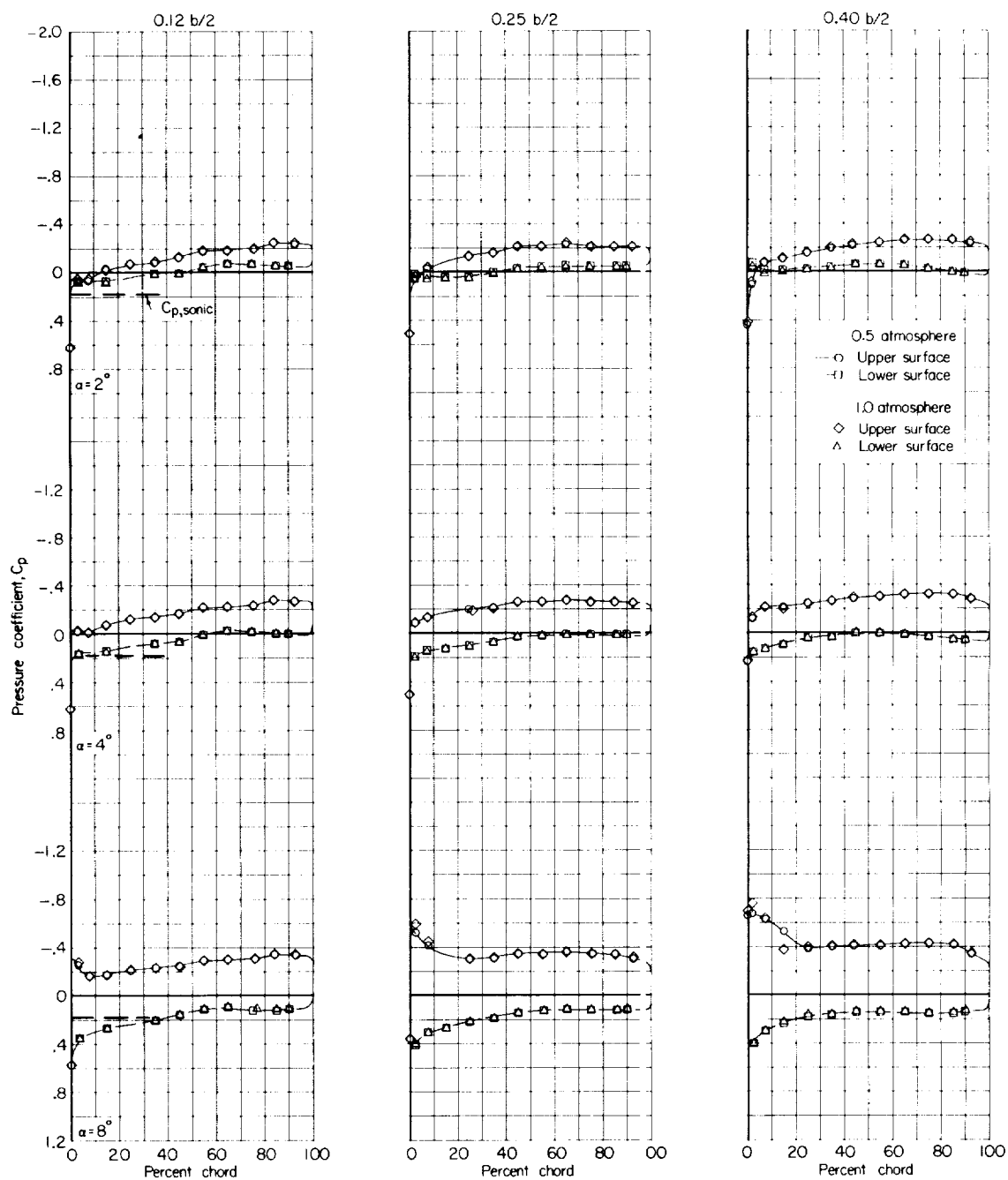
(p) $M = 1.125$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



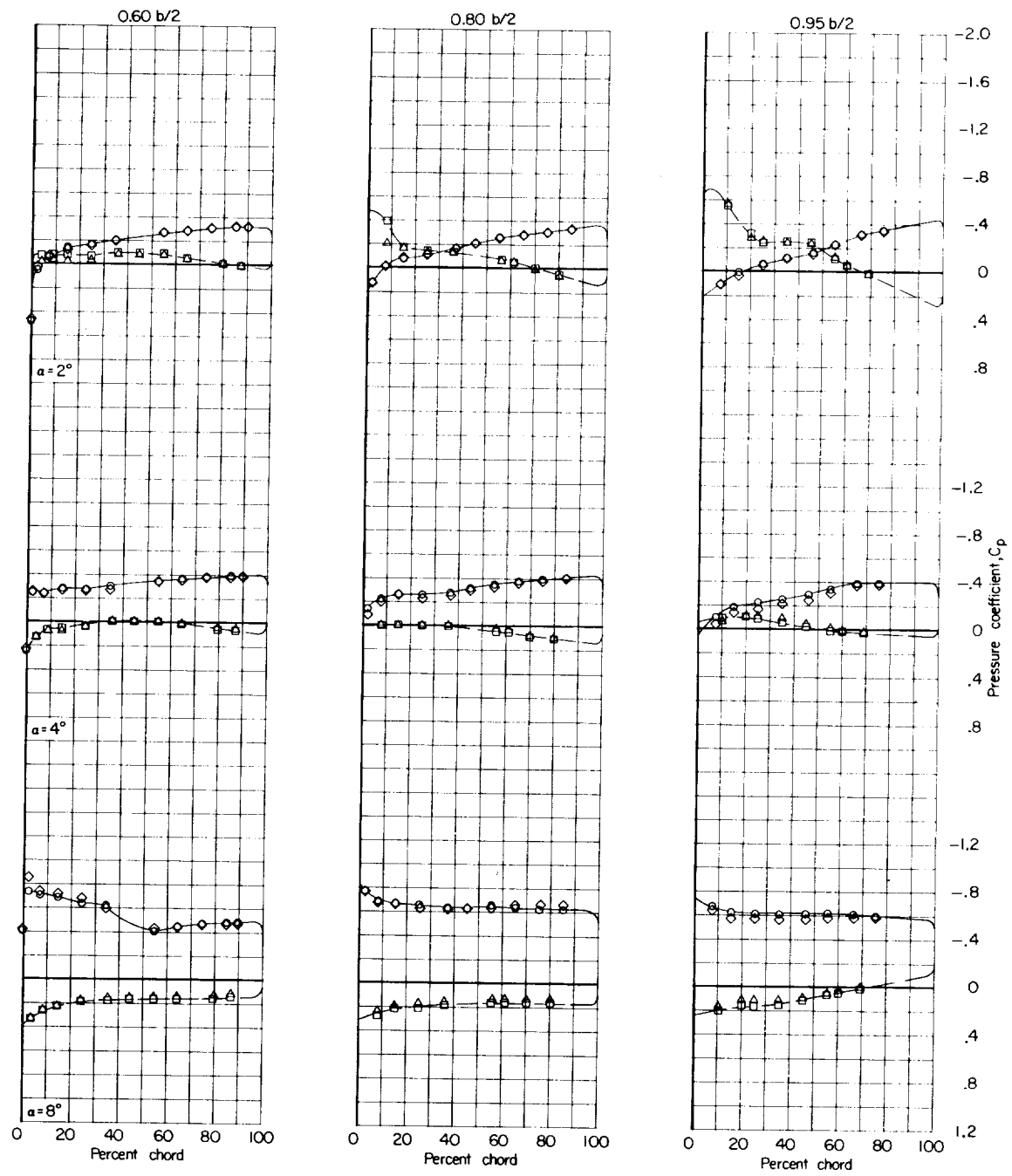
(p) Concluded.

Figure 4.- Continued.



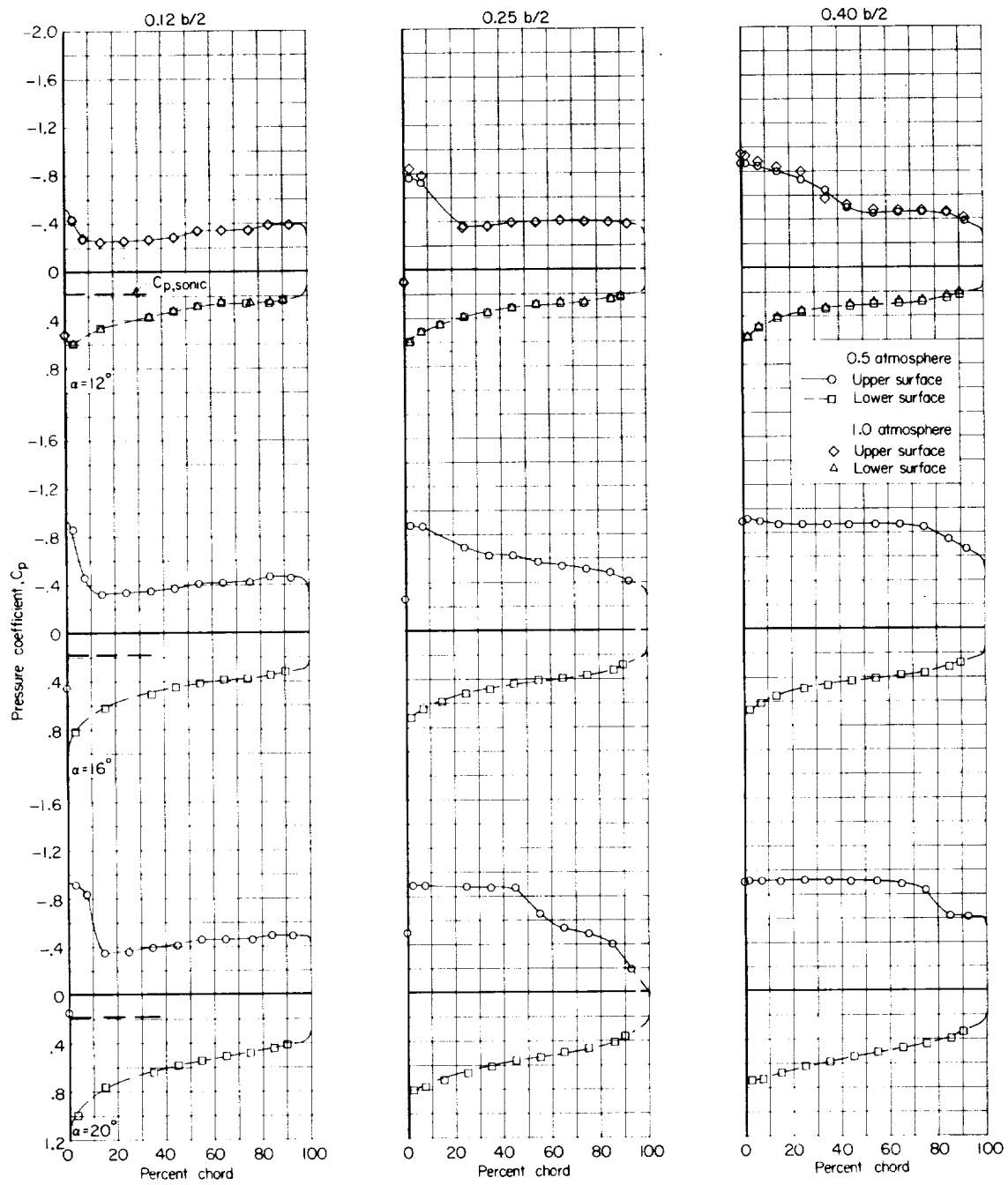
(q) $M = 1.125$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



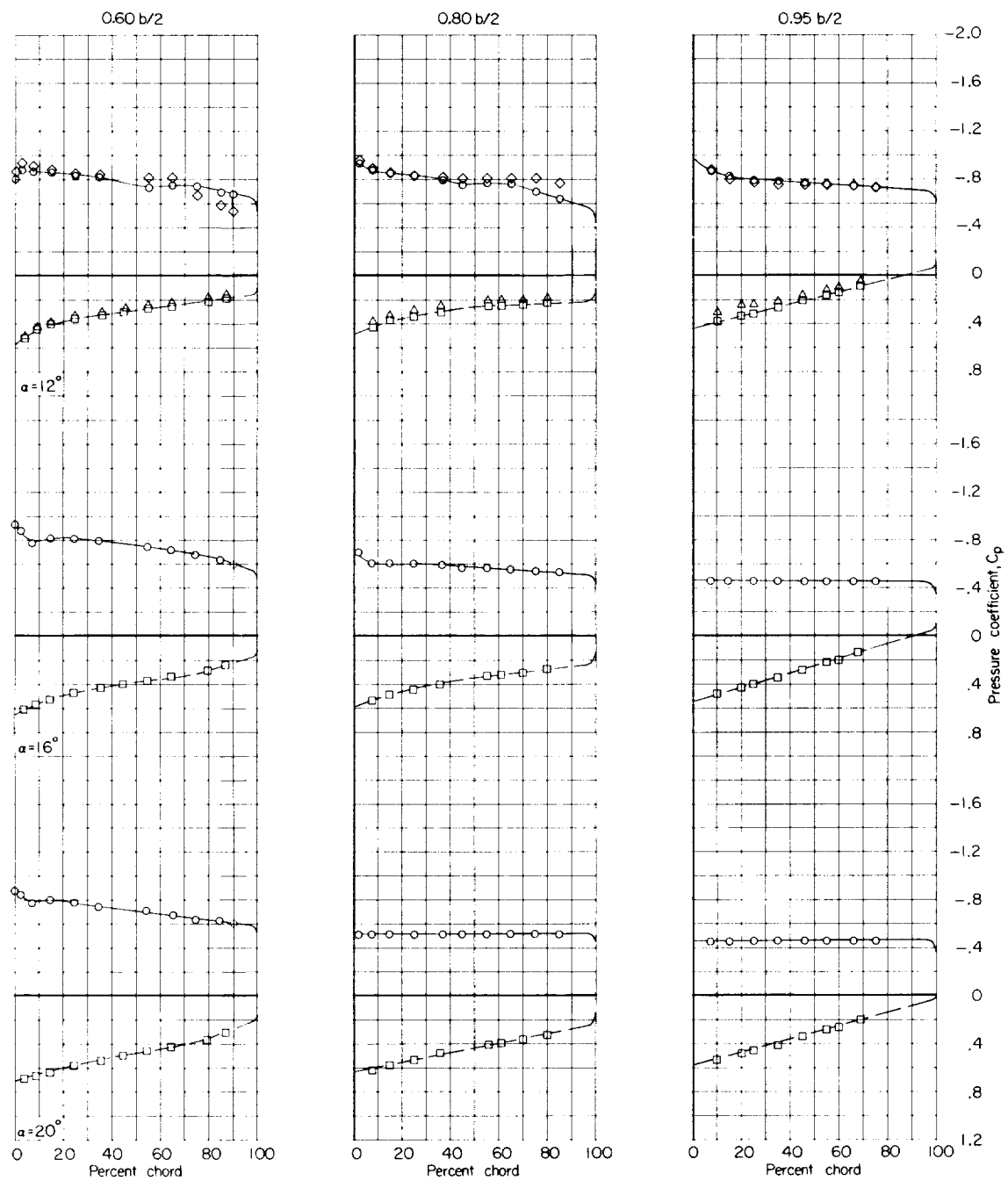
(q) Concluded.

Figure 4.- Continued.



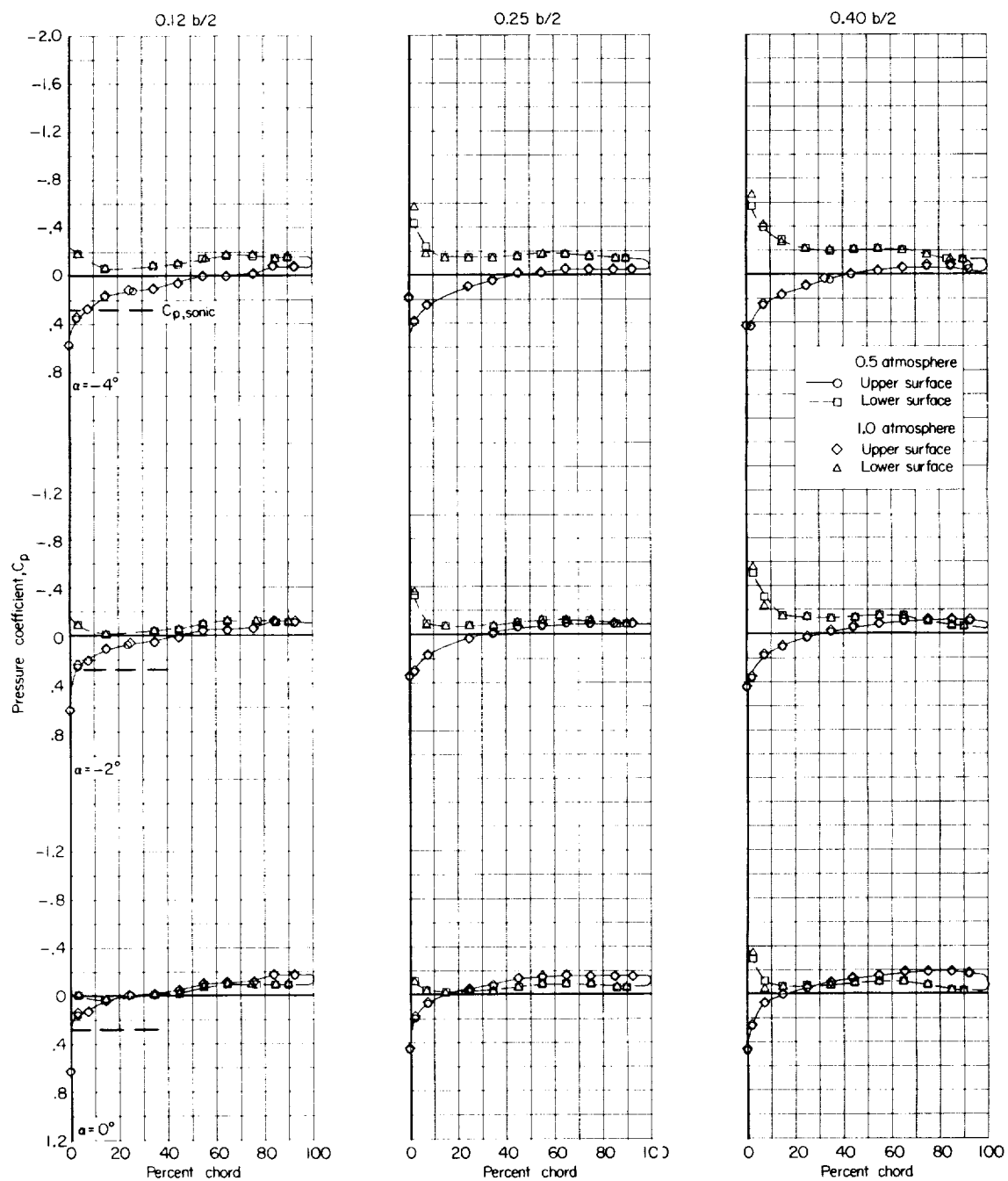
(r) $M = 1.125$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



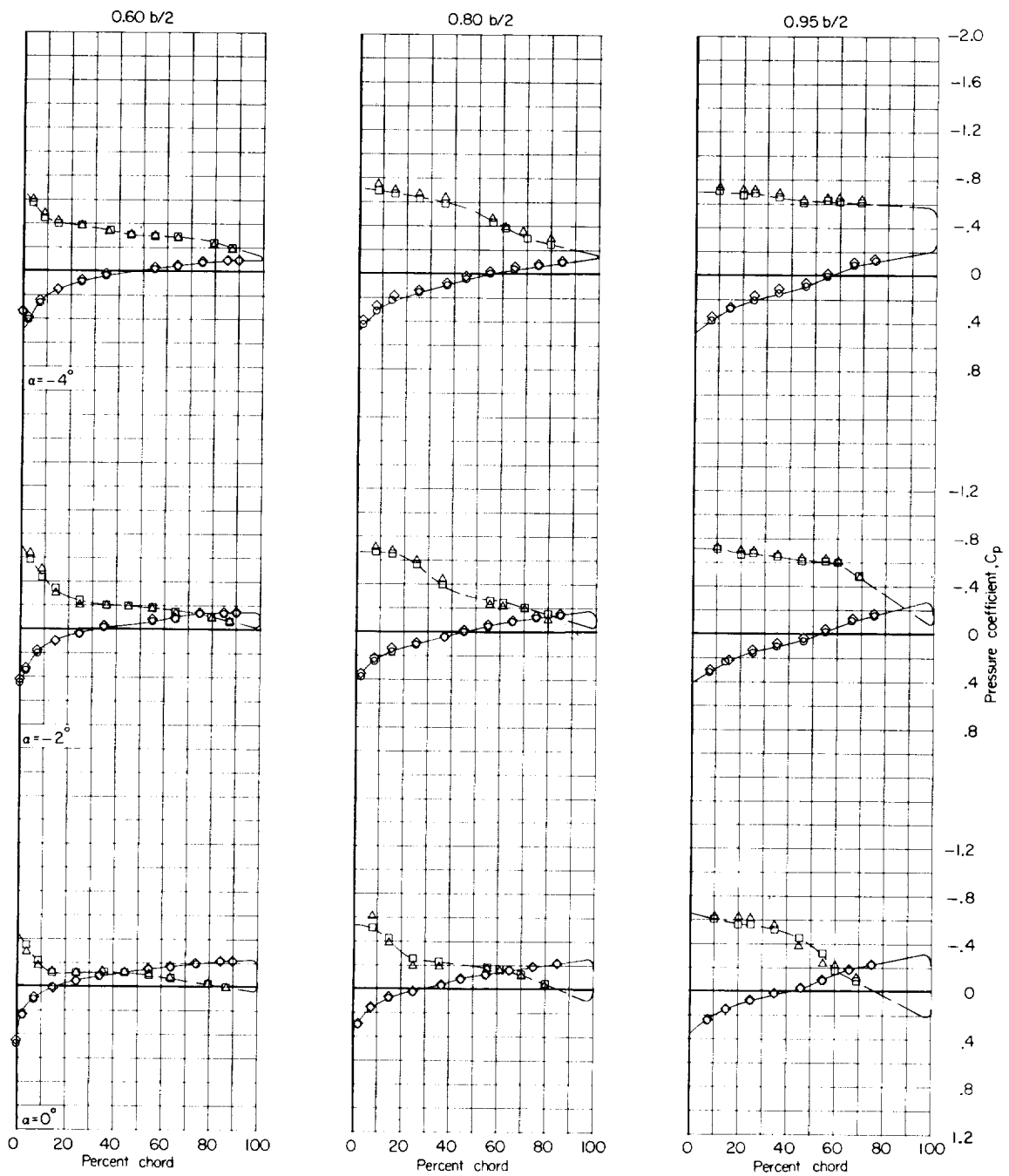
(r) Concluded.

Figure 4.- Continued.



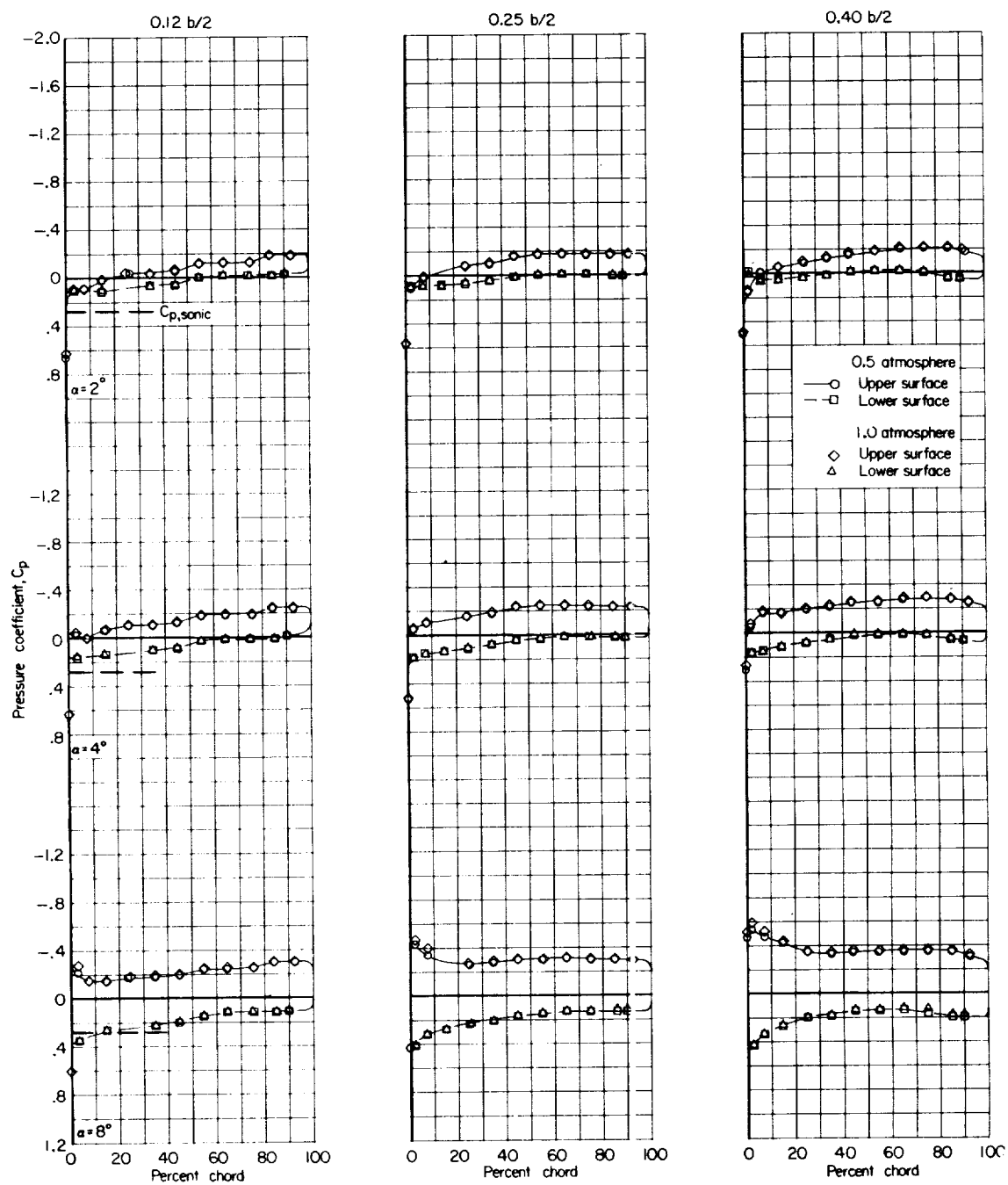
(s) $M = 1.200$; $\alpha = -4^\circ$, -2° , and 0° .

Figure 4.- Continued.



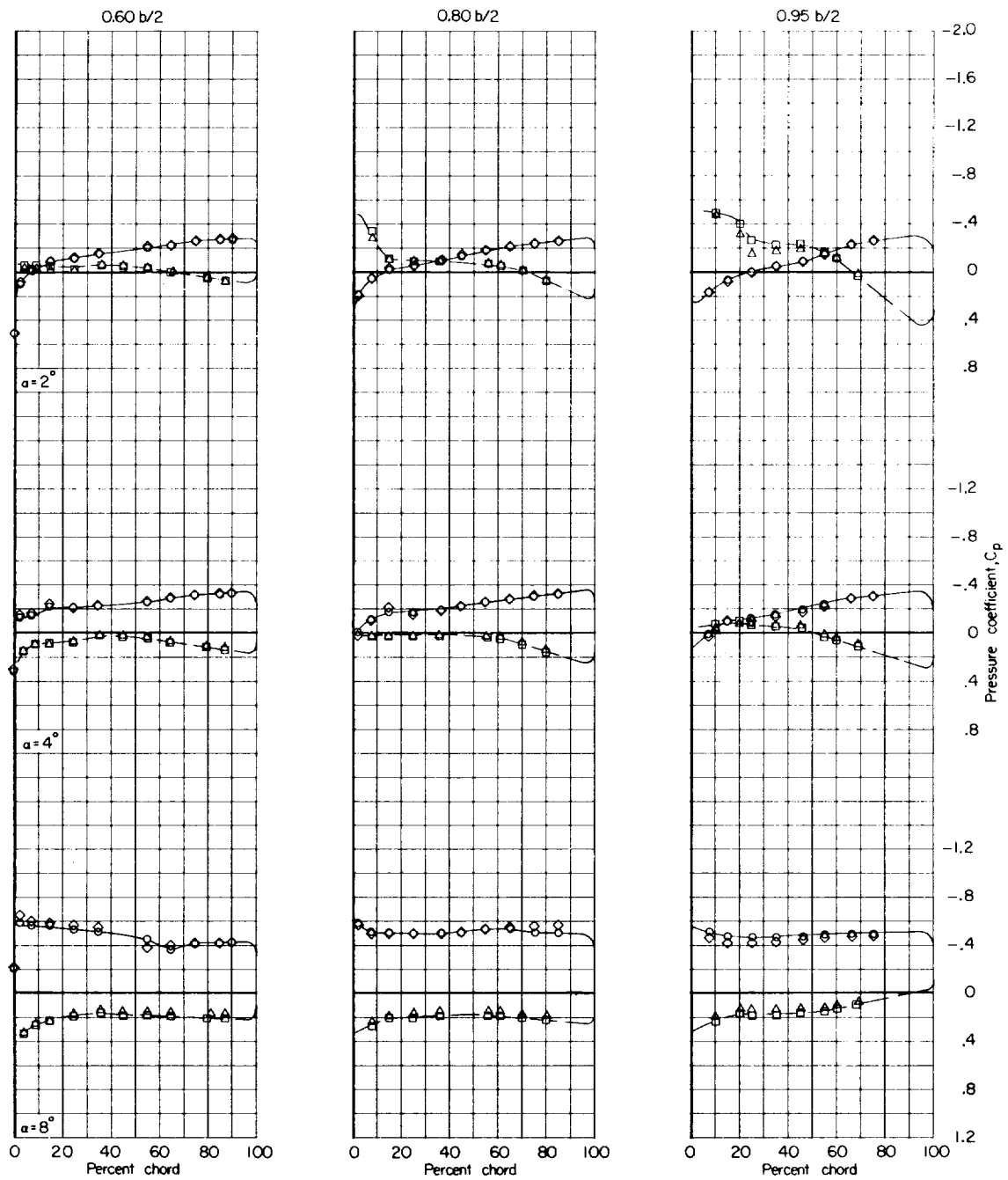
(s) Concluded.

Figure 4.- Continued.



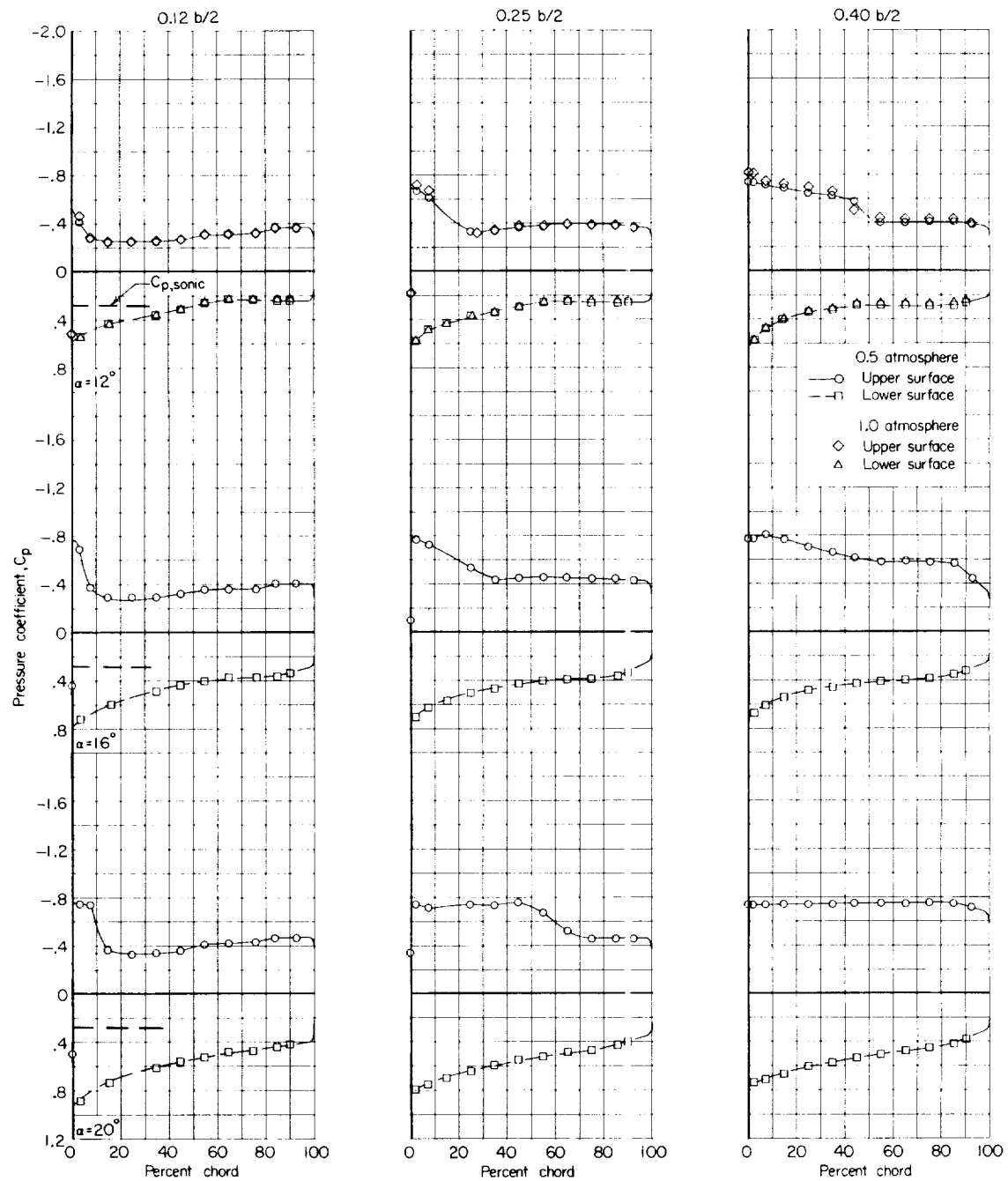
(t) $M = 1.200$; $\alpha = 2^\circ$, 4° , and 8° .

Figure 4.- Continued.



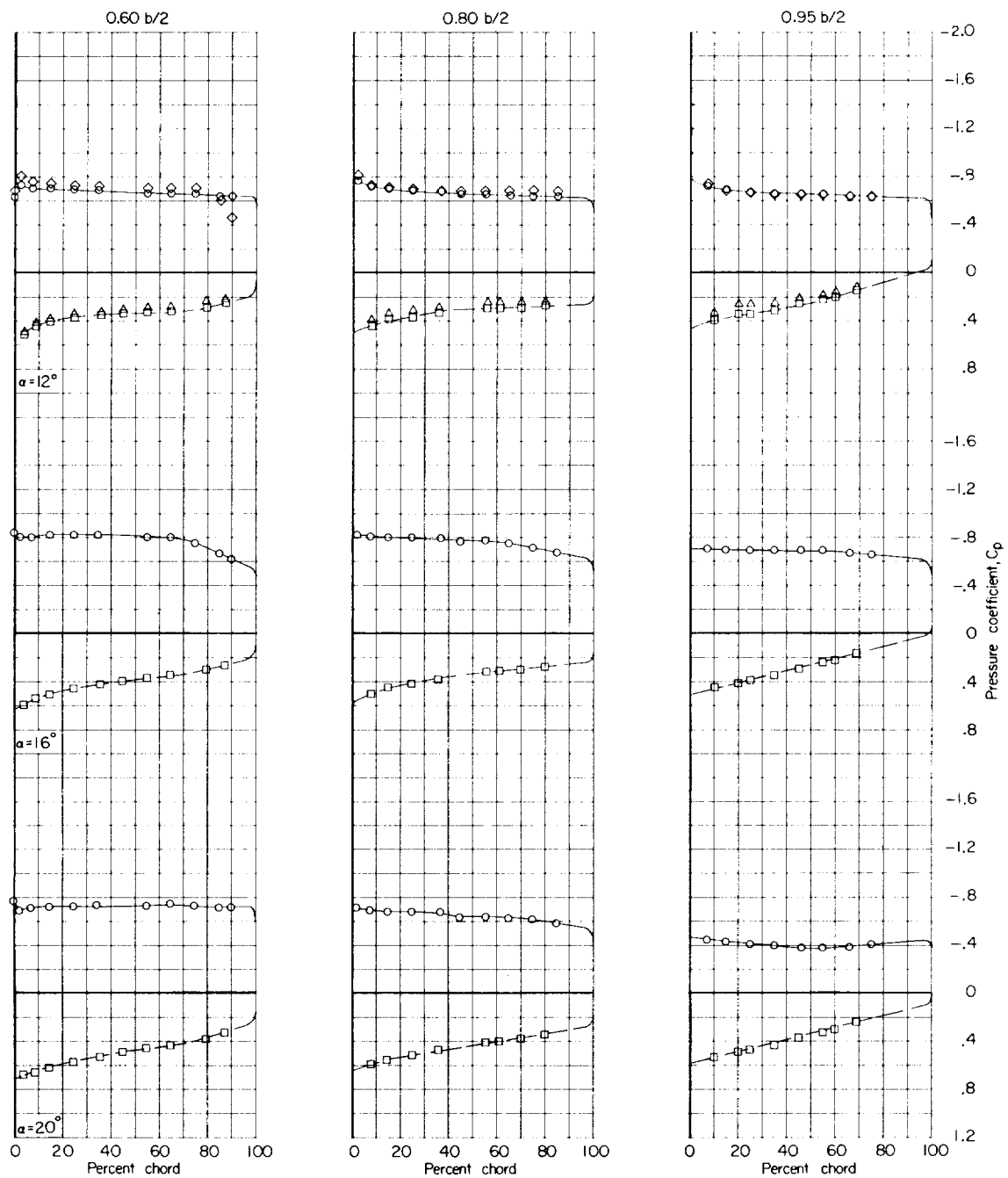
(t) Concluded.

Figure 4.- Continued.



(u) $M = 1.200$; $\alpha = 12^\circ$, 16° , and 20° .

Figure 4.- Continued.



(u) Concluded.

Figure 4.- Concluded.

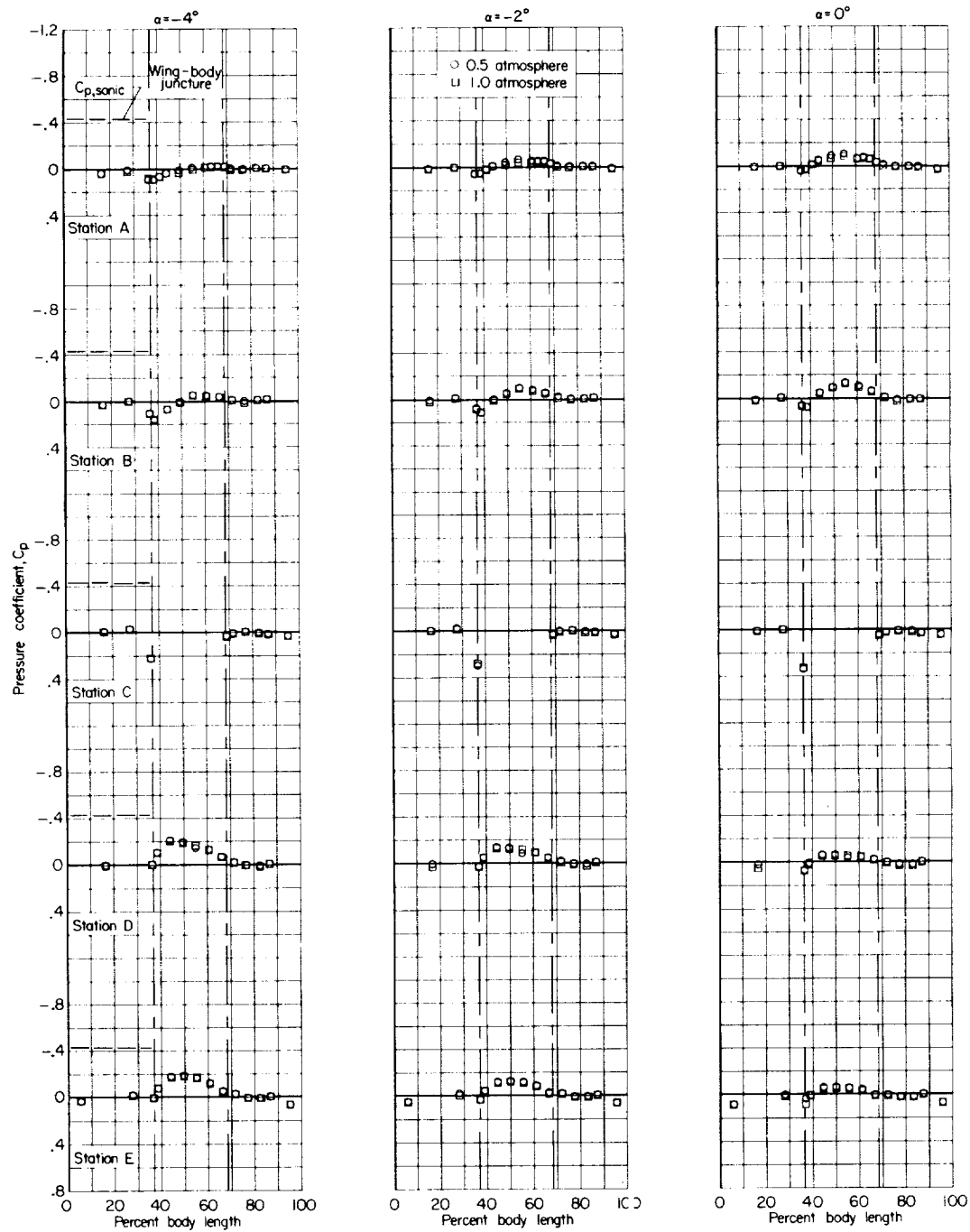
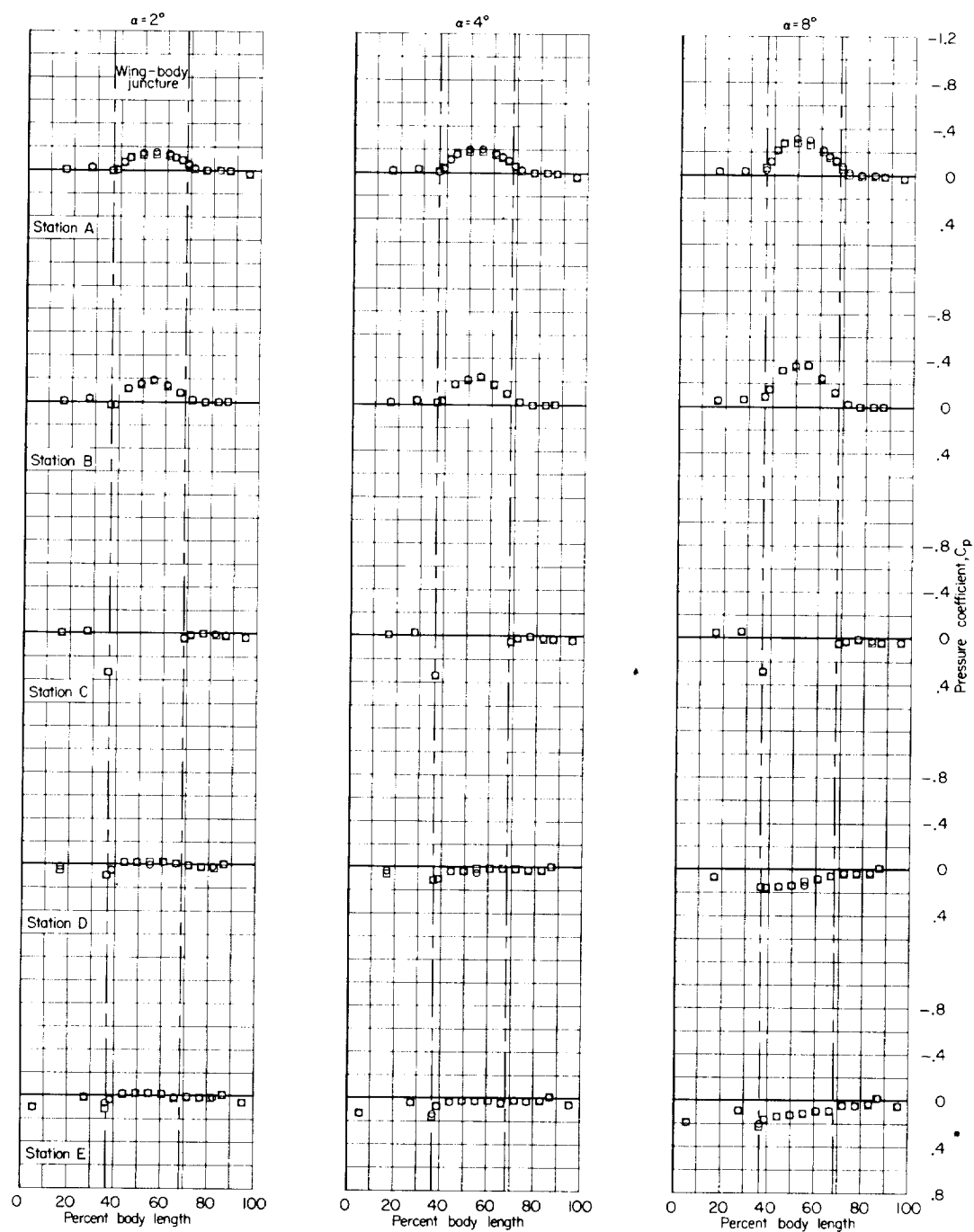
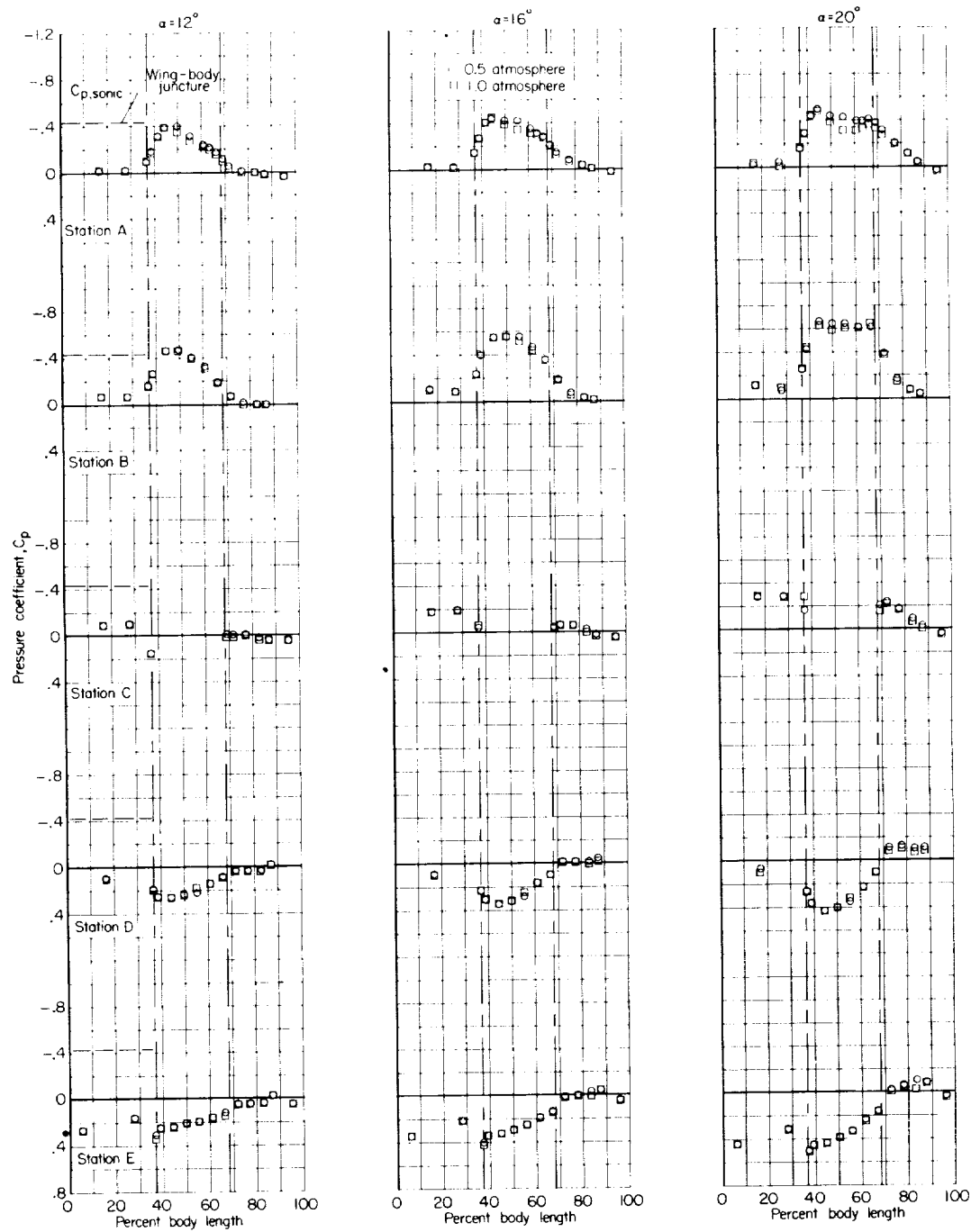
(a) $M = 0.800$.

Figure 5.- Pressure measurements on the body in the presence of the wing.



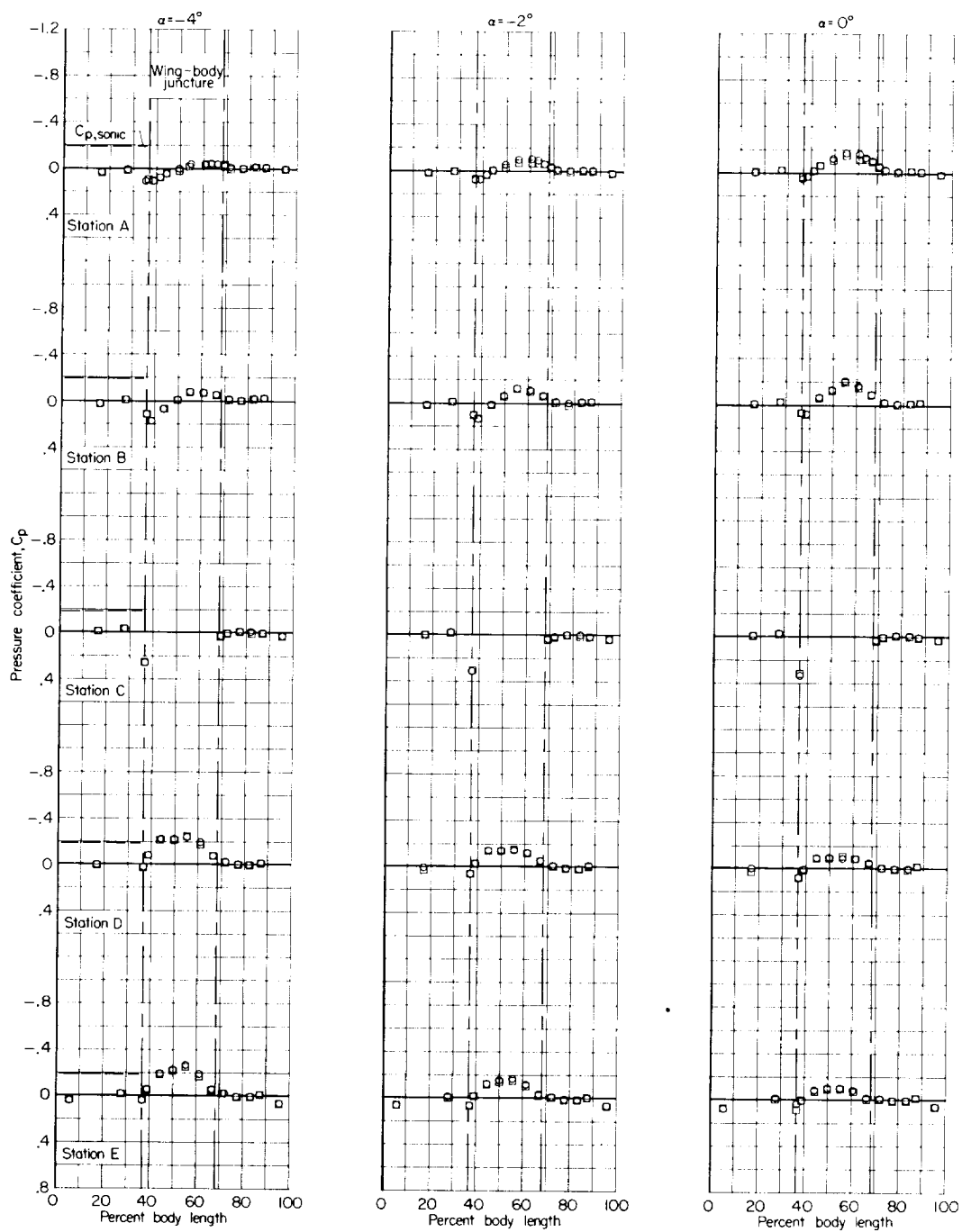
(a) Continued.

Figure 5.- Continued.



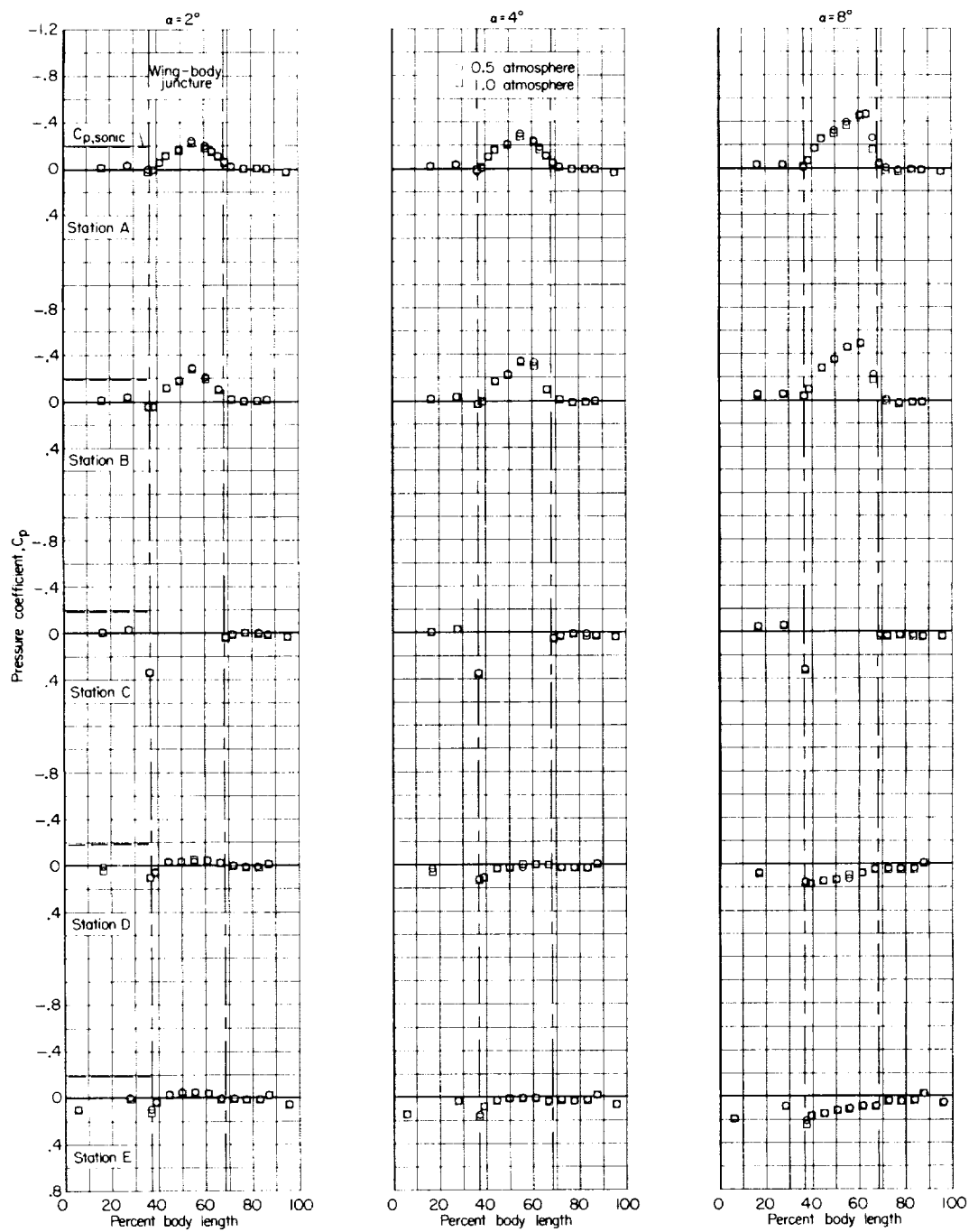
(a) Concluded.

Figure 5.- Continued.



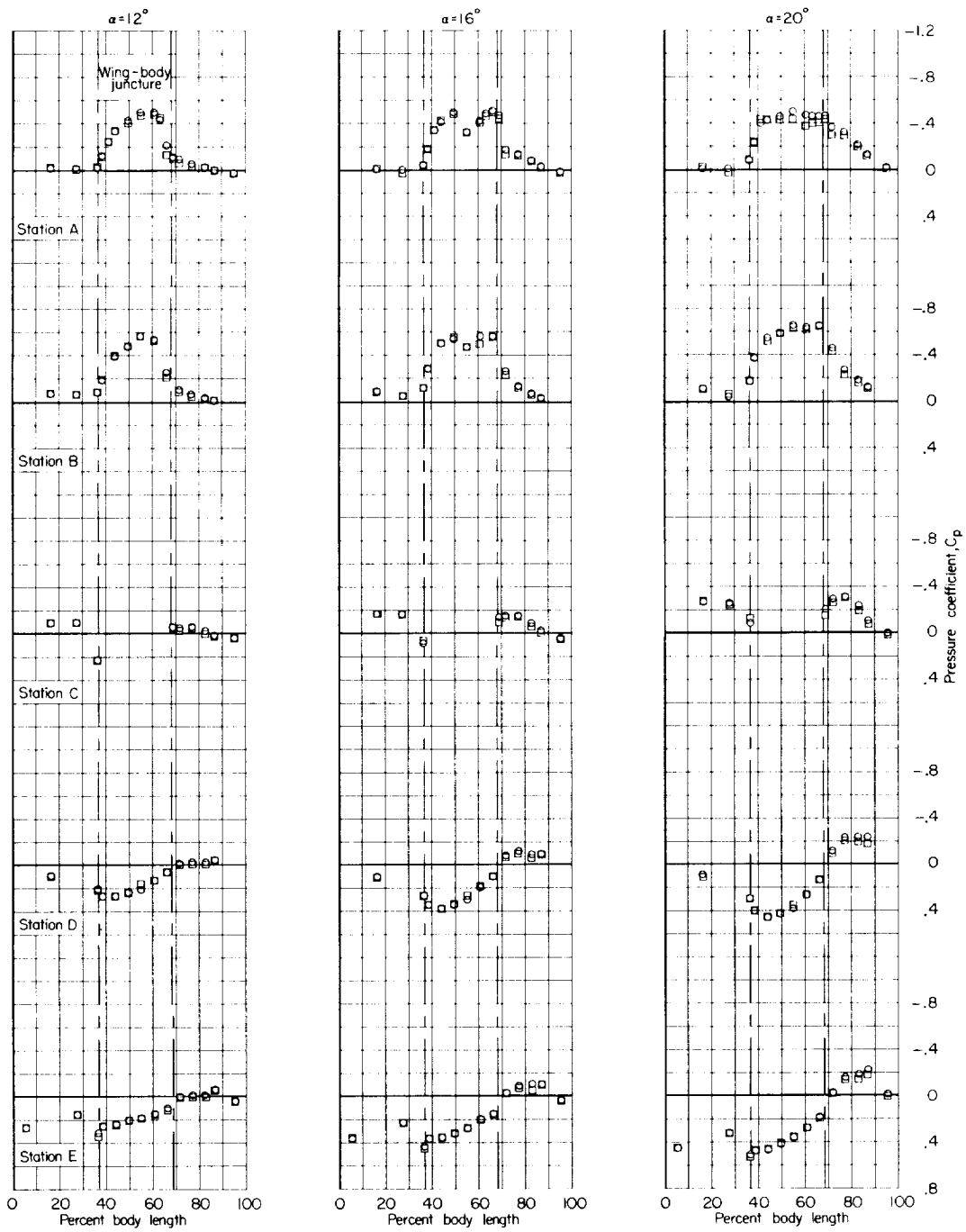
(b) $M = 0.900$.

Figure 5.- Continued.



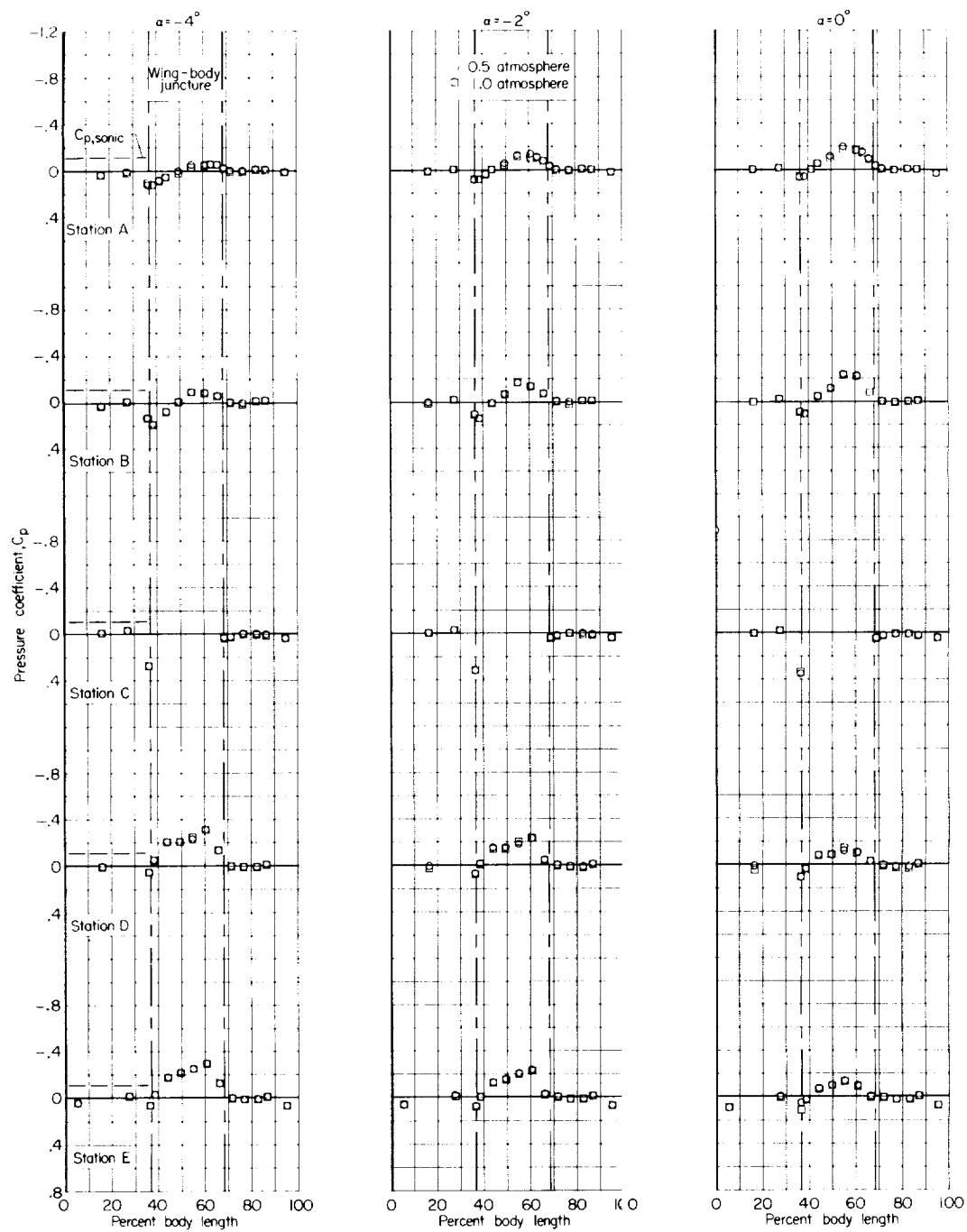
(b) Continued.

Figure 5.- Continued.



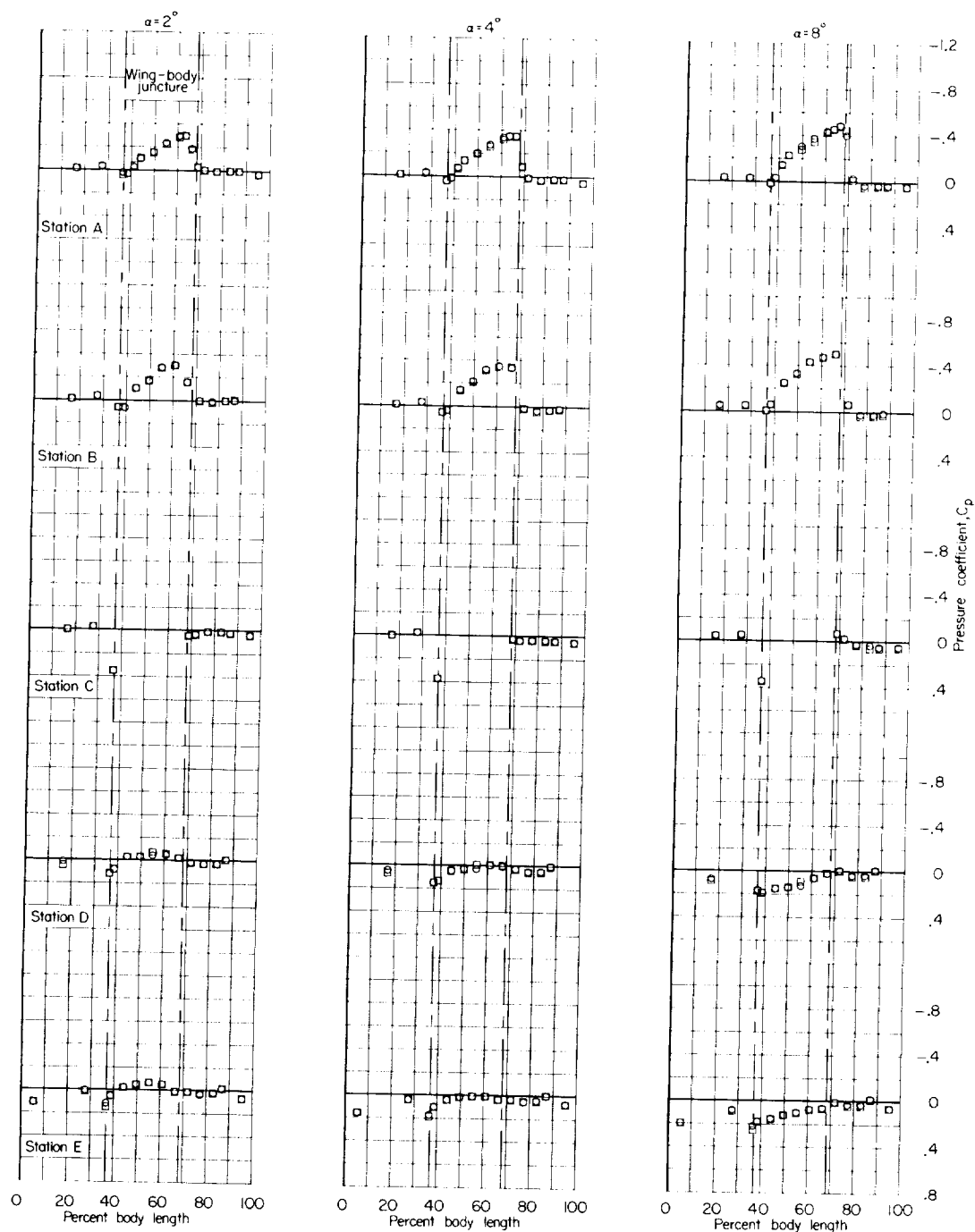
(b) Concluded.

Figure 5.- Continued.



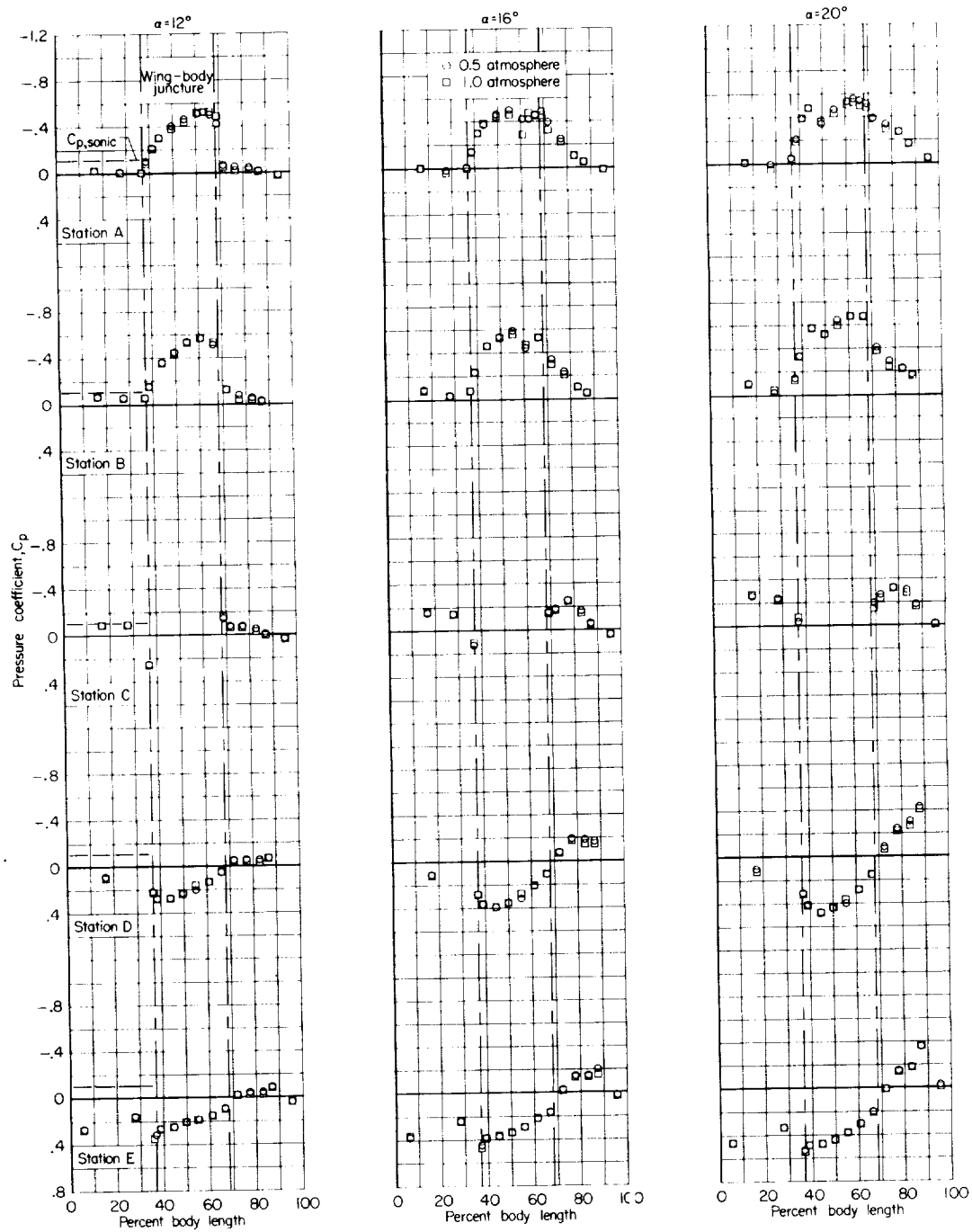
(c) $M = 0.940$

Figure 5.- Continued.



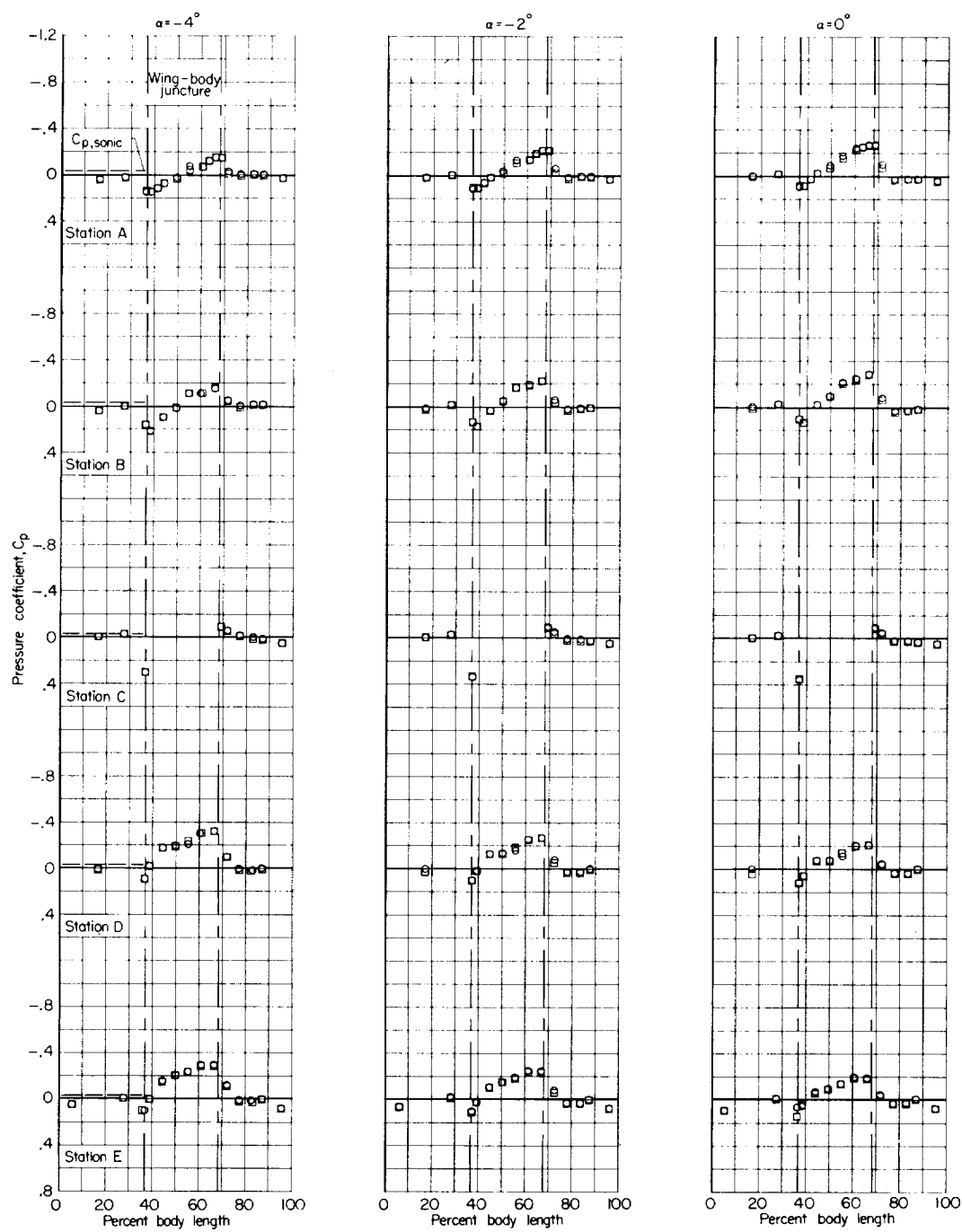
(c) Continued.

Figure 5.- Continued.



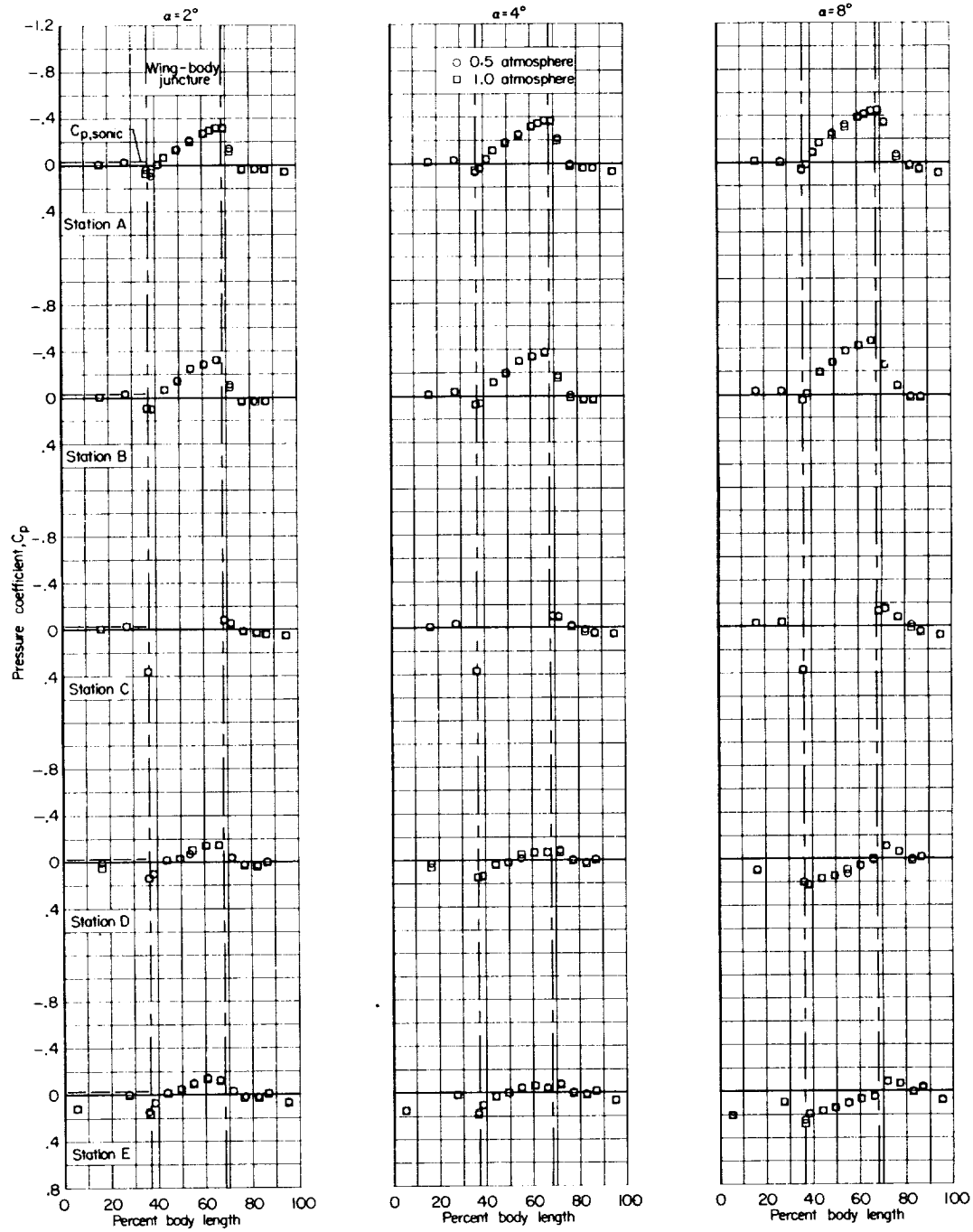
(c) Concluded.

Figure 5.- Continued.



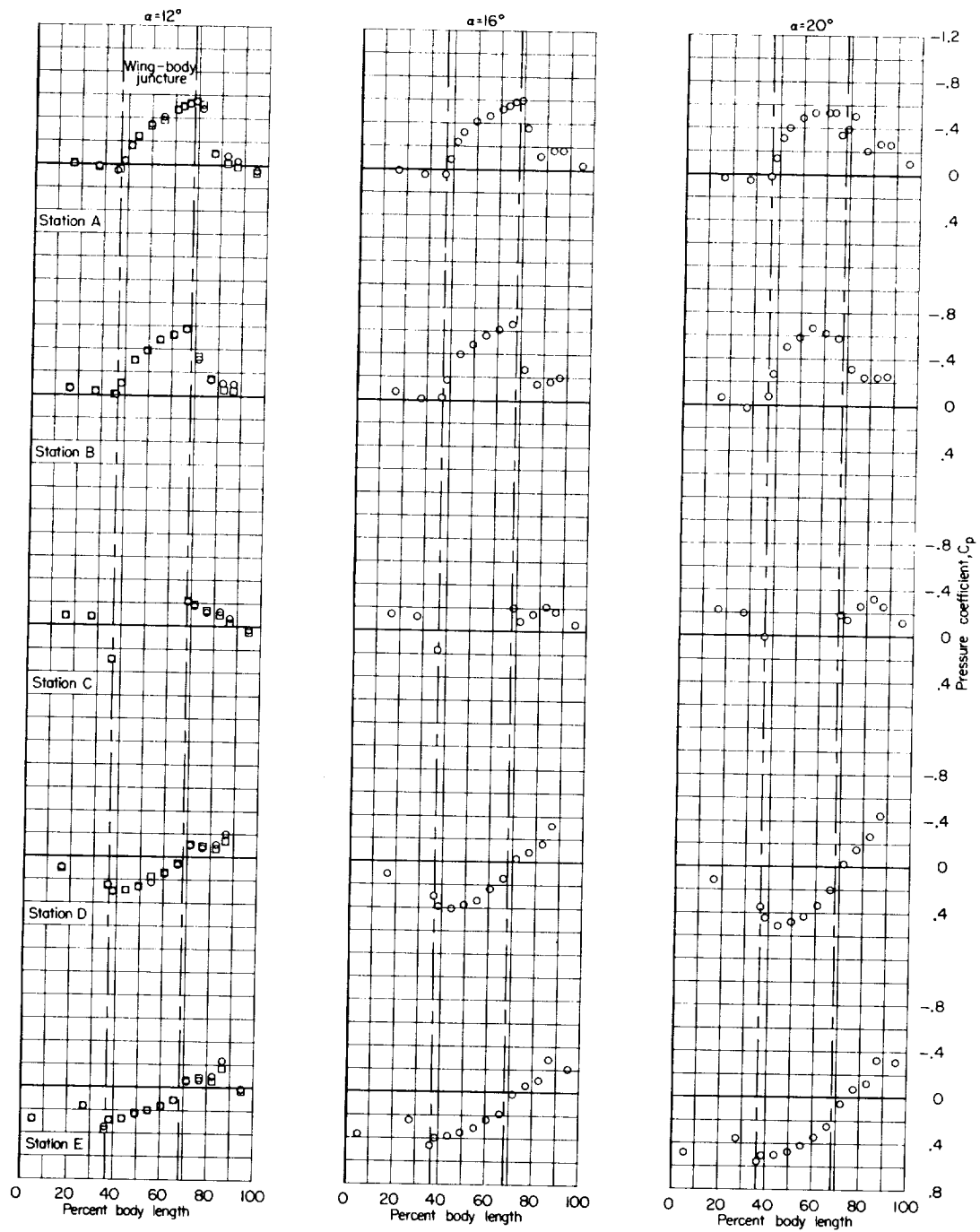
(d) $M = 0.980$.

Figure 5.- Continued.



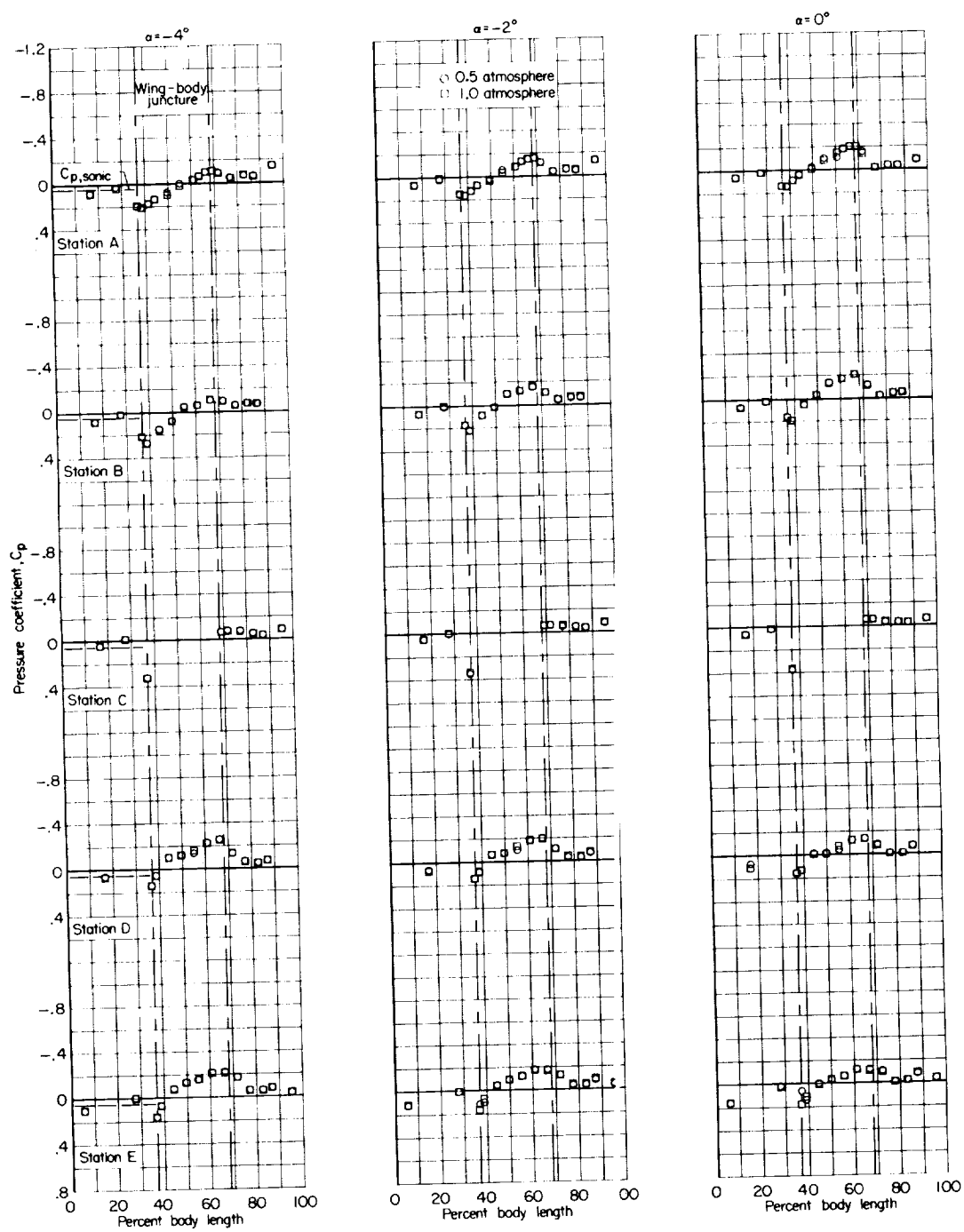
(d) Continued.

Figure 5.- Continued.



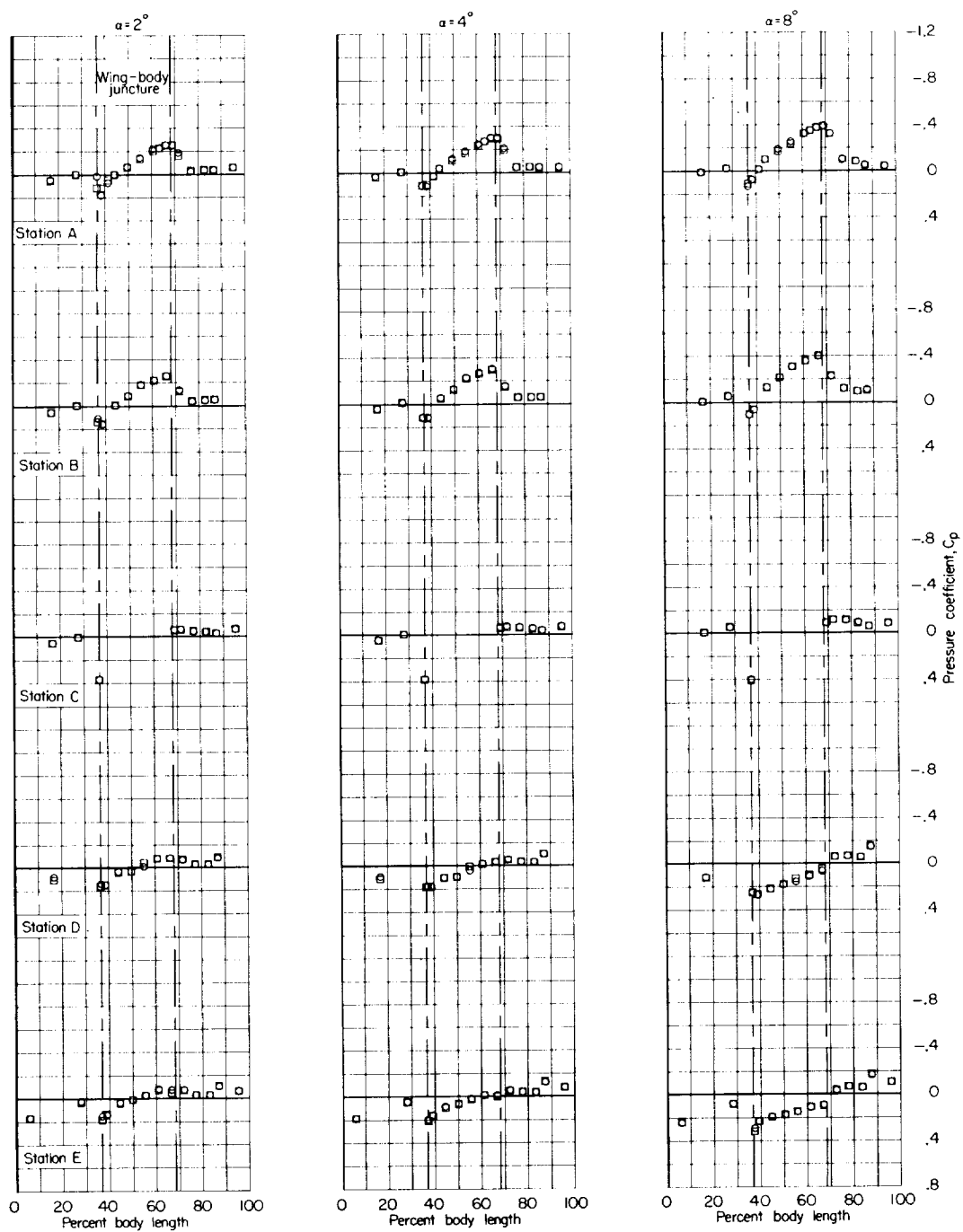
(d) Concluded.

Figure 5.- Continued.



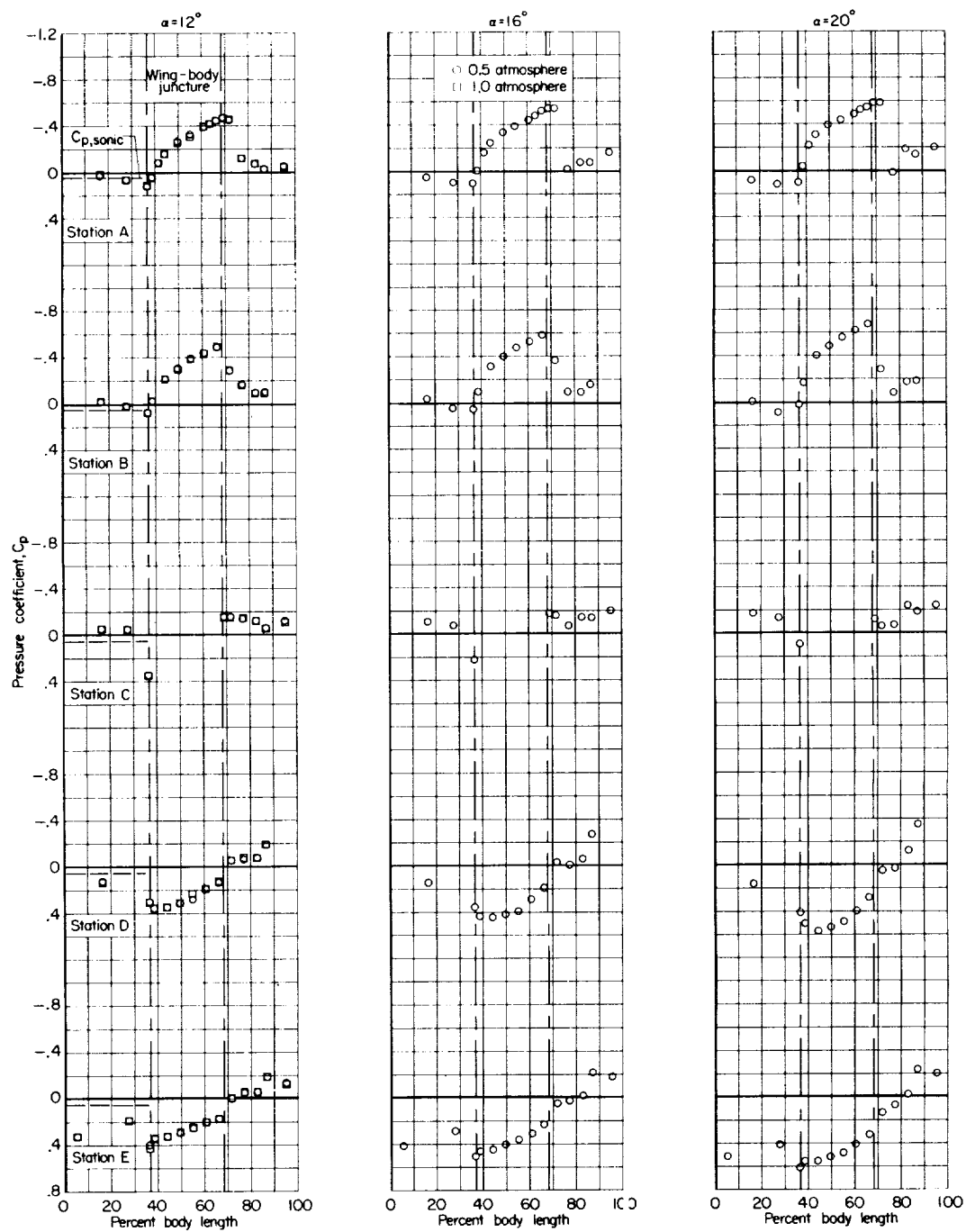
(e) $M = 1.030$.

Figure 5.- Continued.



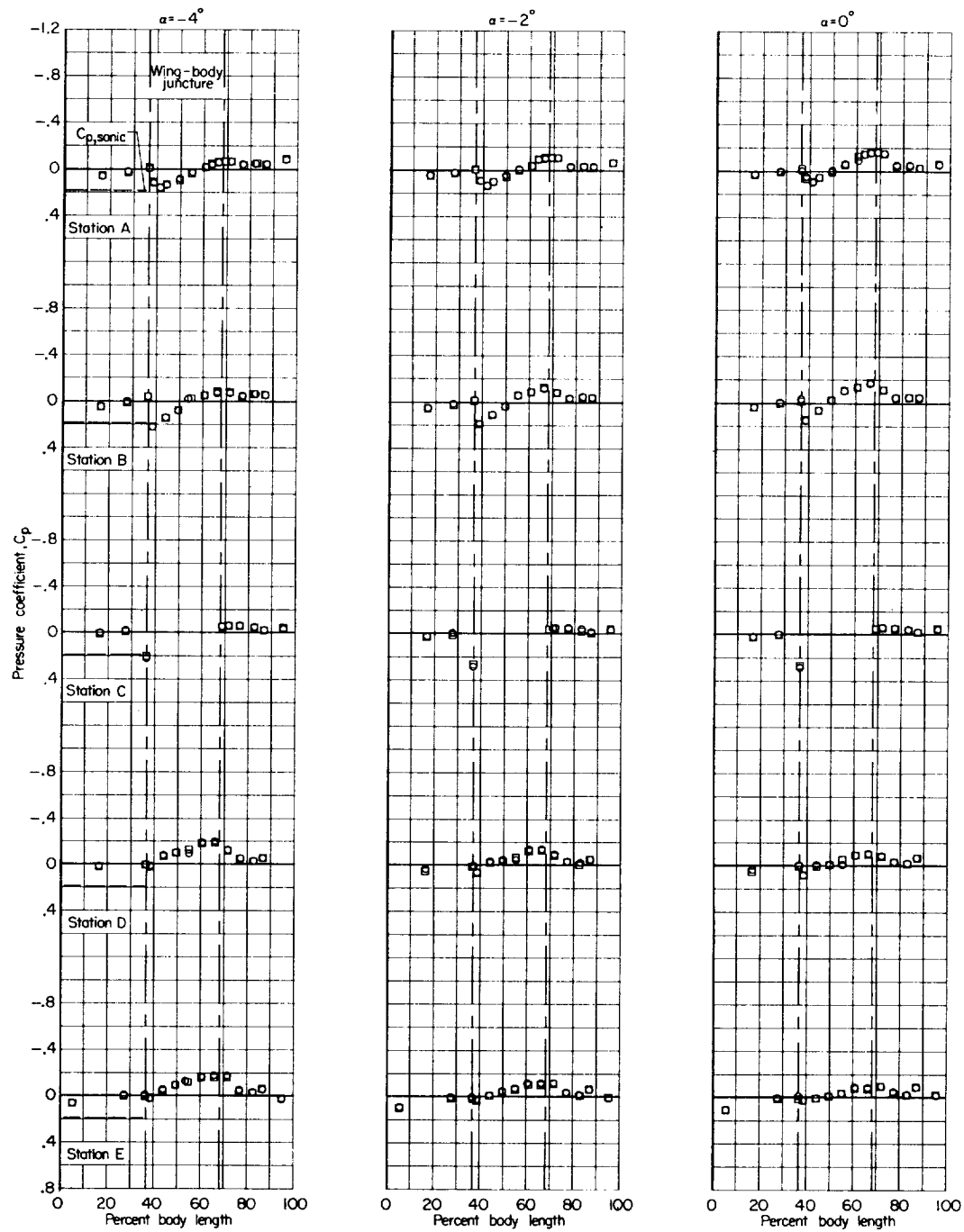
(e) Continued.

Figure 5.- Continued.



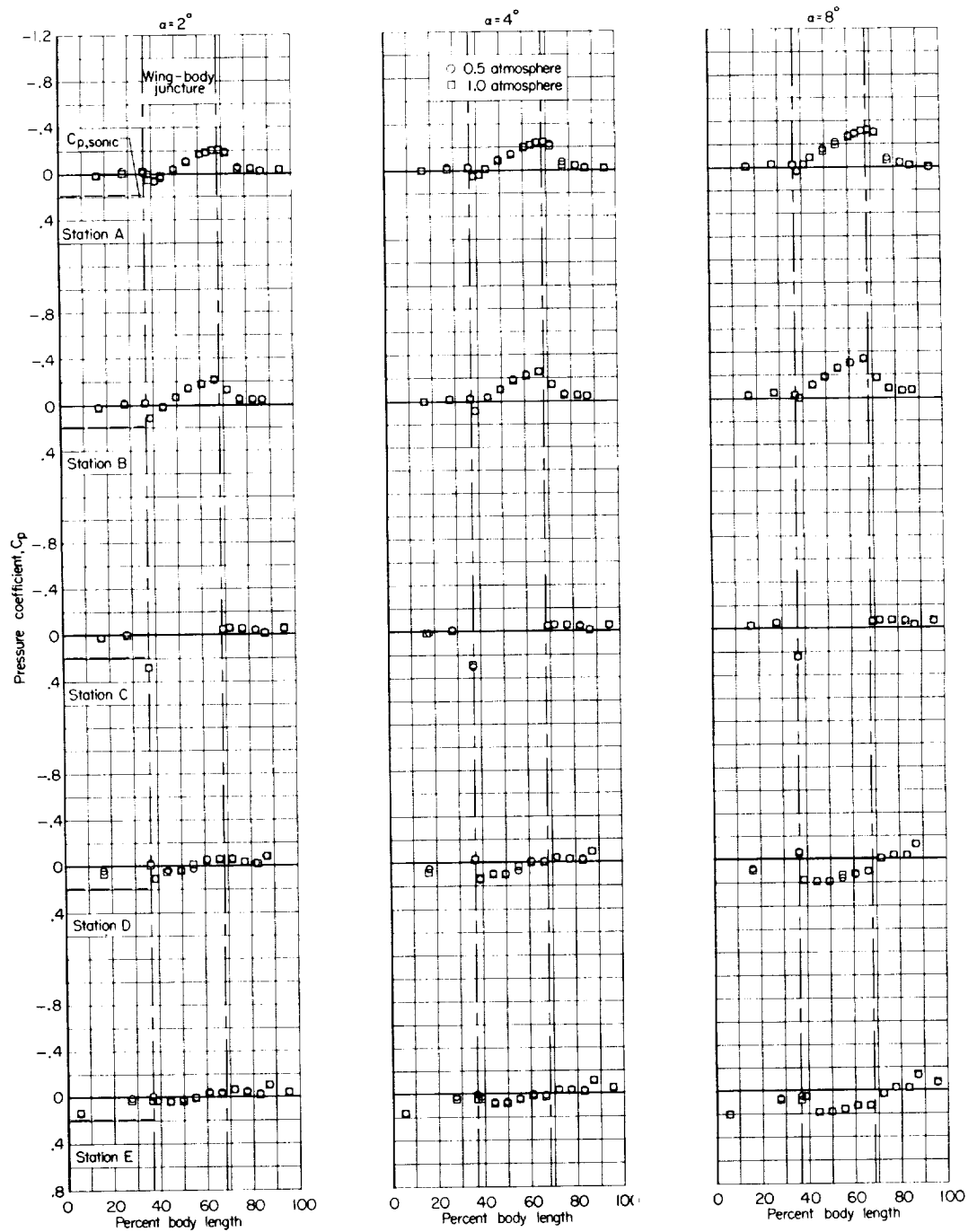
(e) Concluded.

Figure 5.- Continued.



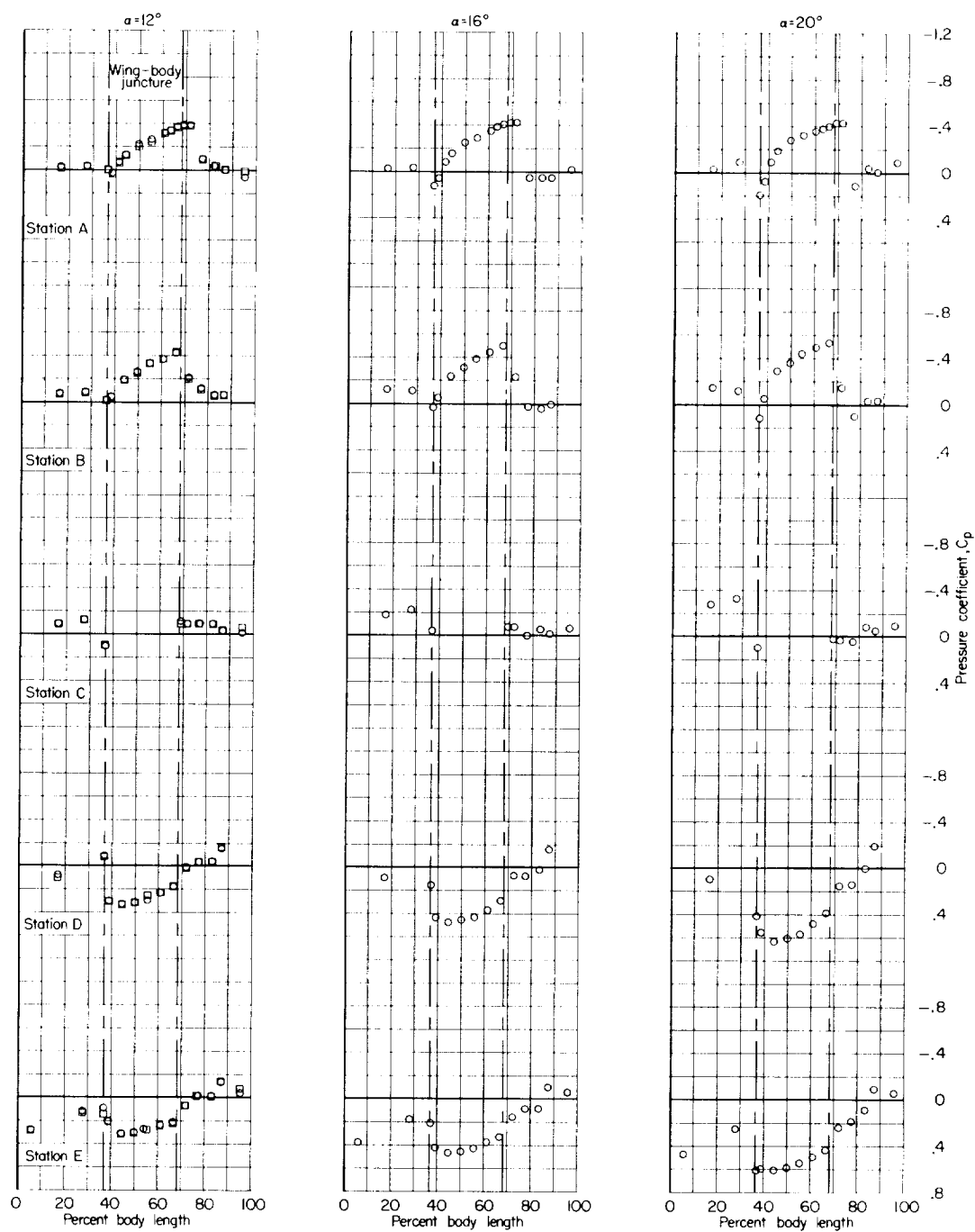
(f) $M = 1.125.$

Figure 5.- Continued.



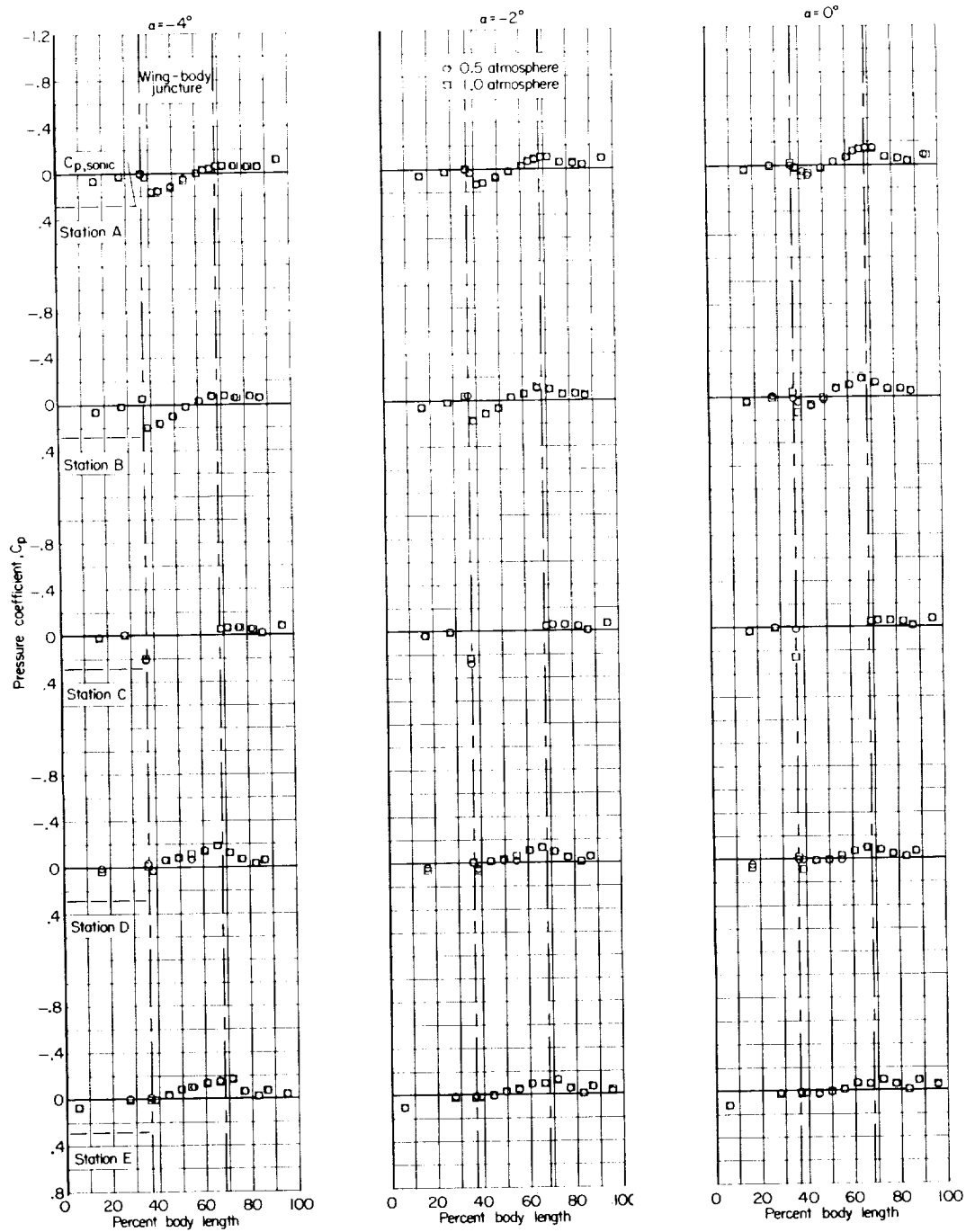
(f) Continued.

Figure 5.- Continued.



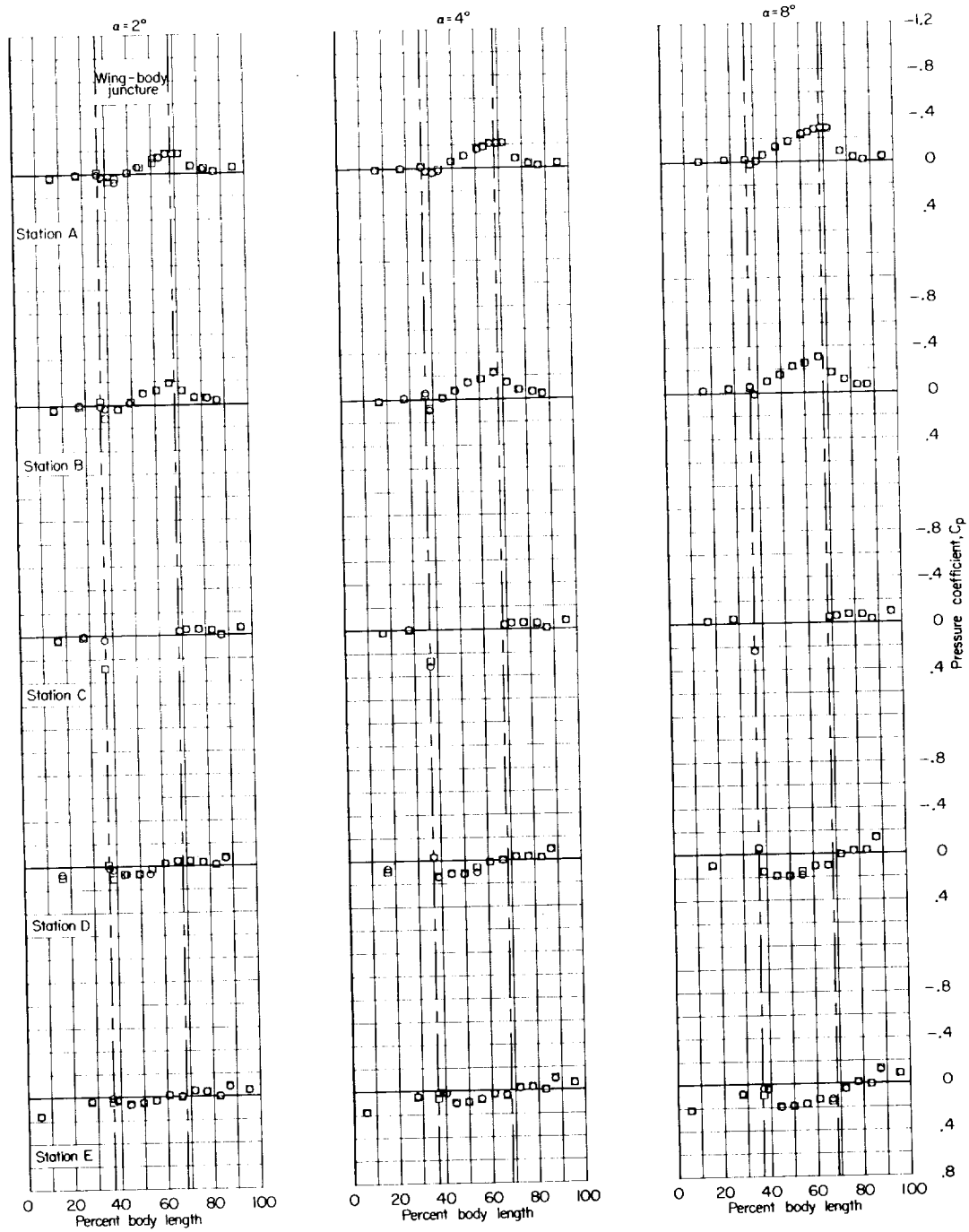
(f) Concluded.

Figure 5.- Continued.



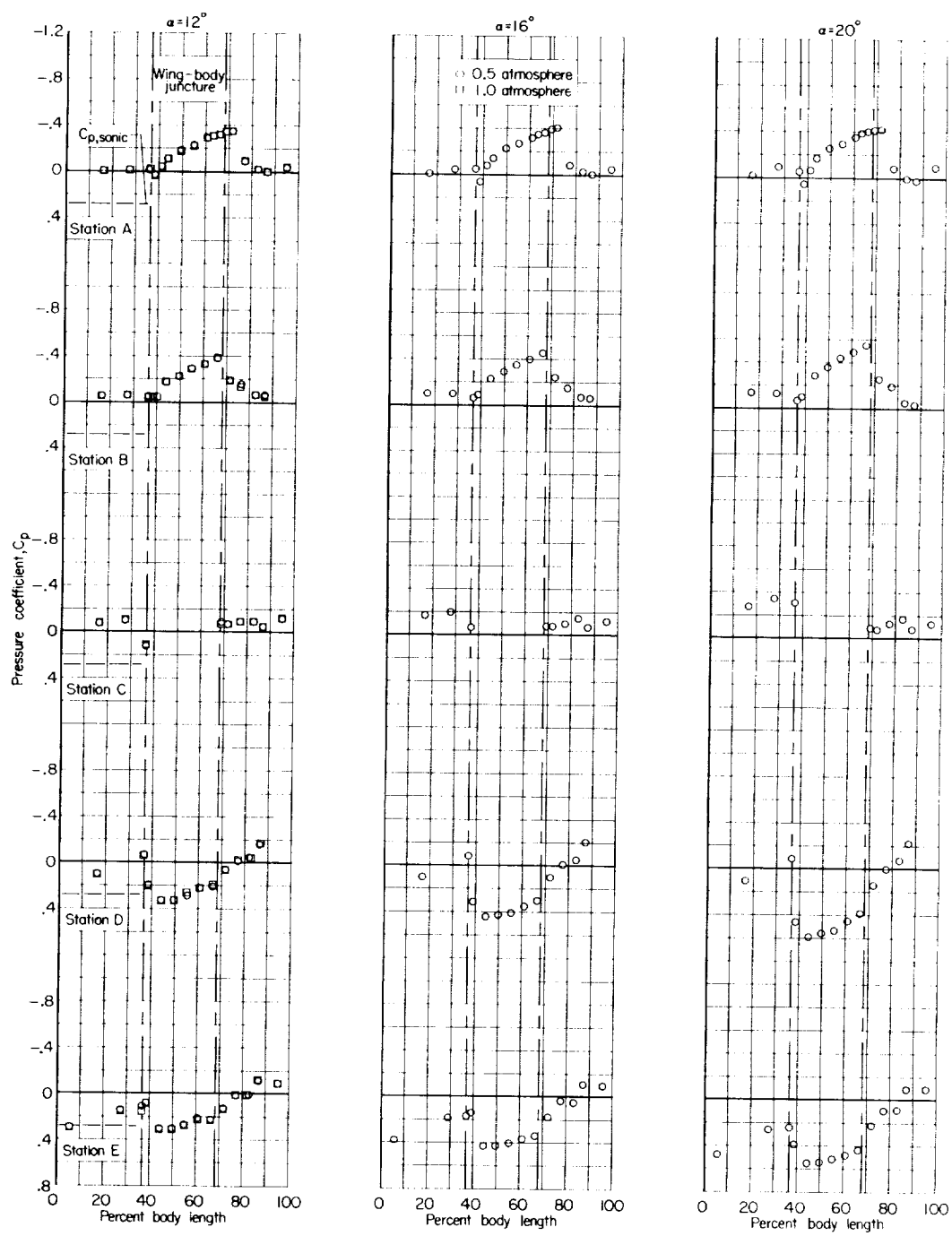
(g) $M = 1.200$.

Figure 5.- Continued.



(g) Continued.

Figure 5.- Continued.



(g) Concluded.

Figure 5.- Concluded.